NASA Contractor Report 3345

Electrostatic Protection of the Solar Power Satellite and Rectenna

Part II - Lightning Protection of the Rectenna

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Electrostatic Protection of the Solar Power Satellite and Rectenna

Part II - Lightning Protection of the Rectenna

Rice University
Houston, Texas

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SUMMARY AND CONCLUSIONS

1. The very high lightning flash density in many parts of the United States and the large size of the SPS rectenna require us to incorporate lightning protection systems in the rectenna design.

2. A distributed lightning protection system is described in this report that will protect the rectenna components from direct lightning strike damage and will, in addition, provide reduced induced lightning effects in the power and control circuits.

3. The proposed lightning protection system should be incorporated as a structural member of the rectenna support system; viewed as such, the lightning protection system will not appreciably increase the total material requirements for the rectenna unless materials are used that are incapable of safely conducting lightning currents.

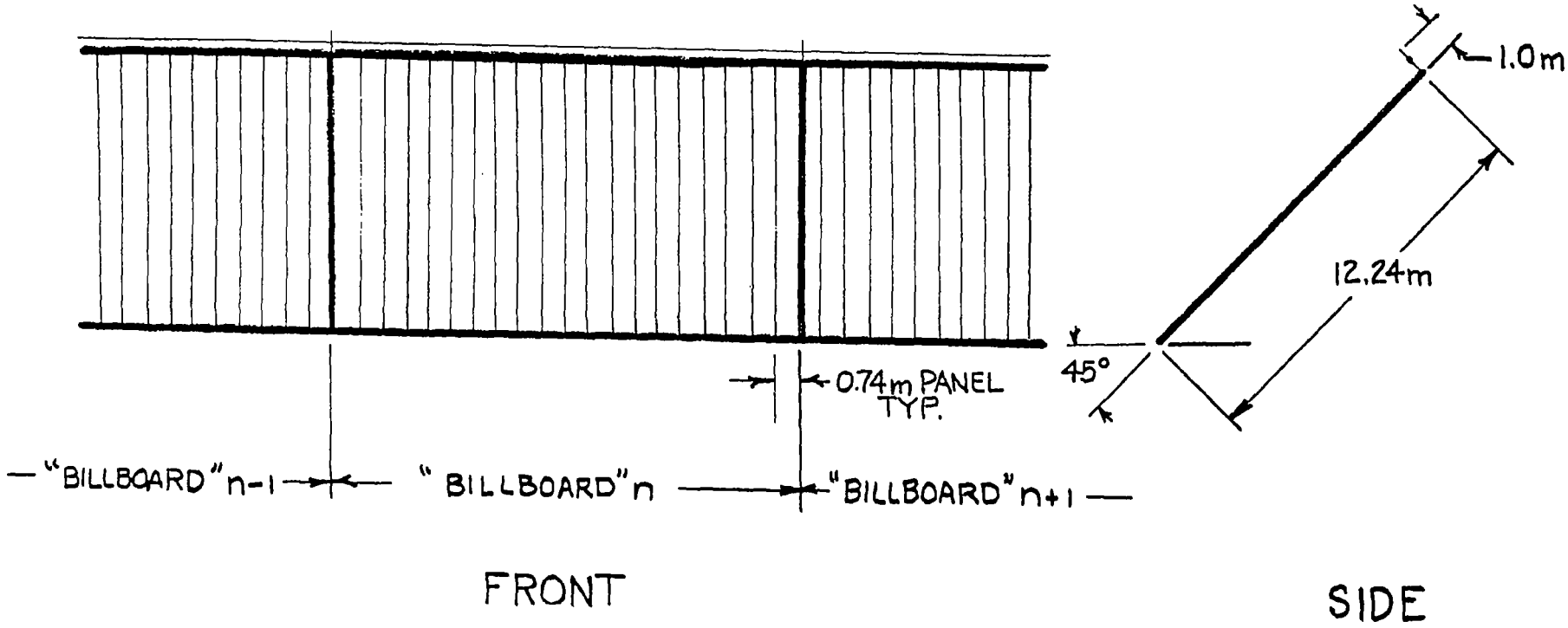
4. The lightning protection design places the conducting elements so that the microwave shadow cast by protection systems falls along the upper edge of the billboard on which it is mounted (and the lower edge of the next billboard to the north); these shadow areas are only a slight fraction of the collecting area, so the protection elements produce very little, if any, additional power loss to the rectenna as a whole.

5. Individually the microwave diodes are self-protecting with respect to "average" lightning and those near the center of the rectenna are safe from extreme lightning. However, the series connection of the diodes to form 40,000 V strings creates a protection requirement for the string. Standard surge protection practices are necessary for the string.

6. Electric power industries usually attribute 10% of the cost of power transmission equipment to lightning protection requirements. If this factor is not already included in cost estimates, it should be added.

SUMMARY OF THE RECOMMENDED LIGHTNING PROTECTION DESIGN

Based upon our research, computer simulations, and laboratory tests with a scale model, we recommend a distributed lightning protection system that employs a horizontal conducting member with points and grounds placed at every bay or billboard (14.69 meters apart). This configuration not only provides greater protection than other configurations that were evaluated, it is more easily integrated into the structural design of the rectenna. The recommended system is shown in Figure 1.



DISTRIBUTED LIGHTNING PROTECTION SYSTEM

FIGURE 1

PREFACE

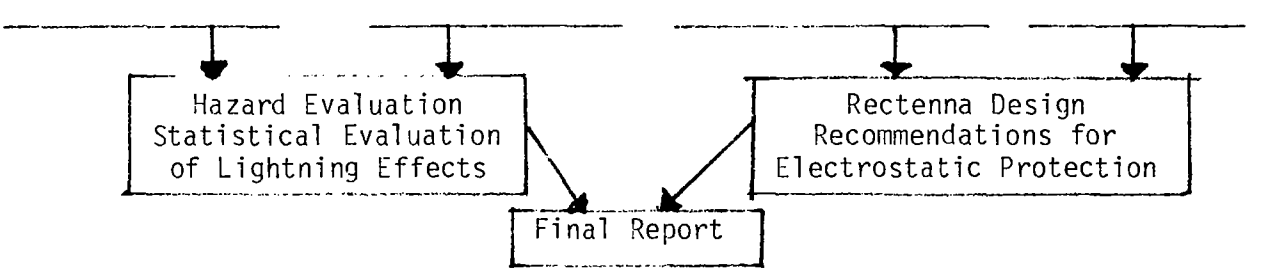
The objectives of this study are to evaluate the hazard posed by lightning flashes to ground on the SPS rectenna and to make recommendations for a lightning protection system that will provide sufficient protection to the rectenna. For purposes of this study, the SPS rectenna design is based upon the data supplied to us by Rockwell International in July, 1978.

This study has four major components, each with several elements of investigation. The components were: lightning distribution; lightning interactions; rectenna damage estimates; rectenna protection. The elements of each component are listed in Table A. The study plan was to proceed from top to bottom evaluating the elements listed in each component; work proceeded in a parallel manner for the four components. The organization of this final report reverses this order by presenting the more important results of the study first, then following this with the material and considerations leading to the conclusions.

TABLE A

Rectenna Electrostatic Protection

Lightning Distribution	Lightning Interactions	Rectenna Damage Estimates	Rectenna Protection
1. Obtain climatological data.	1. Review/compile data on lightning parameters.	1. Diode failure modes (scaled from available diodes.)	1. Panel transient protectors.
2. Format data for computer use.	2. Construct program for computation of fields and currents in the rectenna plane from parameterized lightning	2. Insulation breakdown.	2. Billboard surge protectors.
3. Construct program for computation of lightning density.	3. Evaluate enhancement factors.	3. Direct strike damage estimates.	3. Lightning Inverter protectors
4. Produce contour map of lightning density.	4. Conduct laboratory simulations.	4. Direct strike damage estimates.	4. Lightning rod systems.



The Principal Investigator was J.W. Freeman, Jr., and the principal author of this section of the final report was A.A. Few, Jr. They wish to express their thanks and appreciation to the following co-authors, all of whom were or are associated with Rice University.

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I. ANALYSIS OF LIGHTNING ROD PROTECTION CAPABILITIES FOR A CONFIGURATION SUITABLE TO THE RECTENNA

1. Cone of Protection Considerations:

I. 1.1 Definition and Considerations

The capability of a vertical conductor to attract a lightning flash is described by the cone-of-protection, or perhaps more accurately the cone-of-attraction. In theory, any lightning flash that would have entered this cone had the vertical conductor not been in place, will strike instead the conductor and be shunted to the ground. The method by which this process takes place is as follows:

> The lightning stepped leader creates high voltages over a wide area on the rectenna because of the large charge on the leader tip. At points on the rectenna where the electric field reaches breakdown values due to local enhancement factors, upward propagating sparks are initiated which move to meet the downward propagating stepped leader. The upward propagating spark which first makes contact with the leader completes the electrical circuit and the lightning flash current will pass through the structure that initiated the successful upward going spark.

The cone of protection is primarily a function of the height of the vertical conductor because of the field-enhancement factor which enables the taller object to initiate the upward spark before lower objects. Other factors enter into the consideration of the cone of protection, such as the charge on the leader tip and the velocity of the leader, because these factors strongly influence the timing of the production of upward sparks and the height at which the spark and leader meet. In general, the results of research into this subject have shown that the larger the leader charge, then the larger the angle β of the associated cone of protection. Since larger leader charges are usually associated with the larger lightning currents, we find a fortunate result that the cone of protection increases with the potential hazard of the lightning flash.

It follows then that the angle β of the cone of protection (See Figure 2) varies with the particular lightning flash. $\beta = 45^0$ is a very commonly used design angle in the United States and many of the examples in this report employ $\beta = 45^0$.

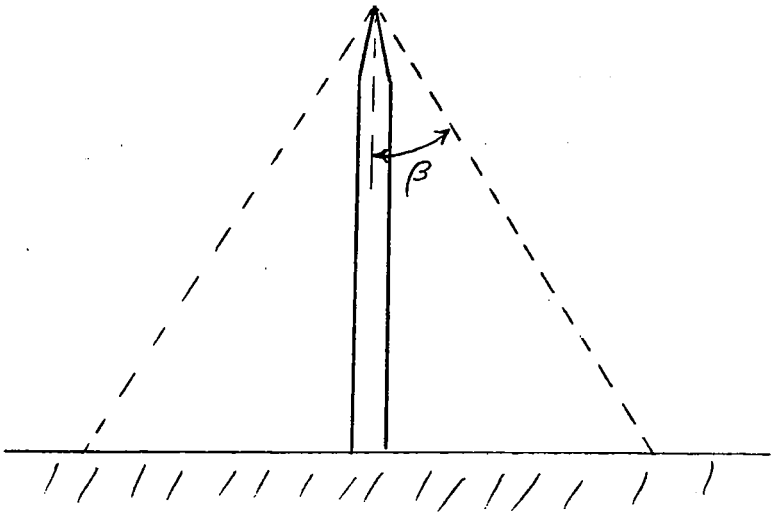


Figure 2

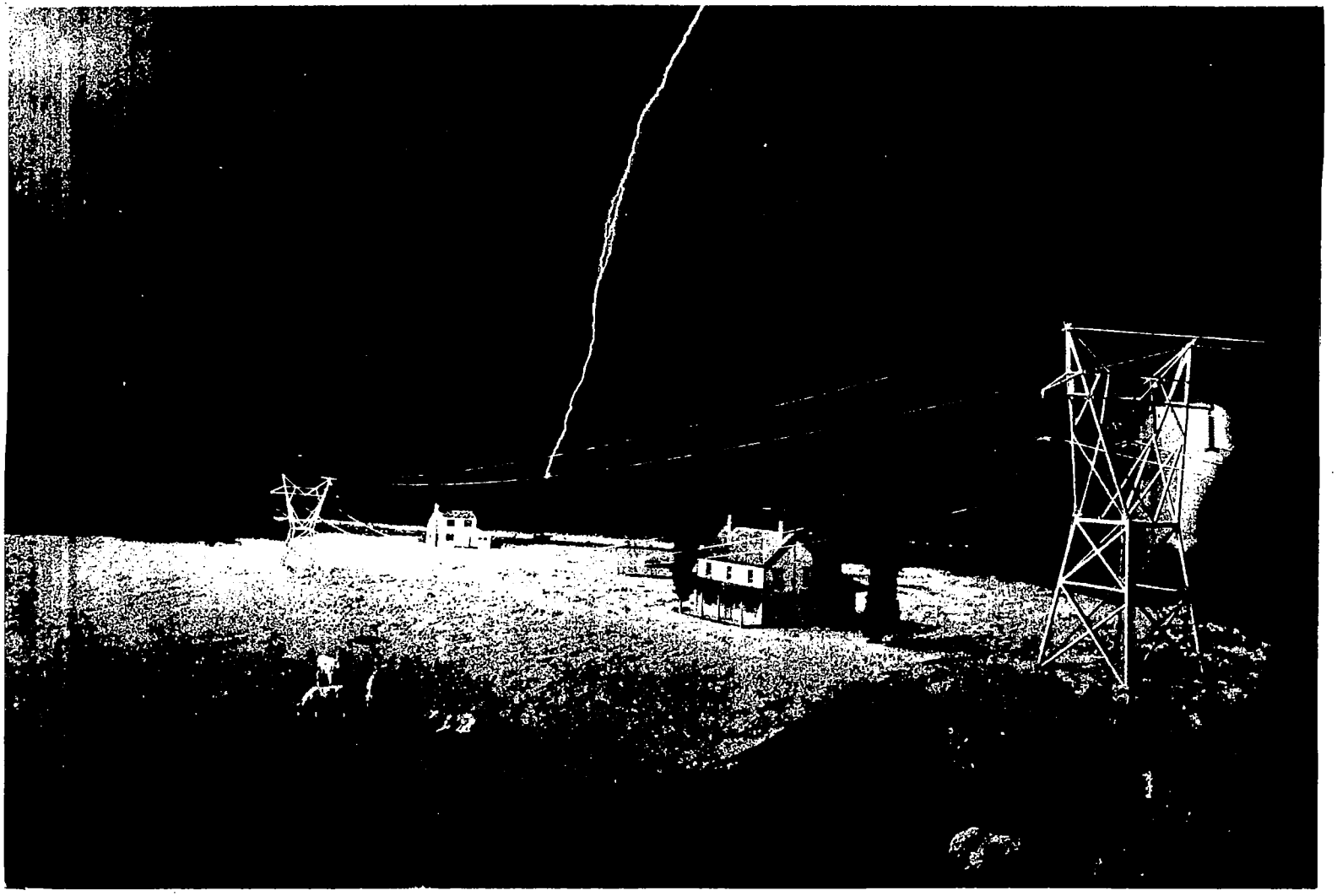
1.2 Distributed Lightning Protection Systems

The cone of protection and the experimental data used to evaluate are specifically related to the single elevated point, and in most cases the system under consideration is 10 to 100 meters in height. As will be seen later, lightning protection of the rectenna falls into a class of structures that requires distributed lightning protection tactics. Figure 3 illustrates a distributed system used by power transmission companies. The main point is that the cone of protection concept is of limited usefulness in the total protection problem. We will use it on the panel and billboard scale as a technique to make a comparative assessment of capabilities of various configurations.

2. Lightning Rod Protection Configurations Compatible with the SPS Rectenna

We have considered three different configurations of lightning rod systems in this effort. In the smallest scale system considered each rectenna panel (0.74m in width) had a short lightning rod attached; see upper example in Figure 4. In the medium scale system each rectenna support structure (14.69m apart) or billboard will have an attached lightning rod; see middle example in Figure 4. And, in the distributed protection system, short terminals located on each rectenna support structure (14.69m apart) were connected by horizontal conducting structures; see lower example in Figure 4.

As seen in the analysis of the billboard scale system, it is impractical to seriously consider larger scale systems.



POWER LINES EMPLOY DISTRIBUTED LIGHTNING PROTECTION SYSTEMS. THIS ILLUSTRATION SHOWS A "STATIC" OR GROUNDED PROTECTION WIRE TAKING A STRIKE AND PROTECTING THE POWER LINES BELOW.

FIGURE 3

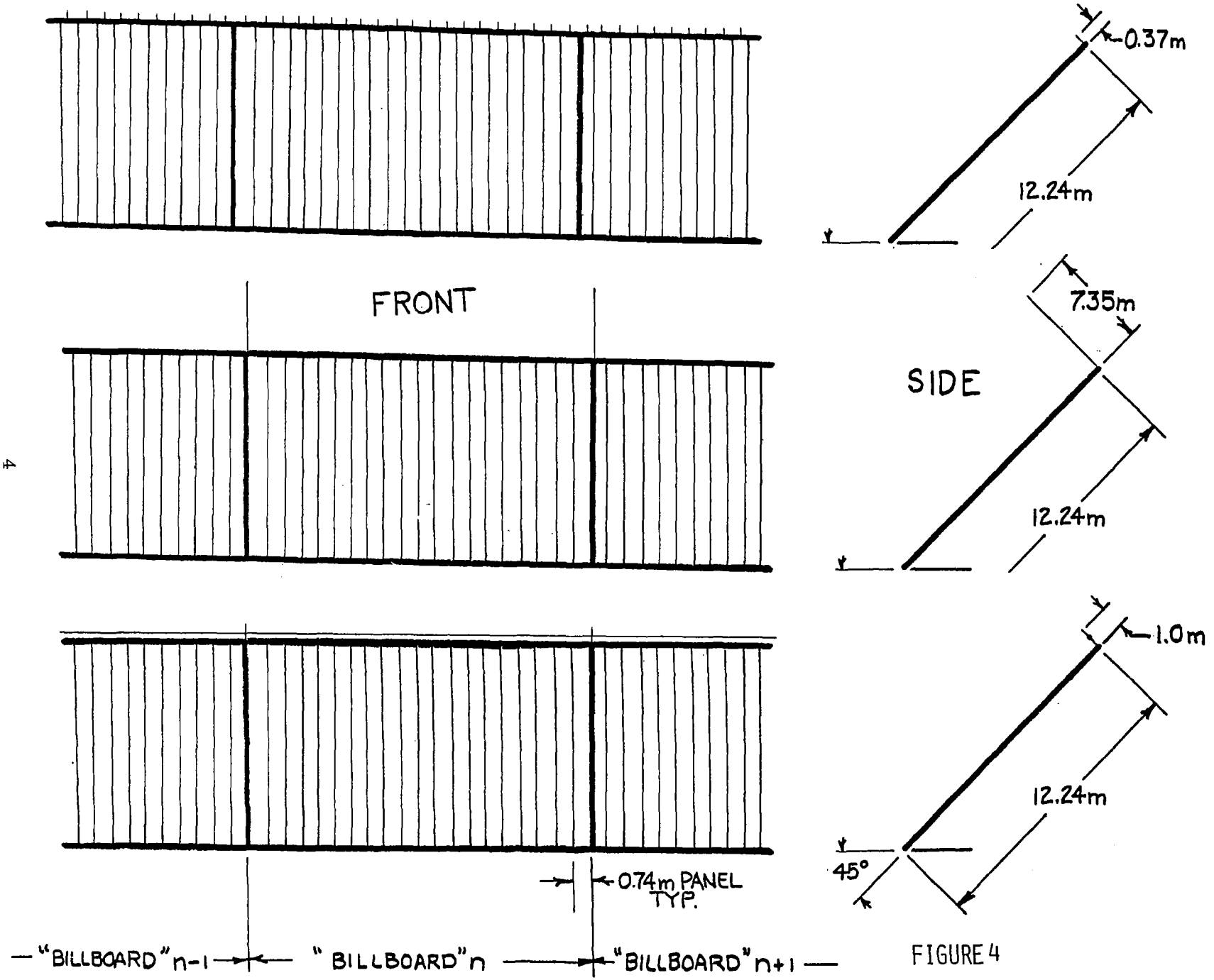
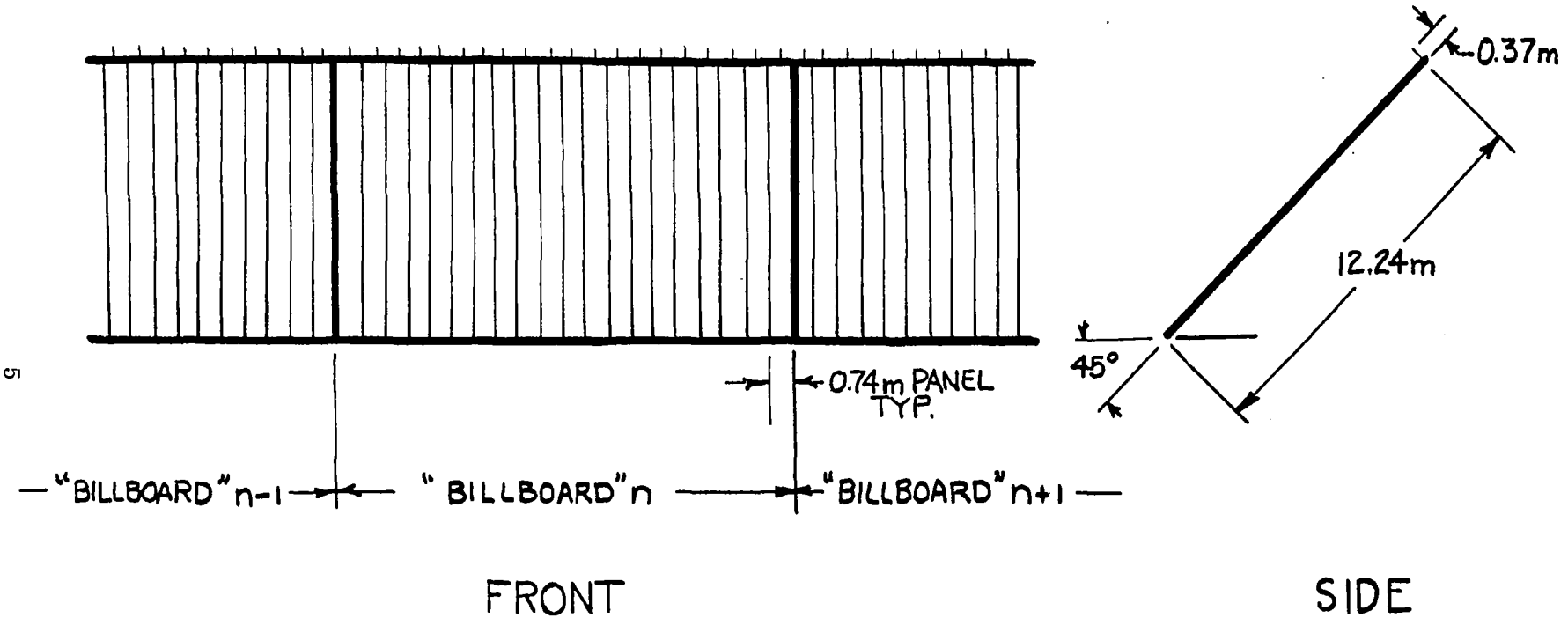

FRONT
SIDE
0.37m
12.24m
7.35m
12.24m
1.0m
12.24m
45°
0.74m PANEL TYP.
"BILLBOARD" n-1
"BILLBOARD" n
"BILLBOARD" n+1

FIGURE 4



PANEL SCALE LIGHTNING PROTECTION SYSTEM

FIGURE 5

2.1 Lightning Rod Protection at the Panel Scale

In this system configuration a relatively short lightning rod is positioned at the top of each panel and oriented perpendicular to the panel face (see Figure 5). Conceptually the rod is centered on the top of the panel, but in practice it could be on the panel edge without altering the results of this analysis.

Let α be the inclination of the rectenna. Figure 6 illustrates the case where β, the angle of the cone of protection, is greater than α. This figure applies only to the conditions in the vertical plane that passes through the lightning rod and is perpendicular to the rectenna face. In this particular projection it appears that the short (example 0.74m) lightning rod on the panel provides adequate protection to the rectenna. In other projections we see that there are, however, "holes in the armor."-

Figure 7 is an enlargement (x10) of the lightning rod portion of Figure 6, and defines the parameters to be used in the following discussions. The cone of protection intersects the plane of the rectenna to form conic sections:

(1) If $\alpha + \beta = 90^0$ the intersection is a parabola.
(2) If $\alpha + \beta < 90^0$ the intersection is an ellipse. (this is the case illustrated in Figures 6 & 7)
(3) If $\alpha + \beta > 90^0$ the intersection is a hyperbola.

If we now look at the intersection of the cone of protection with the panel for the specific cases above, we see the emergence of the protection problem with this type of lightning rod protection configuration. From the geometry of Figure 7 we see that the axis of the cone is at $\ell = L \tan \alpha$ and that the vertex of the conic is at $d = L \tan(\beta - \alpha)$ relative to the top of the panel.

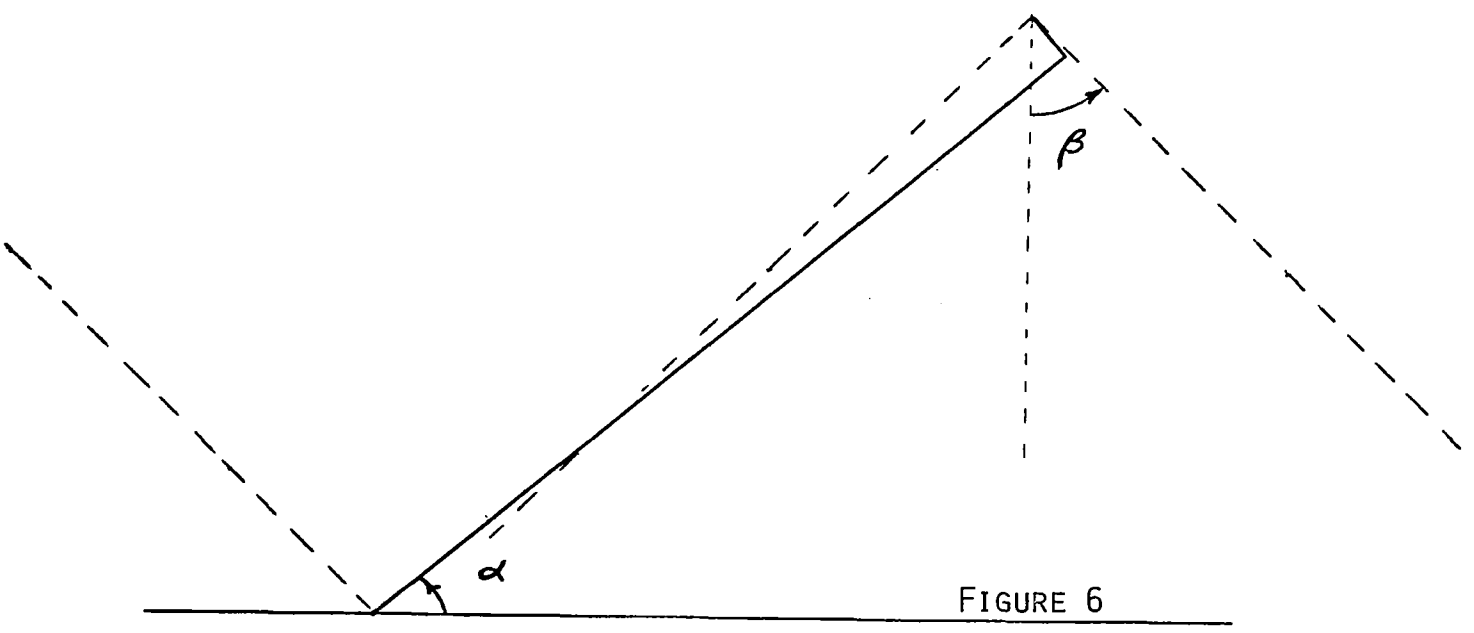


FIGURE 6

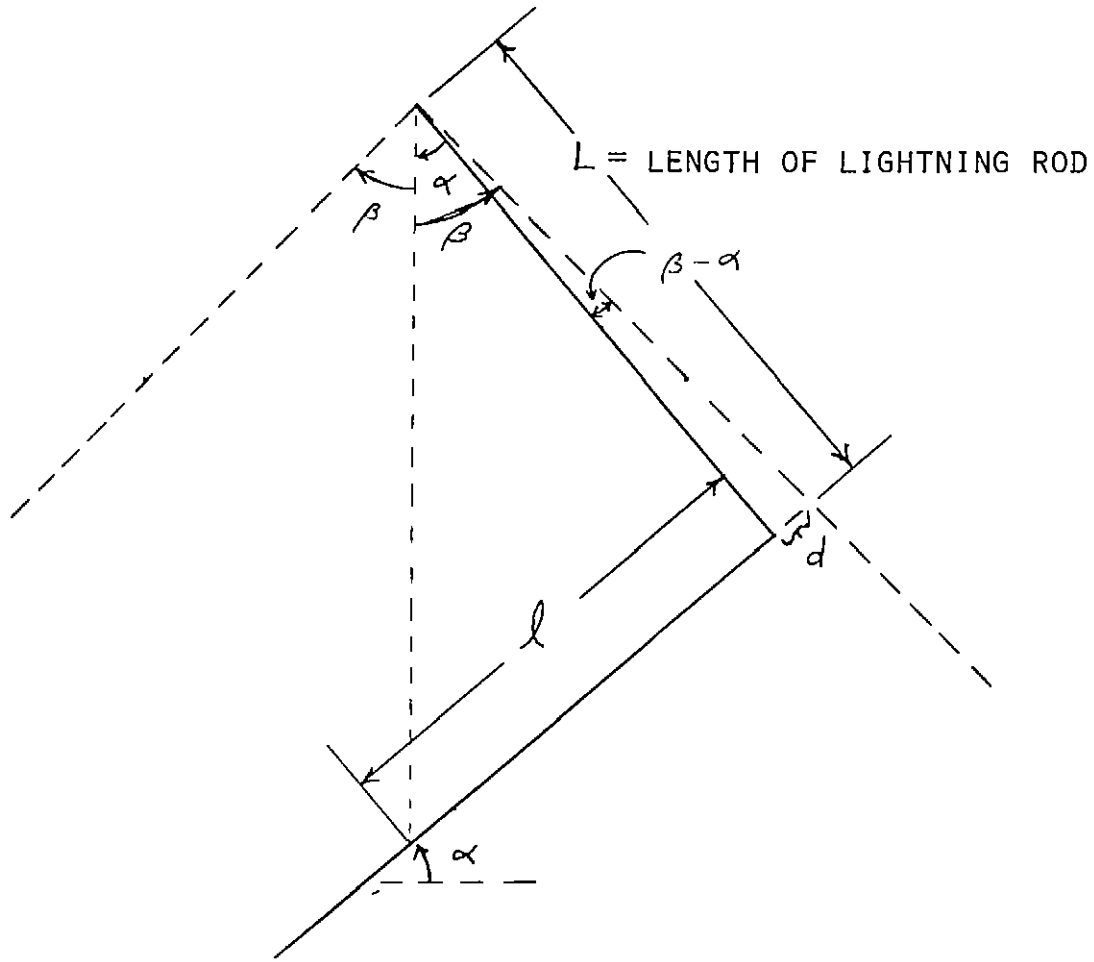


FIGURE 7

ENLARGED VIEW OF THE UPPER END OF THE RECTENNA IN FIGURE 7.

In a coordinate system defined in the rectenna plane with the origin at the axis of the cone and the y axis directed north (toward top of rectenna) and the x axis directed east, the equation for conic is:

$$\frac{x^2\cos^2\alpha}{L^2\tan^2\beta} + \frac{y^2(\cos^2\alpha - \sin^2\alpha\tan^2\beta)\cos^2\alpha}{L^2\tan^2\beta} + \frac{2y\sin\alpha\cos\alpha}{L} = 1$$

For the parabolic solution this equation reduces to:

$$x^2 = -\frac{2L\sin^2\beta}{\cos\beta\cos\alpha}\left(y - \frac{L}{2\cos\beta\cos\alpha}\right)$$

In figure 8 we have plotted the intersection of cones of protection for three lightning rods of lengths 0.185m (= 1/4 panel width), 0.37m (= 1/2 panel width), and 0.74m (= panel width.)

In these examples the rectenna inclination angle α is taken to be 45° and the cone of protection β is equal to 45°. The resulting intersections are parabolas for the cases depicted in Figure 8. For the parabolic solution the cone of protection is parallel to the face of the rectenna in the vertical plane bisecting the panel (The view of Figure 6 and 7 except that here $\alpha = \beta = 45^0$).

At lower latitude sites (below 40°) the rectenna inclination angle α is less than 45° and the 45° cone of protection intersection becomes an ellipse; in Figure 6 the vertical projection illustrates the intersection in the plane through the lightning rod. The elliptic solutions leave regions along the base of the rectenna unprotected. Hence, the parabolic solutions of Figure 8 and the table (Fig. 9) represent maximum protection capabilities of the cone of protection with the panel scale protection configuration. The small ellipse in Figure 11 shows the cone of protection intersection for $\alpha = 40^0$, $\beta = 45^0$, and L = 0.74m.

2.2 Lightning Rod Protection at the Bay or Billboard Scale

In this system a longer lightning rod is placed at the center (or end) of each bay or billboard making them 14.69m apart. The mathematical description here is identical to that for the panel scale system (2.1). Only sizes are different. Figure 10 illustrates the billboard scale system.

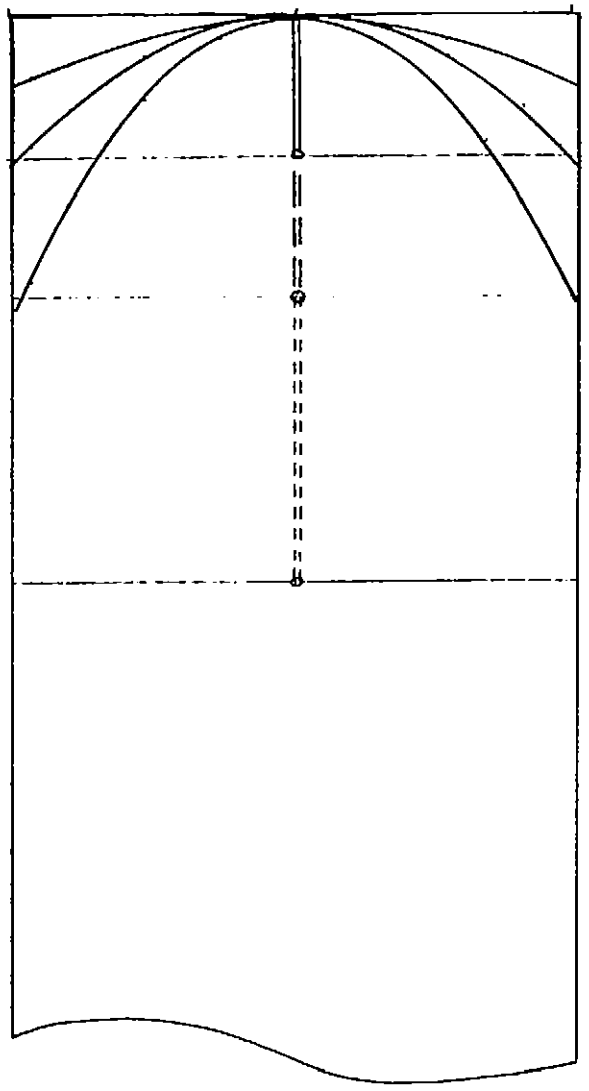


FIGURE 8

THE INTERSECTION OF THE CONE OF PROTECTION WITH A RECTENNA PANEL (THE CURVED LINES) SHOWN IN THE PLANE OF THE PANEL. LIGHTNING ROD LENGTHS = ¼, ½ AND 1 TIMES THE PANEL WIDTH ARE SHOWN PROJECTED VERTICALLY ONTO THE PANEL.

PARABOLIC TYPE SOLUTIONS

ROD LENGTH IN METERS	UNPROTECTED AREA IN %	UNPROTECTED AREA X ENHANCEMENT FACTOR
.185	1.1%	2.9%
.37	.55%	1.5%
.74	.28%	.74%

FIGURE 9

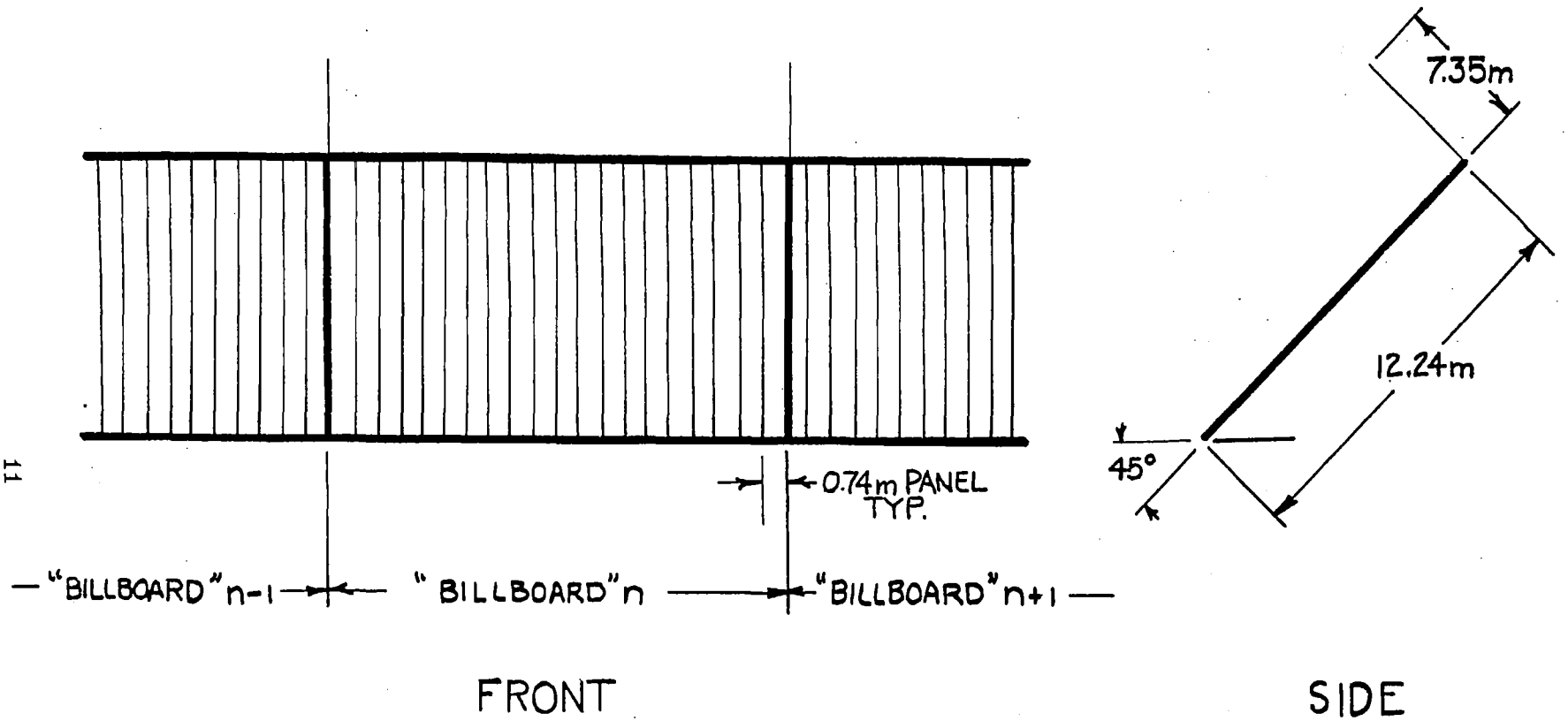


FIGURE 10

BILLBOARD SCALE LIGHTNING PROTECTION SYSTEM

To illustrate the cone of protection concept for this configuration we use as an an example, $\alpha = 40^0$, $\beta = 45^0$, and L = 7.35m (= 1/2 billboard width). The resulting intersection is a portion of an ellipse and is shown on Figure 12. Even if these long (7.35m) lightning rods were placed every 14.69m, a significant fraction of the rectenna (6.7% or when weighted by enhancement factor 18%) is unprotected (i.e. is not inside a cone of protection).

Furthermore, there are serious mechanical problems associated with supporting these long (i.e., over 22 feet) lightning rods. We think these examples are sufficient to demonstrate that configurations employing fewer lightning rods at longer spacing decreases protection and creates structural problems that ultimately will increase the total materials requirement.

For example, if we were to increase the length of the lightning rod in this configuration to the point that it could offer protection to the billboard in front of the one on which it is mounted (i.e. to the south), then with the appropriate phasing of rods between rows of billboards we could get total protection in the cone of protection context. The length of the rods would need to be 12m in order to provide this coverage.

2.3 The Distributed Lightning Protection System

The distributed lightning protection approach replaces the many lightning rods with a continuous horizontal conducting structure, as depicted in Figure 13. The region of protection now becomes the volume beneath two planes whose intersection is the horizontal protecting structure. This protection tactic is essentially the one employed by the power transmission companies. The angle between the protecting planes and vertical is variable; 45° is thought to be adequate but some designs use 30° for extra protection. This line is called the "static" by the power companies and this term is used here for convenience.

Figures 7 and 8 provide the correct geometric considerations for the distributed lightning protection if we interpret the end point of the lightning rod to be the location of the static. We note that the figures apply anywhere along the rectenna, not just in the specific locations required by the lightning rod analysis.

For consistent comparisons with the other lightning rod systems we will use $\alpha = 45^0$. Since $\alpha < 45^0$ for rectennas below 40° latitude, the top edge of the rectenna is protected by the static for any value of L, the displacement distance. If we try to use a smaller, more conservative value for β, we will run into problems in protecting the top edge of the rectenna with any system tht does not cast a radio shadow on an active rectenna surface. The design constraint that we will use to specify L will be that the southward plane of protection intersect the rectenna surface at the base. Therefore,

$$L = 12.2\text{m} \tan (45^0 - \alpha).$$

For α in the range 45° to 30°, L has the range of values 0m to 3.3m. This simple analysis ignores the protecting capability of the immediate southward row of the rectenna on the base of the row being considered. When these additional protective effects are considered we find that:

$$L = 6.1m\ (1 - \tan\ \alpha)$$

For α in the range 45^0 to 30^0, L now has the range 0m to 2.6m.

Figure 13 gives the configuration of the distributed lightning protection system for $\alpha = 30^0$, which represents the most difficult situation to protect. In this situation the static is displaced by 2.6 meters from the top edge of the rectenna; note that the 45° planes of protection provide <u>total coverage</u> of the rectenna.

We wish to emphasize that the set of horizontal statics not only provide total protection in the sense that lightning flashes are expected to hit the statics instead of the active rectenna surfaces but that this system also reduces the induced voltages and currents in the rectenna. We estimate that induced charges, currents, and potentials are reduced by 1/2 by the static protection system.

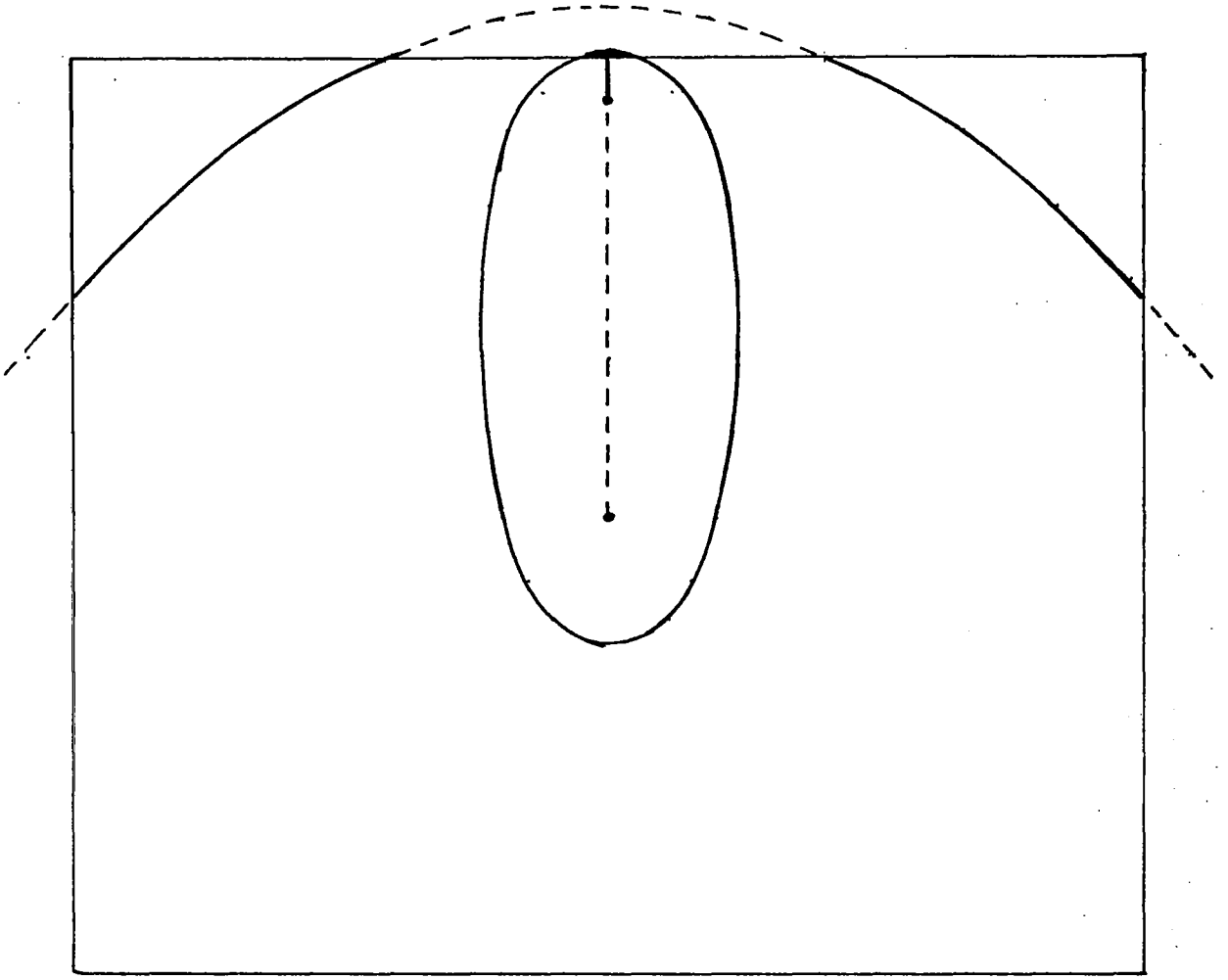


FIGURE 11

PANEL SCALE PROTECTION COMPARED TO BILLBOARD SCALE PROTECTION SHOWN AS IN FIGURE 8 EXCEPT HERE ON A BILLBOARD.

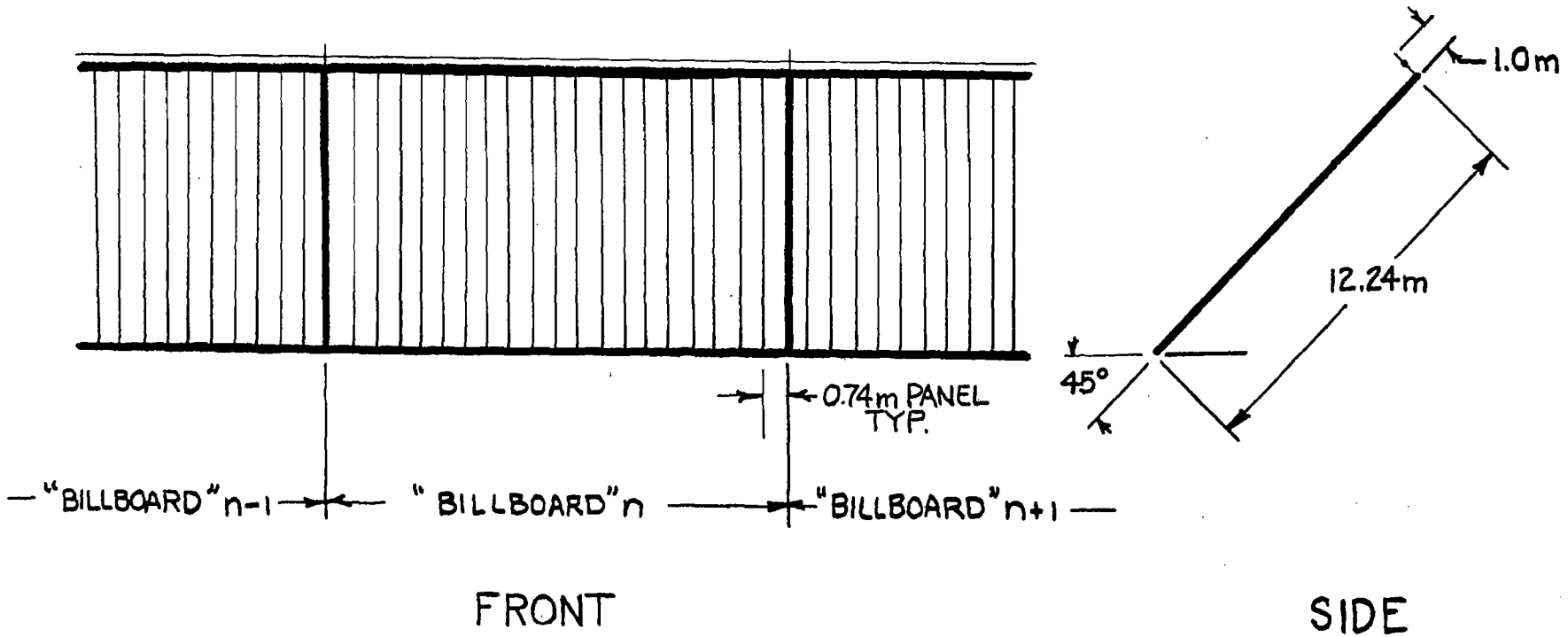


FIGURE 12

DISTRIBUTED LIGHTNING PROTECTION SYSTEM

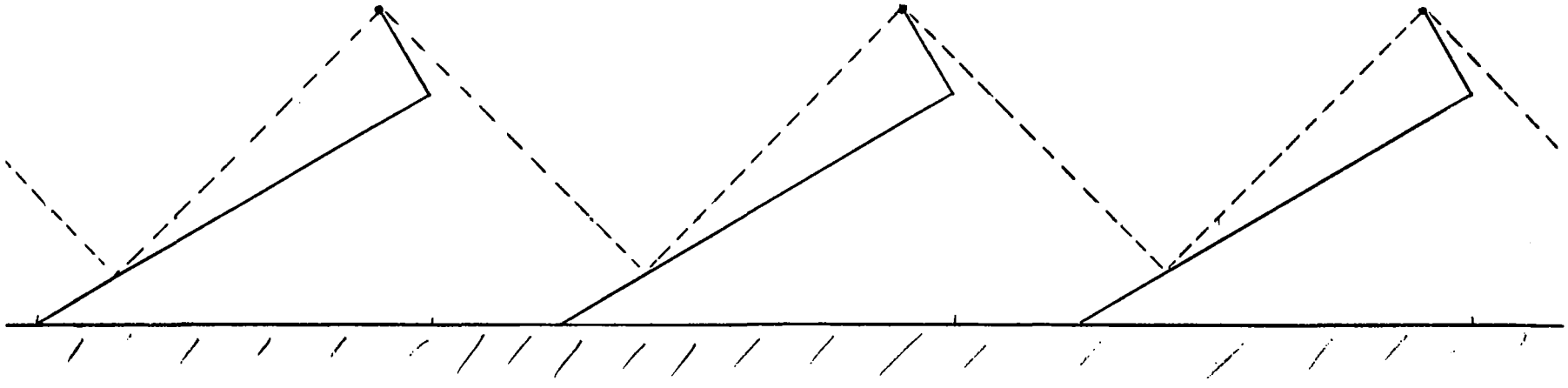


FIGURE 13

DISTRIBUTED LIGHTNING PROTECTION SYSTEM ILLUSTRATING FORWARD AND BACKWARD PROTECTION FOR SMALL INCLINATION ANGLES

II. SIMULATIONS OF LIGHTNING STRIKES TO THE SPS RECTENNA WITH AND WITHOUT PROTECTION

A series of experiments were performed in our electrostatic test chamber with a scale model of the SPS rectenna. The experiments consisted of exposing the model rectenna to a series of high voltage discharges produced with a Tesla coil.

The strikes to the rectenna were photographed using time exposures in a darkened room. A wire from the upper plate conducted the discharge to the vicinity of the model rectenna and provided us with a limited control over the area of the strike. This allowed us to keep the strikes near the volume in focus by the camera.

Different areas of the model rectenna were protected by different systems, and one area was unprotected. The following paragraphs describe samples of these experiments:

1. The Unprotected Rectenna

Most of the strikes were to the upper edge of the billboard because of the larger enhancement factor at that point. Several strikes to the billboard face occurred.

In Figure 14, we see two strikes to the unprotected billboard section, one of which is to the billboard face. Notice that these strikes are perpendicular to the face when near the face; we would anticipate this because the equipotential lines are nearly parallel to the face here.

In Figure 14, we also see for comparison the three lightning protection systems modeled. To the left is the billboard scale system; to the right is the panel scale system; and behind the flashes is the distributed lightning protection system.

2. The Panel-Scale Protection System

The next three figures are examples of strikes photographed on the section of the model rectenna that was protected by the panel-scale lightning protection system.

In Figure 15, we see two strikes on the same billboard, both of which terminate on the panel-scale lightning rods.

Figure 16 shows two strikes from a different view going to two different billboards. The panel-scale protection system here is seen to protect only the front billboard. Protection is probably greater for real lightning because in our experiments we artificially bring the "leader tip" very close to the billboard with the wire.

Multiple strikes to the panel-scale protection system are seen in Figure 18. One of the strikes goes directly to the billboard face. this type of failure will occur in nature, but with lower probability than illustrated here.

3. The Billboard-Scale Lightning Protection System.

Two sets of experiments were made with the billboard-scale lightning protection system. The one illustrated in Figure 19 corresponds to rods of length 7.35m. (A second series of strikes were made with rods cut to one-half of this length, but these were photographed in color and are not suitable for this report.) Figure 19 illustrates the capability of these long rods to direct lightning to the desired point.

In Figure 20, we have a side view of a billboard-scale protector taking a strike and protecting the billboard-face. Figure 21 illustrates the "hole in the armor" of the billboard-scale lightning protection system. Two flashes strike the protection system, but a third strikes the billboards between two protectors, as predicted in Figure 12. With real lightning this is less likely to happen, but it can and will occur.

4. The Distributed Lightning Protection System.

The displacement distance of the static from the billboard was scaled from 0.74m to make it correspond to the height of the panel-scale protection system. Fewer failures-to-protect were observed with this system but they did occur. With real lightning, they would be even less likely to occur.

In Figure 22, we see two strikes to two different billboards from the side view. Figure 23 shows two strikes to the same billboards, which were rovided with a distributed lightning protection system. One strike is to the terminal support rod at the billboard edge, which is the preferred point of strike. The other strike goes to the horizontal static line between the terminal support rods.

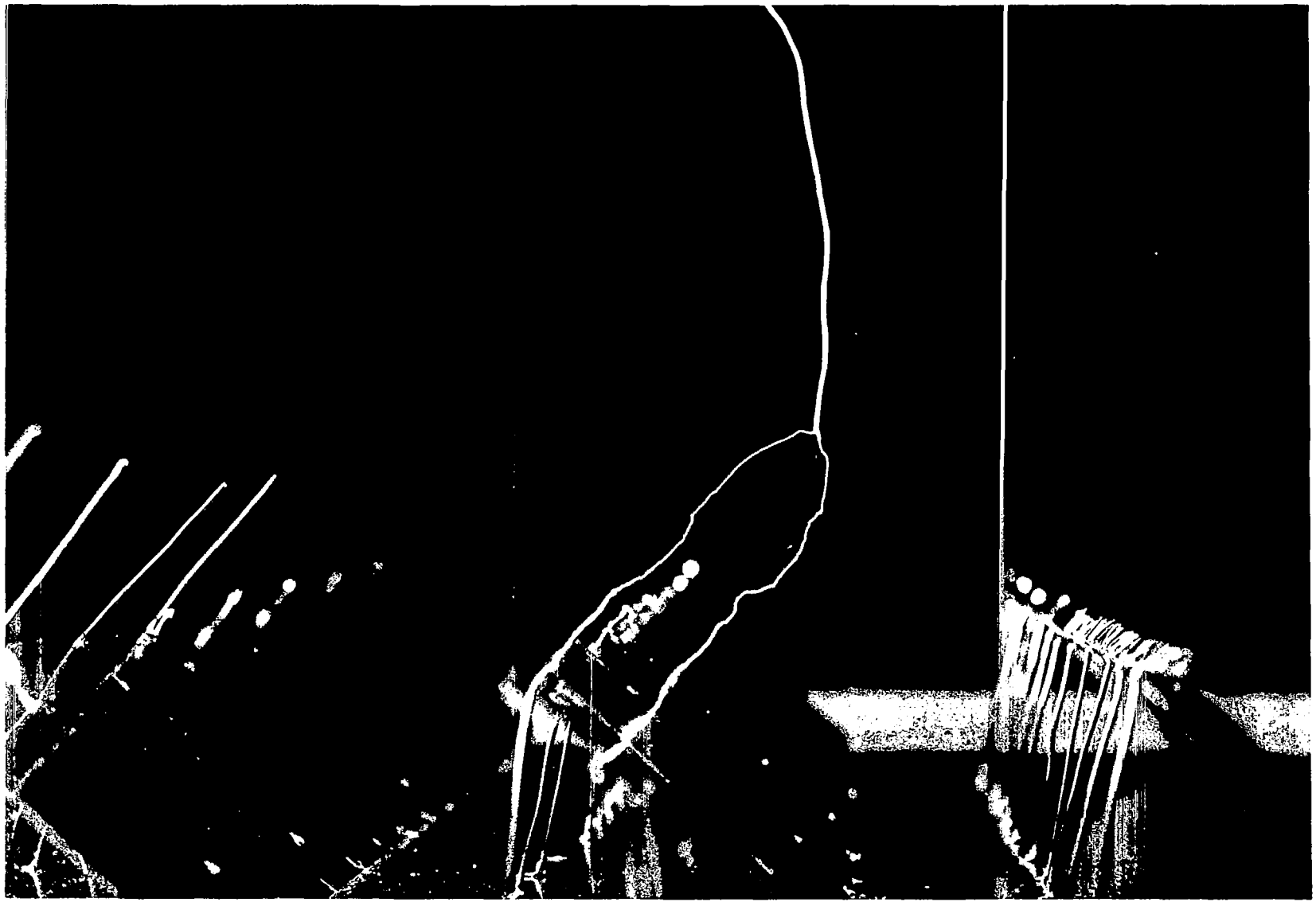


FIGURE 14

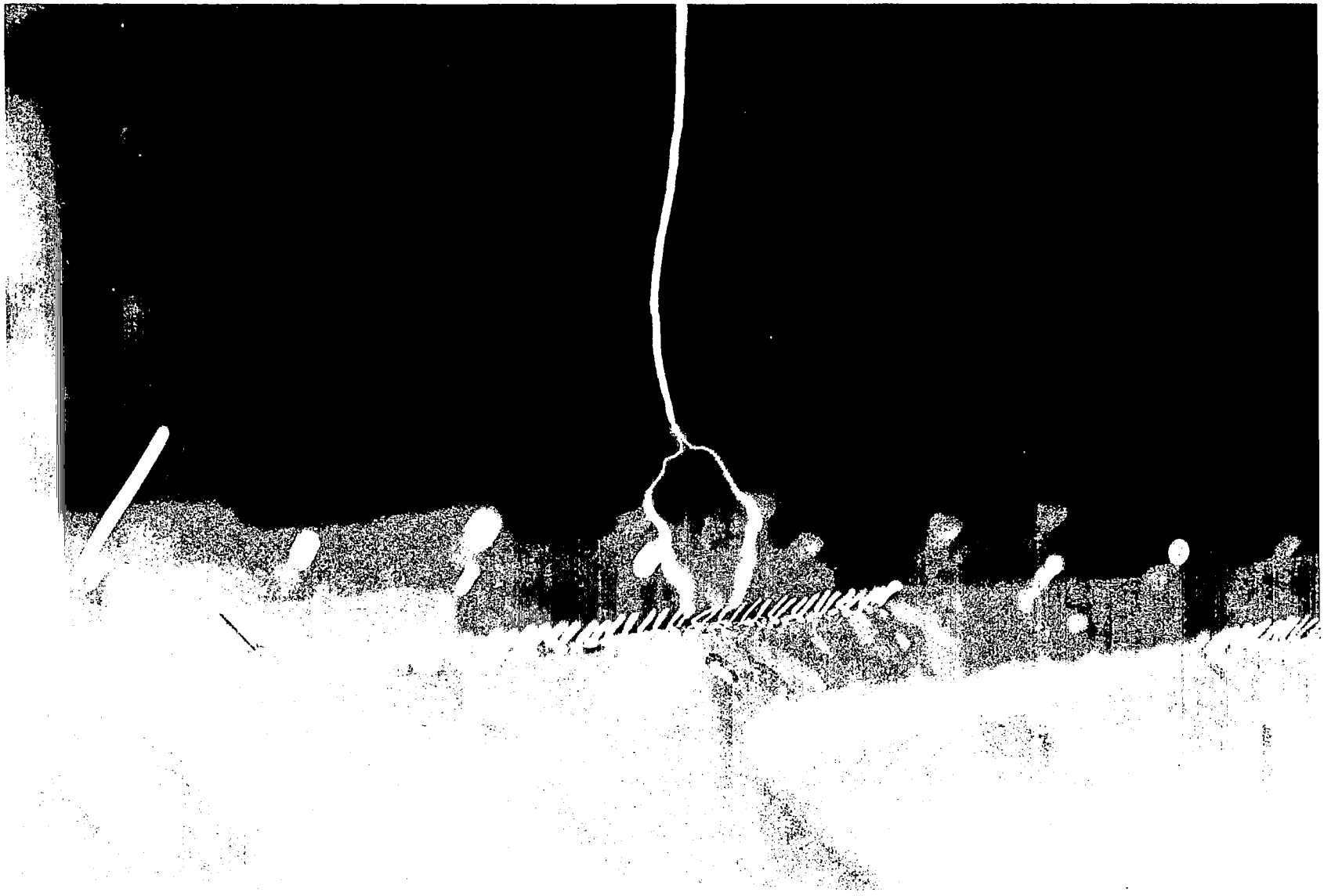


FIGURE 15

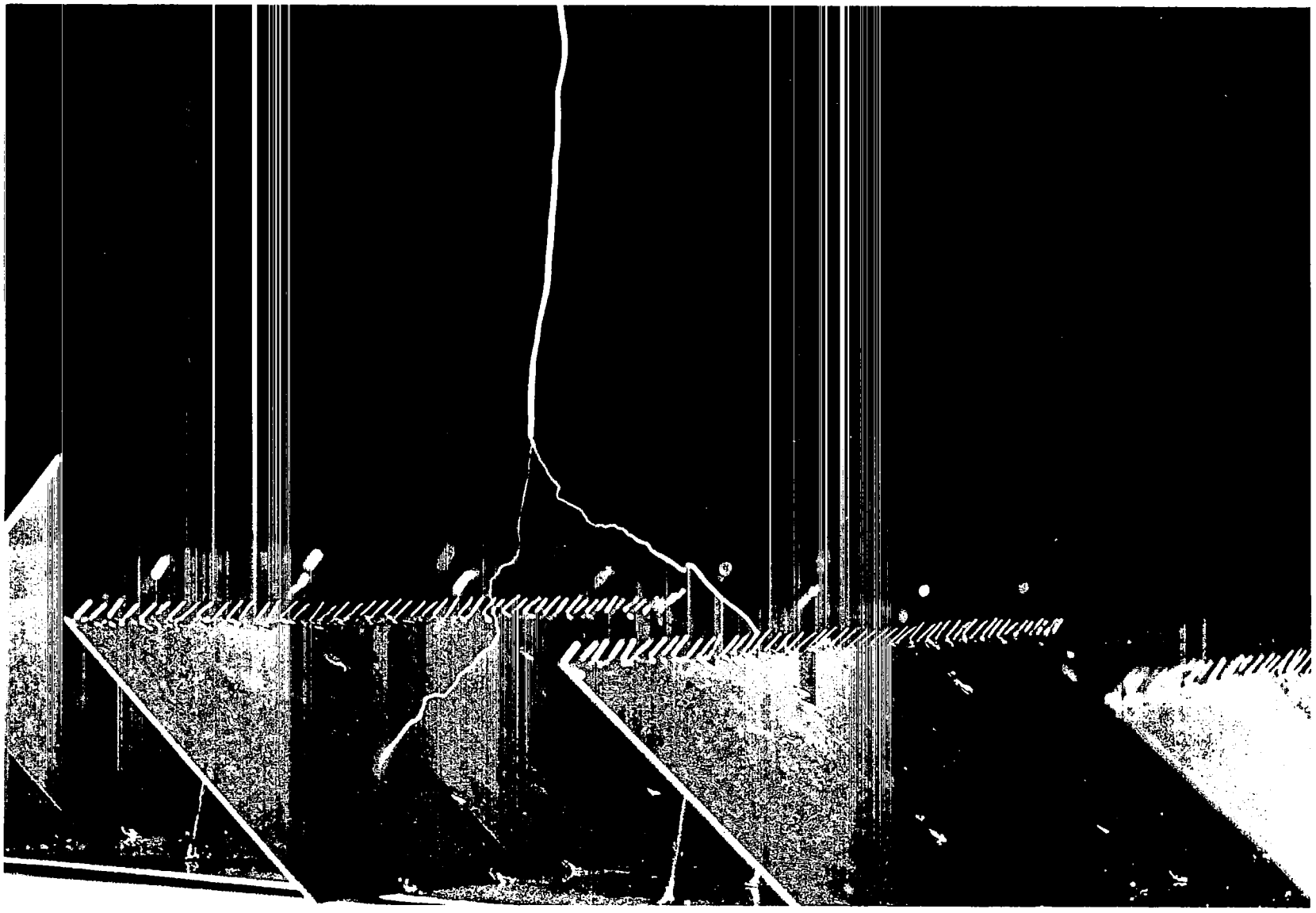


FIGURE 16

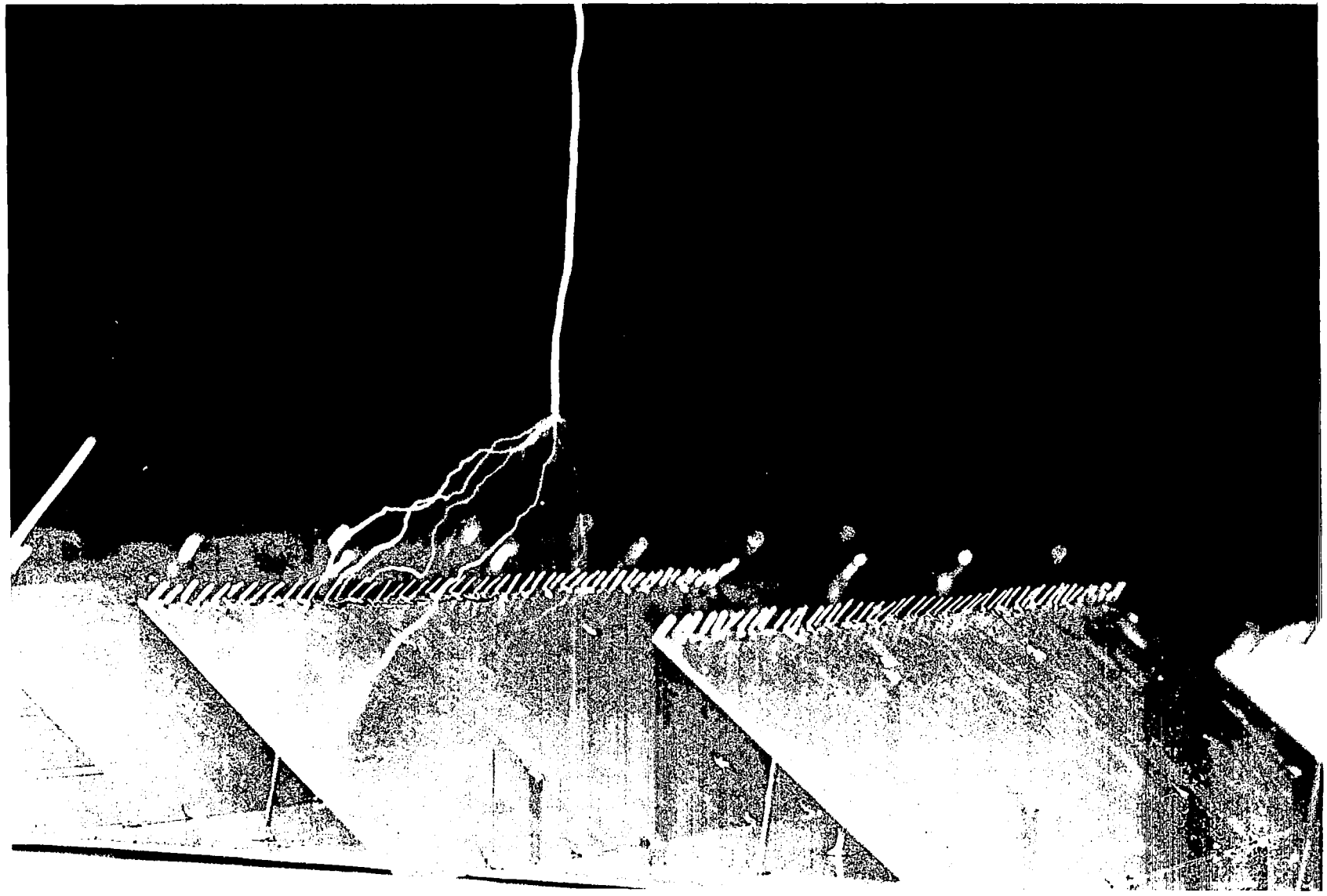


FIGURE 17

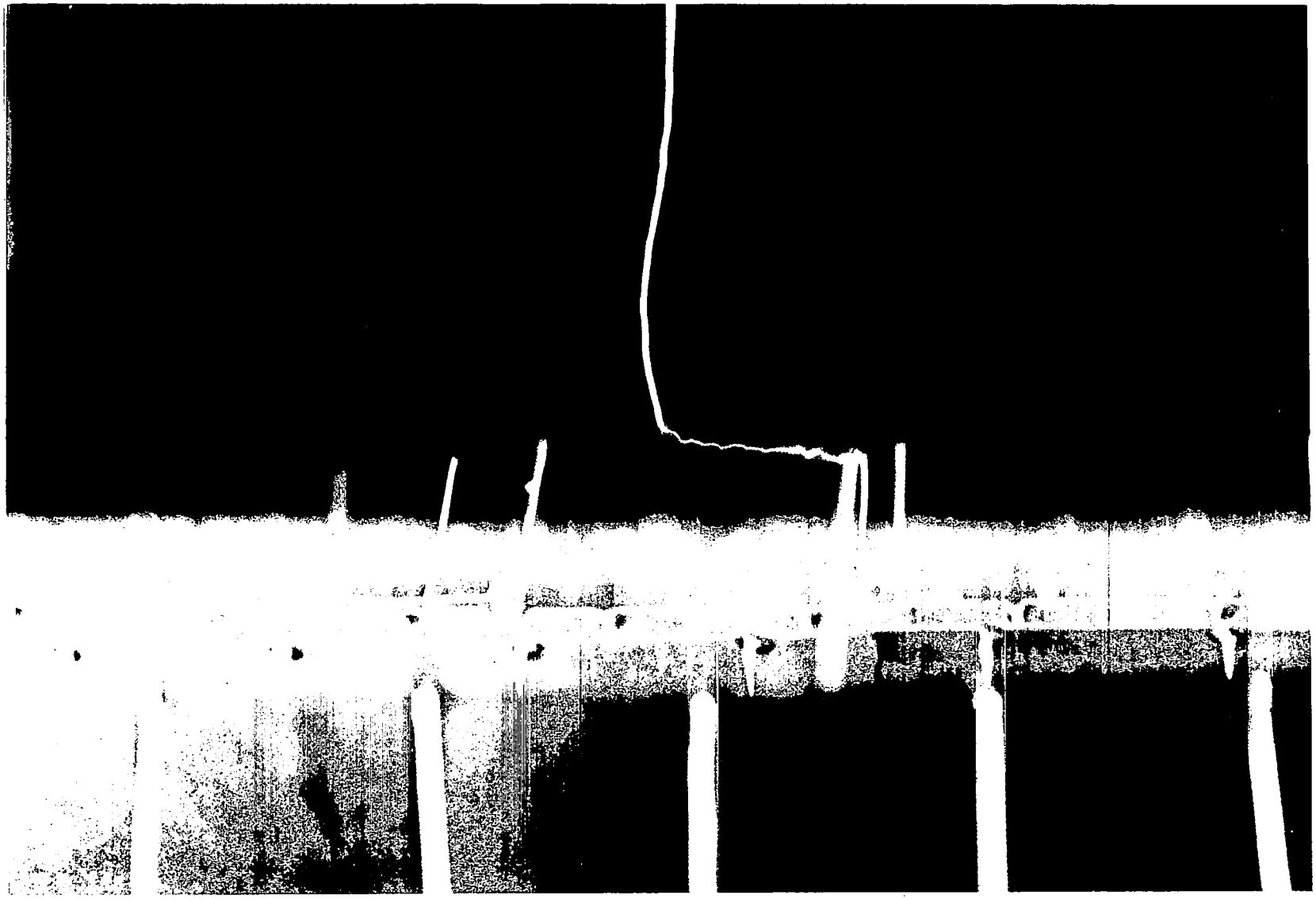


FIGURE 18

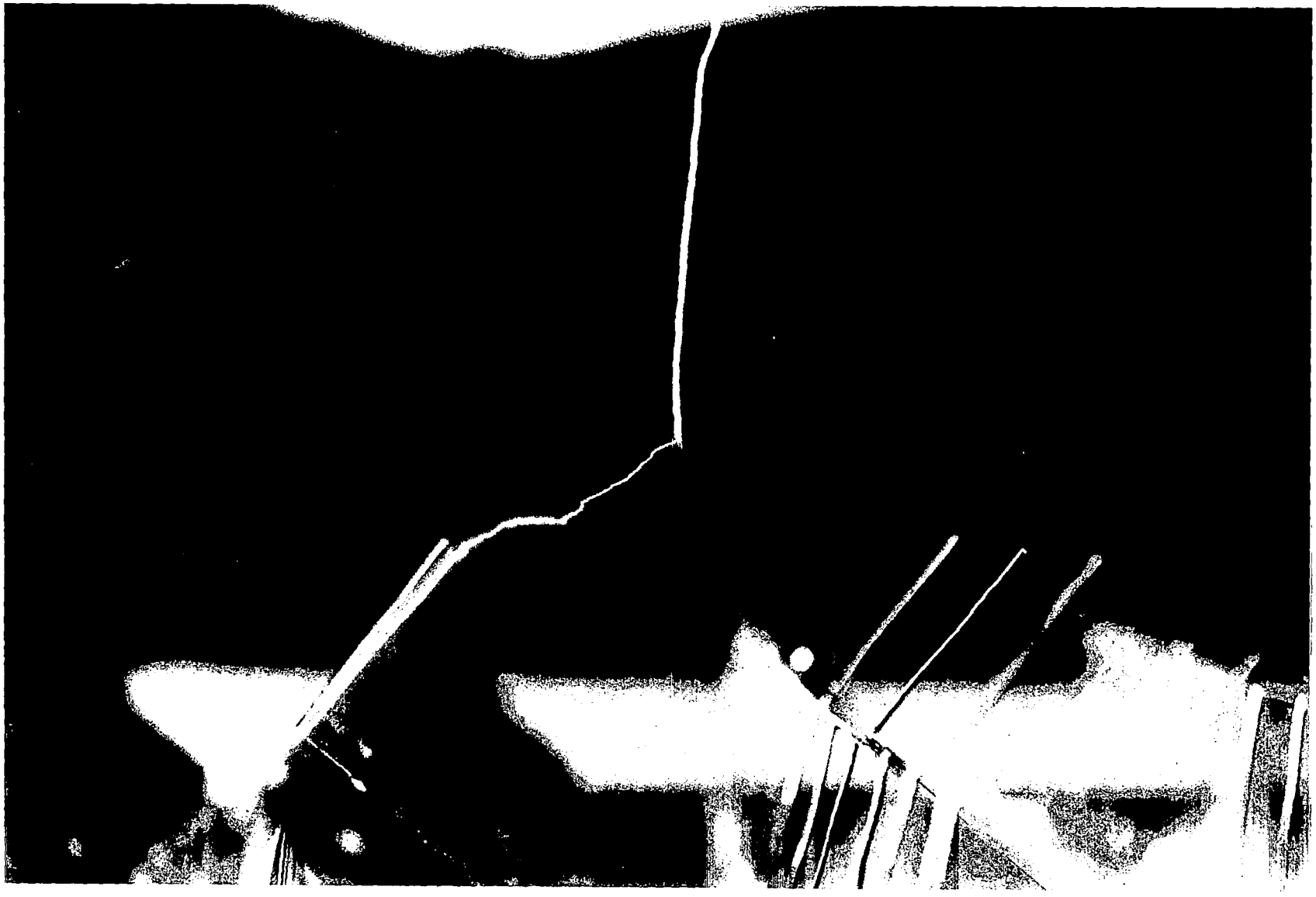


FIGURE 19

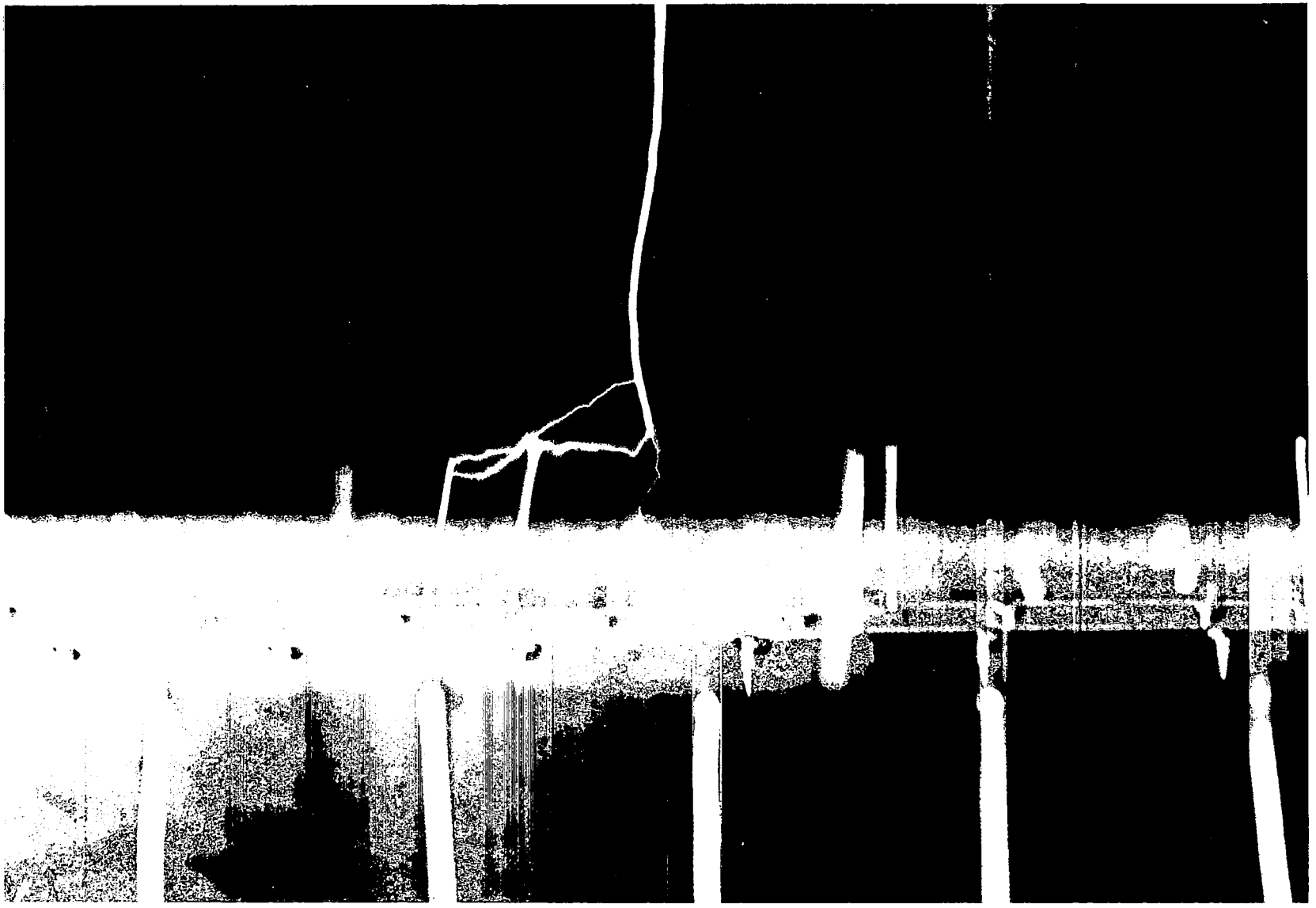


FIGURE 20

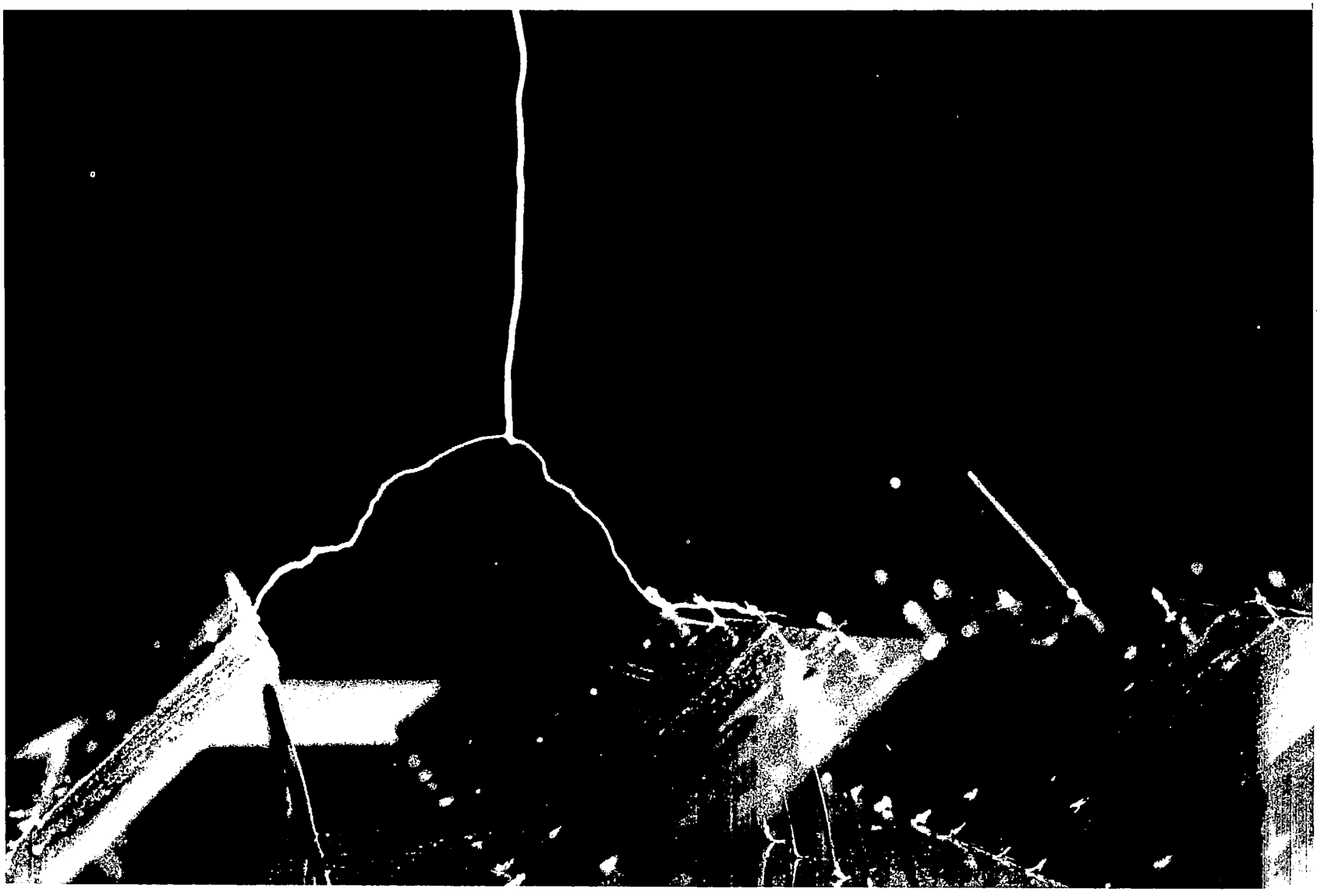


FIGURE 21

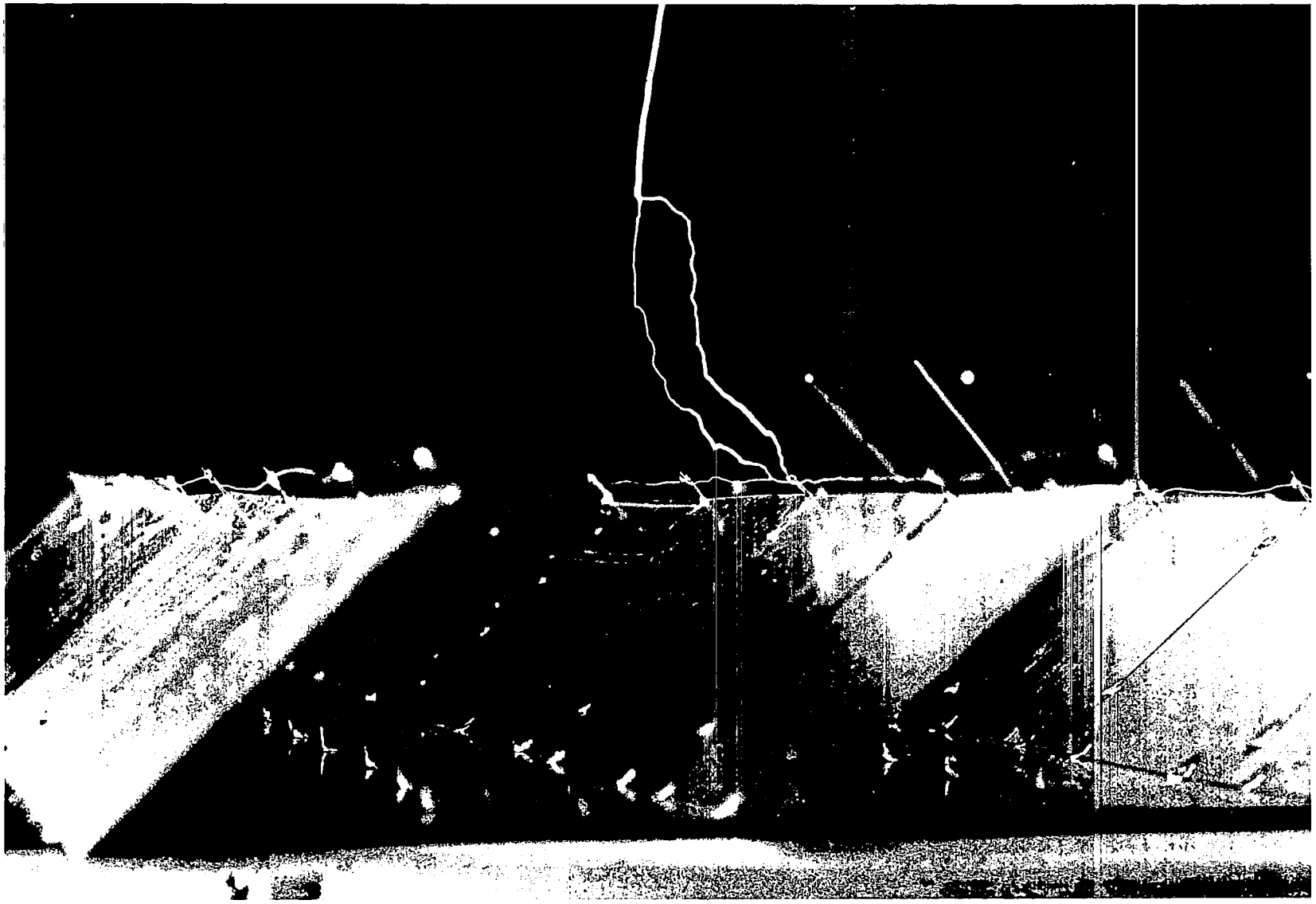


FIGURE 22

III. GROUNDING CONSIDERATIONS FOR THE PROPOSED LIGHTNING PROTECTION SYSTEM

The thundercloud charges induce a large surface charge on the rectenna below the cloud; during the stepped leader period even larger surface charges are induced on the region below the leader tip. Most of the current flowing during the return strokes of the lightning flash must be distributed by the grounding system to connect with the induced surface charges. If adequate paths for these currents are not planned and provided, the lightning will make its own paths. Most of the induced surface charge will reside on the horizontal statics of the recommended distributed lightning protection system. The primary grounding system described here is to provide low impedance paths for the redistribution of the induced surface charges and the part of the lightning charge that resides on the rectenna surface.

1. Primary East-West Grounding

It is absolutely necessary that the horizontal statics have a good low impedance connection at billboard edges. The static should appear to be a continuous very low impedance conductor in the east-west direction, as illustrated in Figure 24.

2. Primary North-South Grounding

It is also necessary that the statics are mutually grounded in the north-south directions; there are two methods of achieving this:

2.1 Periodic connections north-south at the level of the statics. If these north-south statics are aligned along the billboard edges, then there will be little power loss due to microwave shadows (See Figure 24.)

2.2 Interconnect grounding in the north-south direction at the surface or sub-surface level (see figure 25) can also be used, but this approach creates a higher impedance to north-south currents on the static system.

2.3 A surface level grounding network is required in addition to the primary static grounding network. The surface network must handle the redistribution of induced charges on the rectenna surfaces and power distribution systems and it provides a safe working environment at the surface level. East-west continuity with low impedance connections must be provided at the base of the rectenna support structures, and north-south continuity with low impedance connections as discussed in 2.2 and illustrated in Figure 25 must be provided. Figure 26 highlights the surface level grounding network.

2.4. Interconnections between the primary and surface grounding networks should be provided by the vertical conductors located at every billboard upper corner; these are the same structures on which are mounted the terminals and supports for the statics. The vertical interconnections are highlighted in Figure 27.

2.5 The ultimate or final component of the grounding system is the tie-in to Earth ground. At regular intervals in the rectenna a deep earth grounding rod must be driven into the soil to make good contact with a conducting soil for earth ground[28]

The organization of the earth grounding system should be along diagonals, as illustrated in Figure 28. Here we see that the placement of earth ground at every fourth billboard but on a diagonal produces a grid such that lightning striking the primary grounding network will never have to travel more than 30 meters along the east-west conductors before finding a ground, or 32 meters along the north-south conductors (for a rectenna with a 40° inclination angle).

THE PRIMARY GROUNDING SYSTEM AT THE STATIC LEVEL

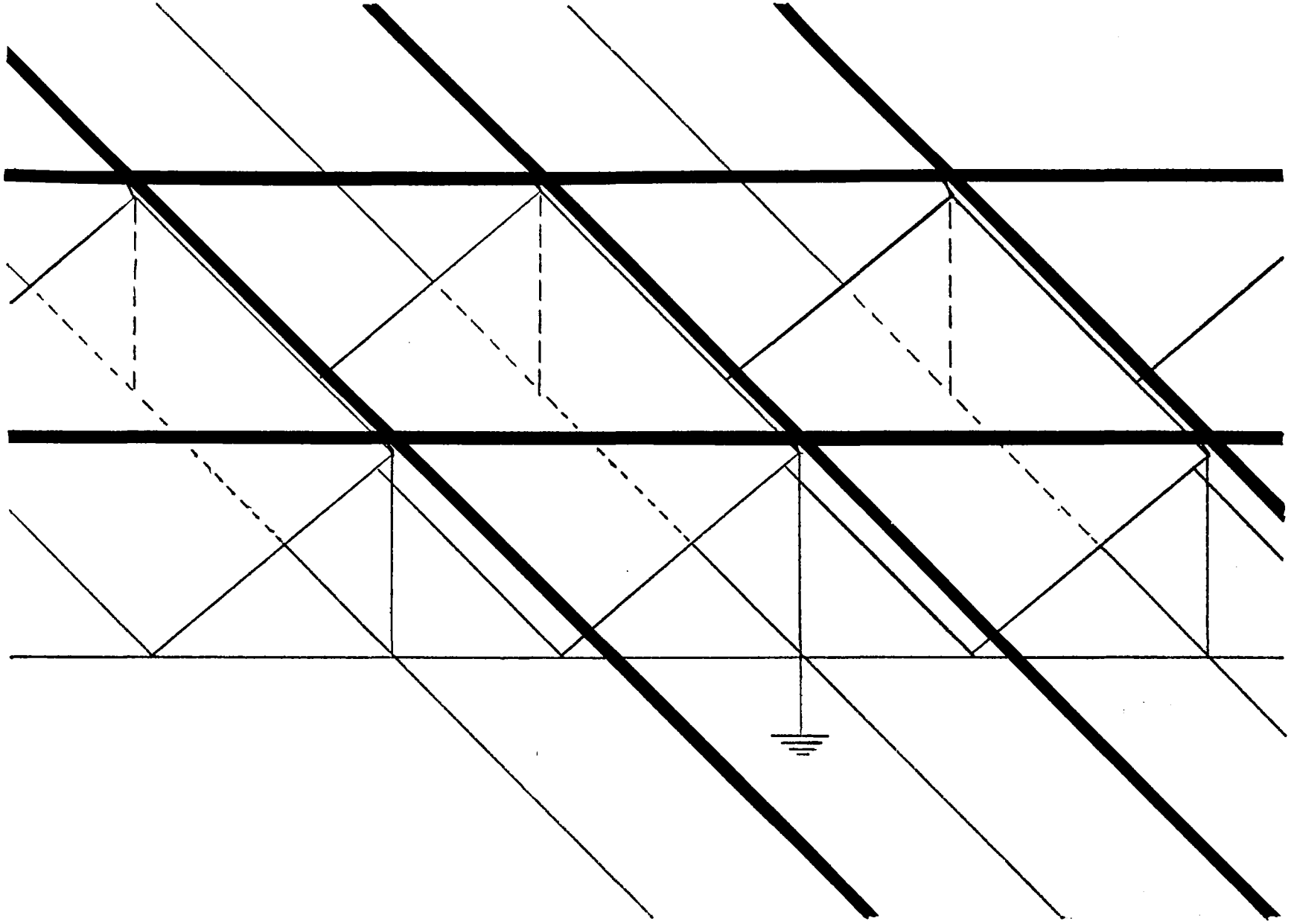


FIGURE 24

GROUNDING
RECTENNA LIGHTNING ROD SYSTEM

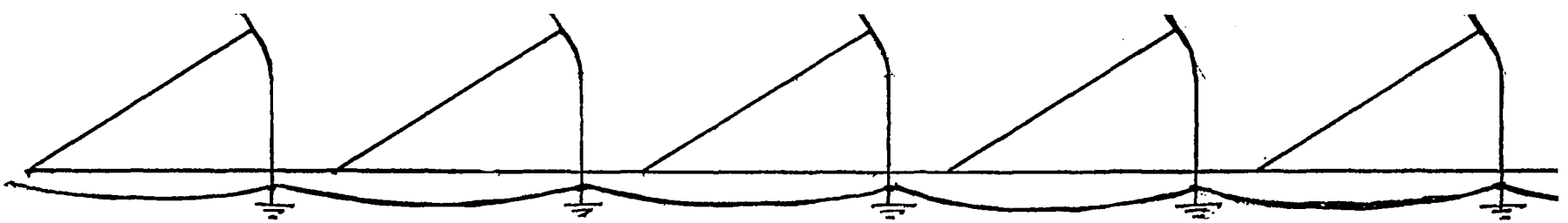


FIGURE 25

THE SURFACE-LEVEL GROUNDING NETWORK

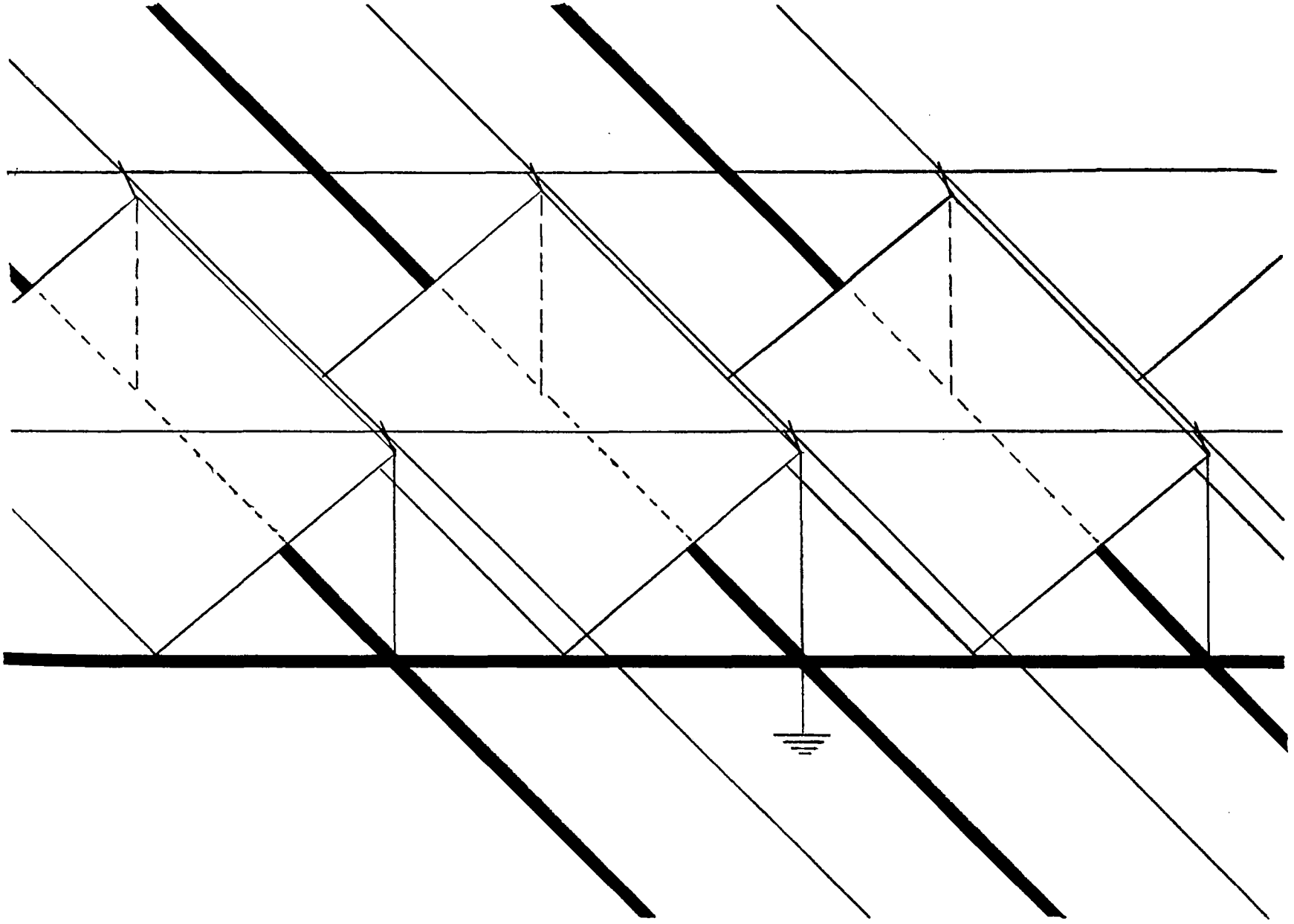


FIGURE 26

VERTICAL INTERCONNECTIONS BETWEEN PRIMARY AND SURFACE NETWORKS AND ON EARTH GROUND

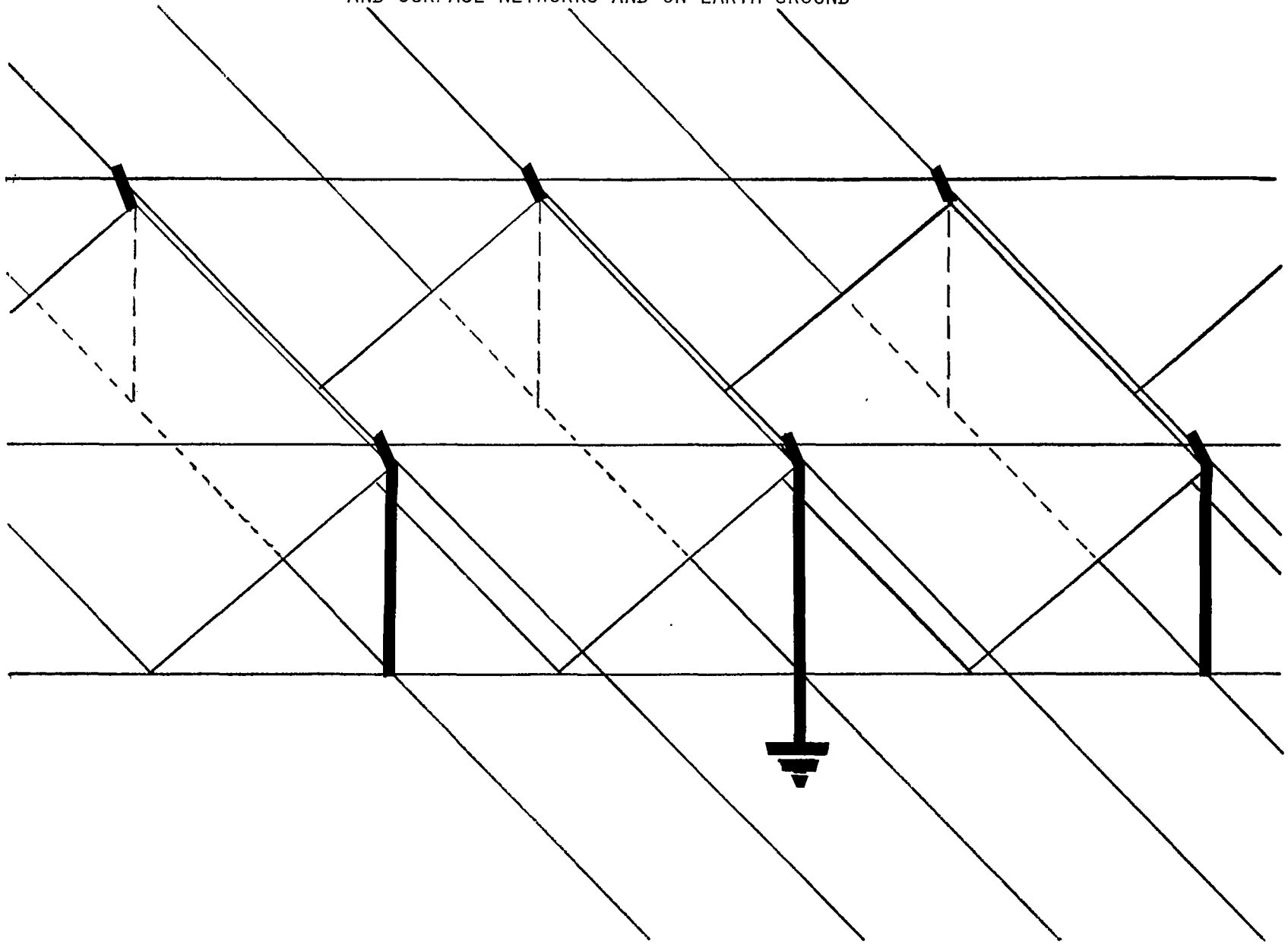


FIGURE 27

PLACEMENT OF EARTH GROUNDS

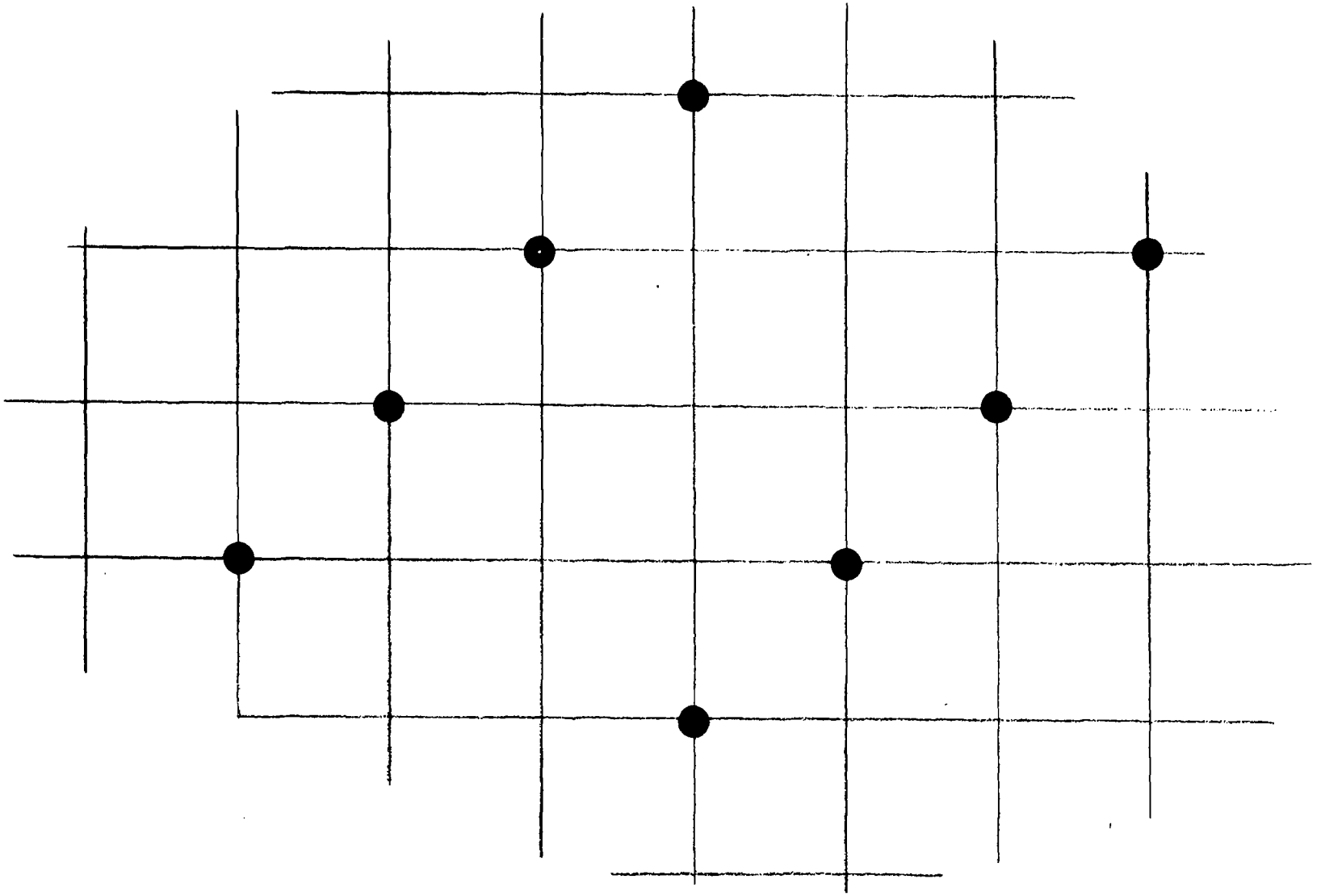


FIGURE 28

IV. MATERIALS AND SPECIFICATIONS FOR LIGHTNING PROTECTION

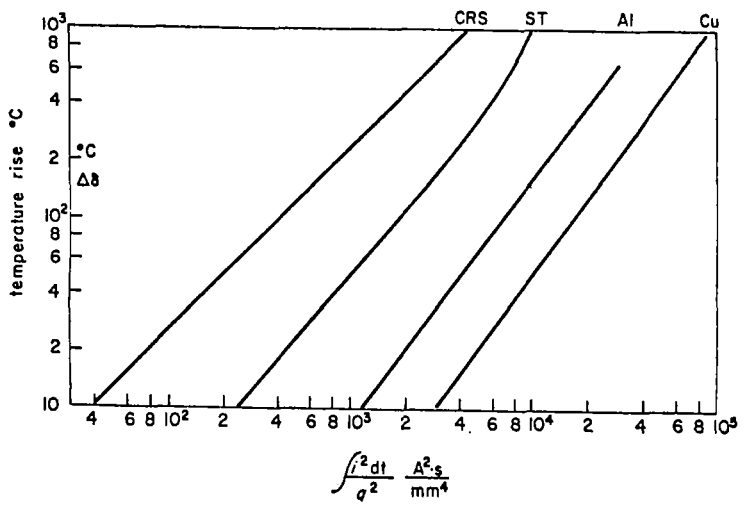
It is premature to specify the final form for the materials for the lightning protection system. We think that the system should be integrated into the structural design of the rectenna itself; in this case many other considerations are necessary in addition to the capability to conduct lightning currents. The data displayed in Figure 29 (H. Baatz, Protection of Structures, in Lightning Vol. 2, ed. by R.H. Golde) is useful for order-of-magnitude estimates of the lightning current requirements.

Example: If the design permits a 100° C temperature rise in an aluminum member carrying 10^5 Amps for 10^5 seconds, we need approximately 3 mm^2 crossectional area of aluminum material in the conductor. Note that the recommended crossections for building codes are larger (~ 80 mm^2) indicating designs for lower temperature operation plus safety margins.

The lightning conductor need not be solid. From a structural point of view a tubular or other extruded shape would be preferable. Such configurations are compatible also with the lightning protection recommendations.

Specific values of materials for wire

Material	Steel	Copper	Aluminium
Density (g/cm^{-3})	7·7	8·92	2·7
Electrical resistance ($\Omega\ mm^{-2}\ m^{-1}$)	0·17	0·0178	0·029
Heat ($cal\ °C^{-1}\ g^{-1}$)	0·115	0·093	0·023
Melting point (°C)	1,350	1,083	658



Temperature rise of conductors as function of current square impulse per cross-section square; Cu = copper, Al = aluminium, ST = steel, CRS = corrosion-resistant steel.

Cross-section for lightning conductors

Installation components	Material	Cross-section (mm^2)	Dimension: Rod (mm, radius)	Dimension: Strip (mm × mm)
Air termination	Steel, galvanized	50 (25)[a]	8	20 × 2·5
Rods up to 0·5 m long	Steel, stainless	110	12	30 × 3·5
Down conductors	Copper	50 (16)[a]	8	20 × 2·5
Conductors in ground	Aluminium[b]	80 (25)[a]	10	20 × 4
Sheet metal	Steel, galvanized			0·5 mm
	Copper			0·3 mm
	Aluminium, Zinc			0·7 mm
	Lead			2.0 mm

[a] Lowest cross-sections used in some countries.
[b] Not for use below ground.

FIGURE 29

V. ESTIMATE OF POWER LOSS FROM THE BEAM

A rough maximum estimate of the power loss from the microwave beam due to the lightning protection devices can be obtained by assuming that the microwave shadow cast by the static lightning protection system is twice the crossectional area of the devices. We assume that the conductors are 2 cm wide of 1 mm thickness tubular material, providing 60 mm^2 of crossectional area for conducting. The assumed shadow of these structures is approximately 0.6% of the rectenna area (see Figure 30.). This is a maximum estimate of the loss.

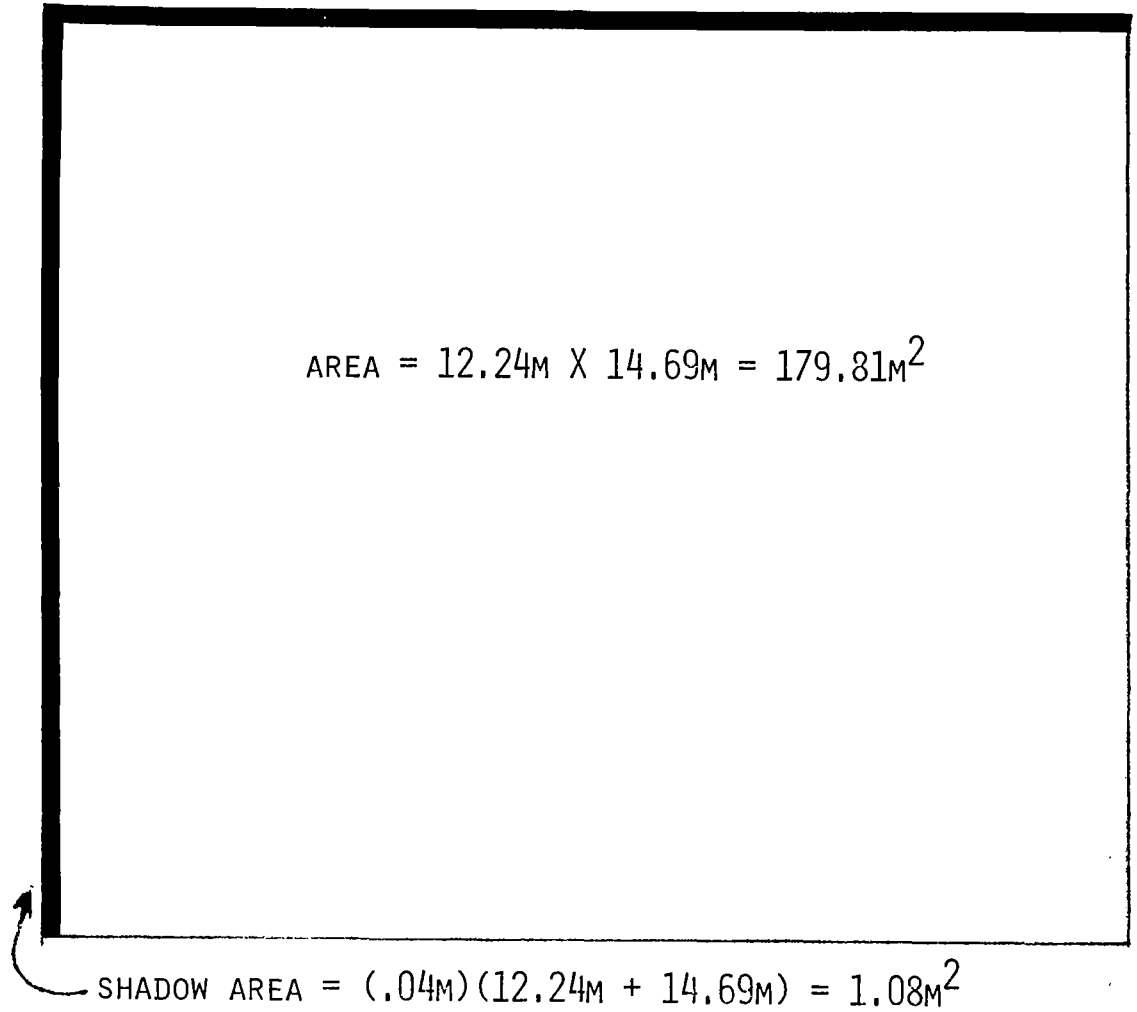

AREA = 12.24M X 14.69M = 179.81M^2
SHADOW AREA = (.04M)(12.24M + 14.69M) = 1.08M^2

FIGURE 30

VI. MICROWAVE DIODE FAILURES DUE TO INDUCED CURRENT TRANSIENTS

The 25 W S GaAs diodes used in the design of the SPS rectenna have not been produced and no failure data is available for these devices. In order to obtain estimates of failure power of the diodes in the design, we used the specification data for the HP5082-2824 microwave diode and scaled the characteristics to 25 W using the."Wunsch relationship" described in the references below. We also obtained advice directly from Dr. D.C. Wunsch regarding the extrapolated power failure current.

1. Defense Department Report D224-13042-1 EMP, Susceptibility of Semiconductor Components, dated September, 1974.

2. Defense Department Report D224-10022-1 EMP, Electronic Analysis Handbook, dated May, 1973.

3. Defense Department Report D224-10019-1 EMP, Electronic Design Handbook, dated April, 1973.

Figure 31 shows the predicted failure power for 25 watt diodes, as a function of pulse width.

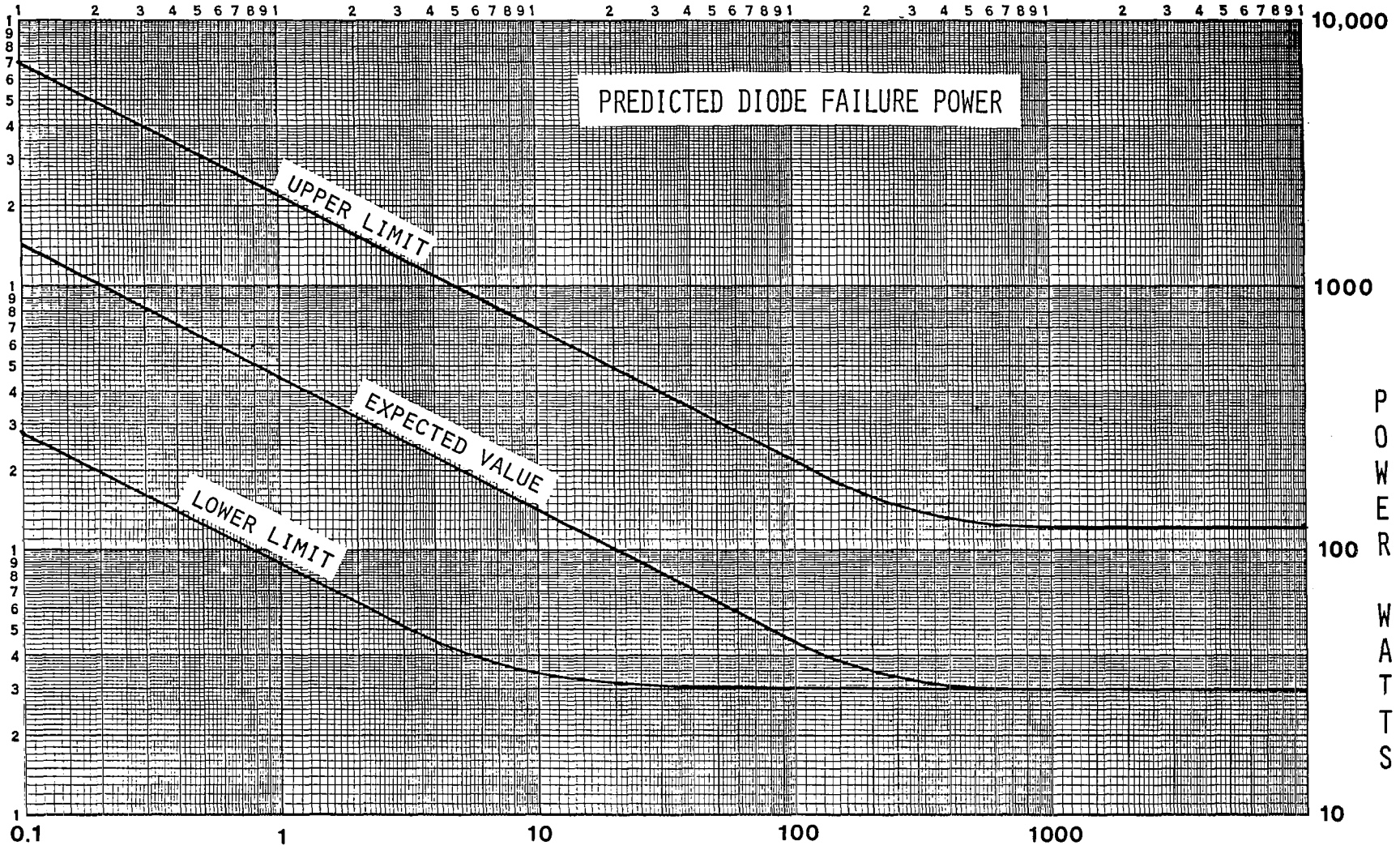

PREDICTED DIODE FAILURE POWER
UPPER LIMIT
EXPECTED VALUE
LOWER LIMIT
10,000
1000
100
10
POWER WATTS
0.1
1
10
100
1000
PULSE WIDTH - MICROSECONDS

FIGURE 31

VII. COMPUTER SIMULATION OF ELECTROSTATIC FIELD AROUND AN SPS RECTENNA

The electrostatic fields produced by the charges on the lightning channel induce charges on the rectenna and on the lightning protection conductors. Changes in this electrostatic field require a redistribution of charge on the rectenna system; the resulting currents can cause diode failure even with a lightning grounding system in place. One output of the computer simulation of the electrostatic field around the SPS rectenna is an evaluation of the induced current on the rectenna with and without the recommended lightning protection equipment.

An additional output from the computer simulation is the potential around the rectenna billboard enabling us to estimate the enhancement factors of the electric field due to the billboard shape.

The algorithm used in the simulation computes an array of values for the potential around the middle of five infinitely long billboards. We assume here that the contribution to the local potential from billboards further away is ignorably small. The surface charge distribution on the billboards is simulated with ten infinitely long line charges evenly spaced along the billboard. The value for the line charges is determined interactively with the computer to produce a zero potential contour that has the same shape as the billboard. Figure 32 illustrates this simulation.

In order to compute the potential, we will need U(x,y), the electrostatic potential at a point (x,y) in free space, where the coordinate system is such that the line of electrical charges giving rise to the potential is located at the origin. If we call the y-coordinate the height h, then U(x,H) is the electrostatic potential at x and h of a line charge λ (coulomb/meter) at a height d directly above the point x = 0. There is also a contribution to U from the image charge. Thus,

$$U(x,h) = -\frac{\lambda}{2\pi\varepsilon_0} \ln \left[\frac{x^2 + (h-d)^2}{x^2 + (H+d)^2}\right]^{1/2} .$$

From this, the potential distribution around the rectenna may be calculated. Let U(1,h) be the potential at x = 1 and y = h due to a periodic system of line charges simulating the rectenna (see Figure 31.) We then have that

$$U(1,h) = \sum_{i=1}^{N} \sum_{j=1}^{M} \left(-\frac{\lambda j}{2\pi\varepsilon_0}\right) \ln \left[\frac{(1 - L[i-1] - X_j)^2 + (h - sX_d)^2}{(1 - L[i-1] - X_j)^2 + (h + sX_j)^2}\right]^{1/2},$$

where the free-space value for the dielectric constant is assumed and where

i = Billboard number,
j = Line charge number on billboard i,
s = Slope of billboard (= tan α),
M = Number of line charges (= 10),
N = Number of billboards (= 5).

SIMULATION OF SPS RECTENNA WITH LINE CHARGES

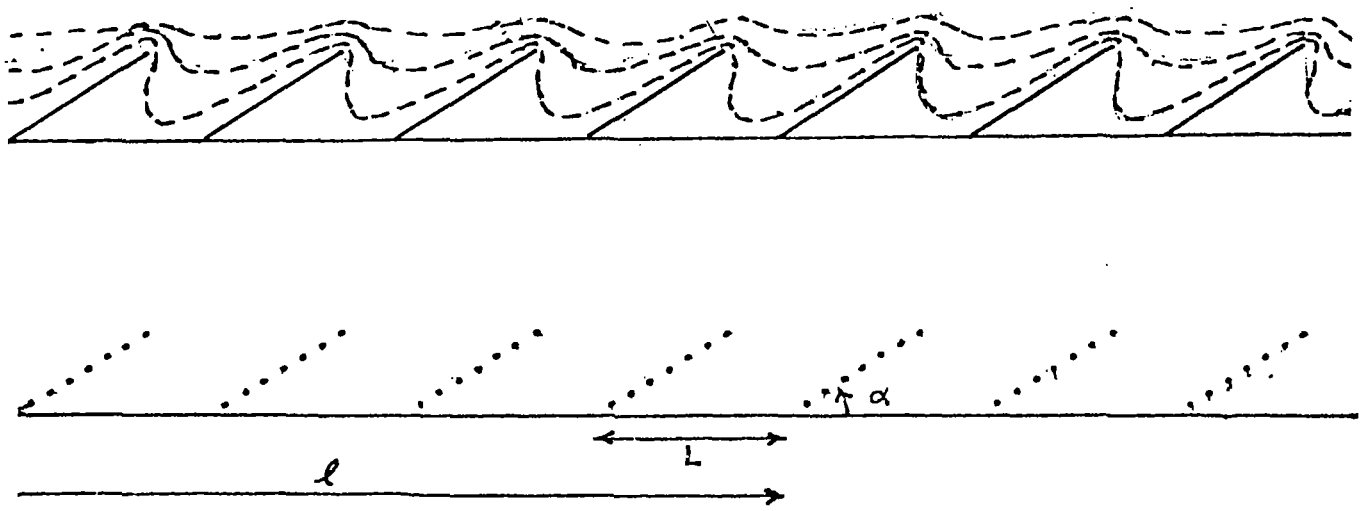


FIGURE 32

In the presence of a uniform electric field of 100,000 volts/meter (directed upward), ten line charges have been selected to produce the array of values shown in Figure 33. Three potential contours have been sketched (zero, 10,000 V, and 100,000 V) around the ten line charges on the billboard. The zero contour follows closely the position of the billboard surface, as required by the simulation algorithm. Note how closely spaced the contours are at the top edge of the billboard. Electric field enhancement factors of at least 6.5 exist in this region based upon our simulations. Higher resolution simulations would be required to refine the enhancement factor estimates.

The values obtained for the 10 individual line charges found for the solution shown in Figure 33 are (in μ Coul./m):

0.36, 0.465, 0.572, 0.679, 0.924, 1.02, 1.14, 1.78, 2.91, 4.14.

We can convert these to a surface charge density by dividing each value by the billboard distance represented by the line charge. The first line charge serves approximately 3/2 $(\frac{12.24\ m}{10})$; the last line charge serves 1/2 $(\frac{12.24\ m}{10})$; and all others are associated with a length $(\frac{12.24\ m}{10})$. Figure 34 is a plot of charge/unit area (μ Coul./m^2) on the billboard as a function of length (northward) along the billboard surface.

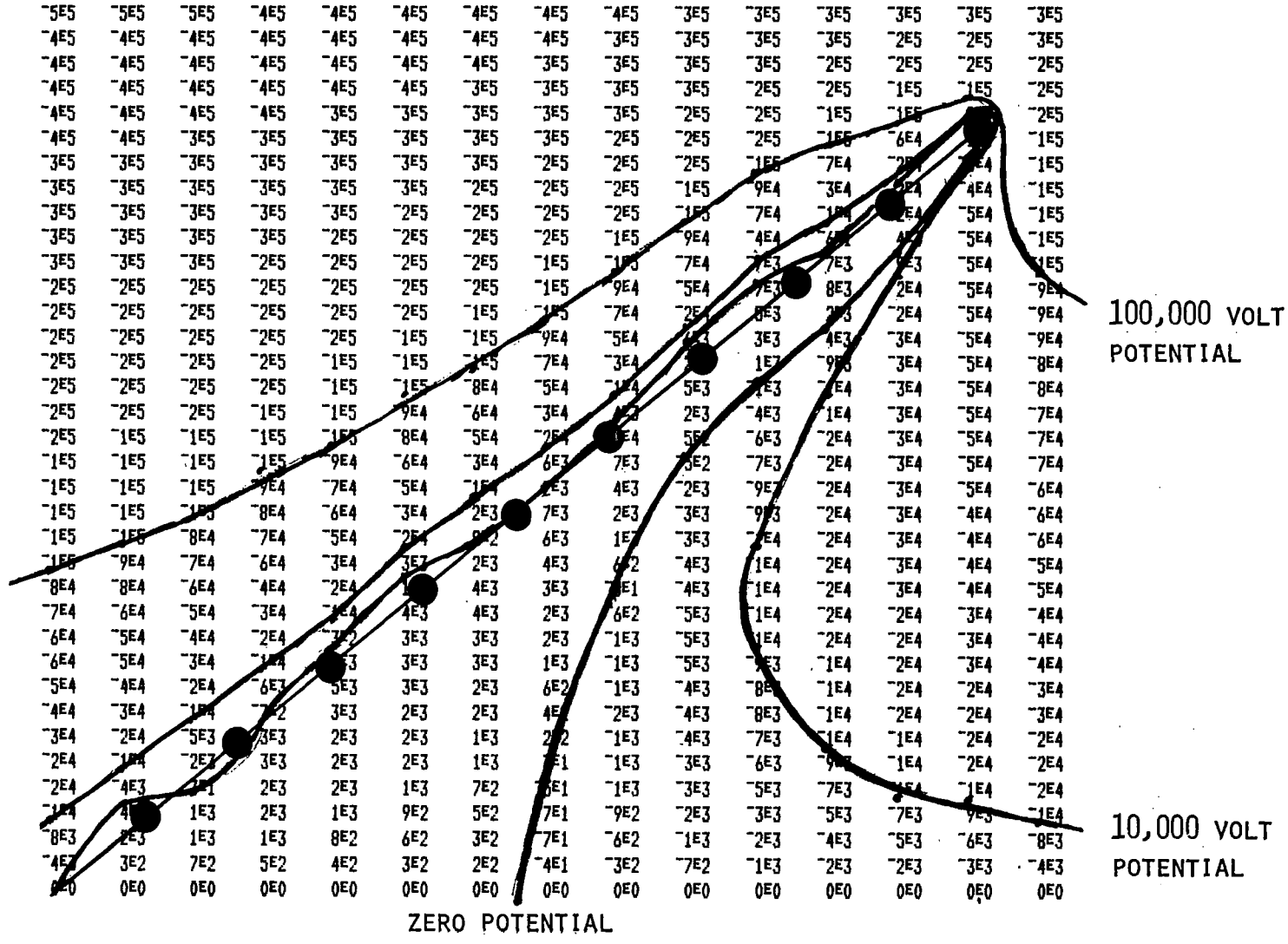
When an additional line charge in placed at the position of the lightning static, and all of line charge values are adjusted to the new configuration, we find the simulated potential function around a protected billboard - Figure 35. The placement of the static in this example is based upon the discussion in Section I.2.3., with L =0.98m, corresponding to $\alpha = 40^0$. The charge/unit length for the static is 4.6 μ Coul./m. The charge/unit lengths for the ten billboard line charges in (μ Coul./m) are:

0.315, 0.47, 0.51, 0.57, 0.87, 0.89, 0.90, 1.35, 1.78, 2.1.

These line charges may be compared with the unprotected billboard charges corresponding to the solutions of Figure 35. The protected billboard charges approach approximately one-half of the corresponding unprotected charges.

The line charges used to simulate the rectenna are normalized to a charge/unit area through division by the associated lengths, as previously described, to obtain the induced charge distribution on the protected rectenna billboard.

Figure 36 is a plot of charge/unit area in μCoul./m^2 as a function of the distance (northward) along the billboard face.



● LOCATION OF LINE CHARGES SIMULATING BILLBOARD

FIGURE 33

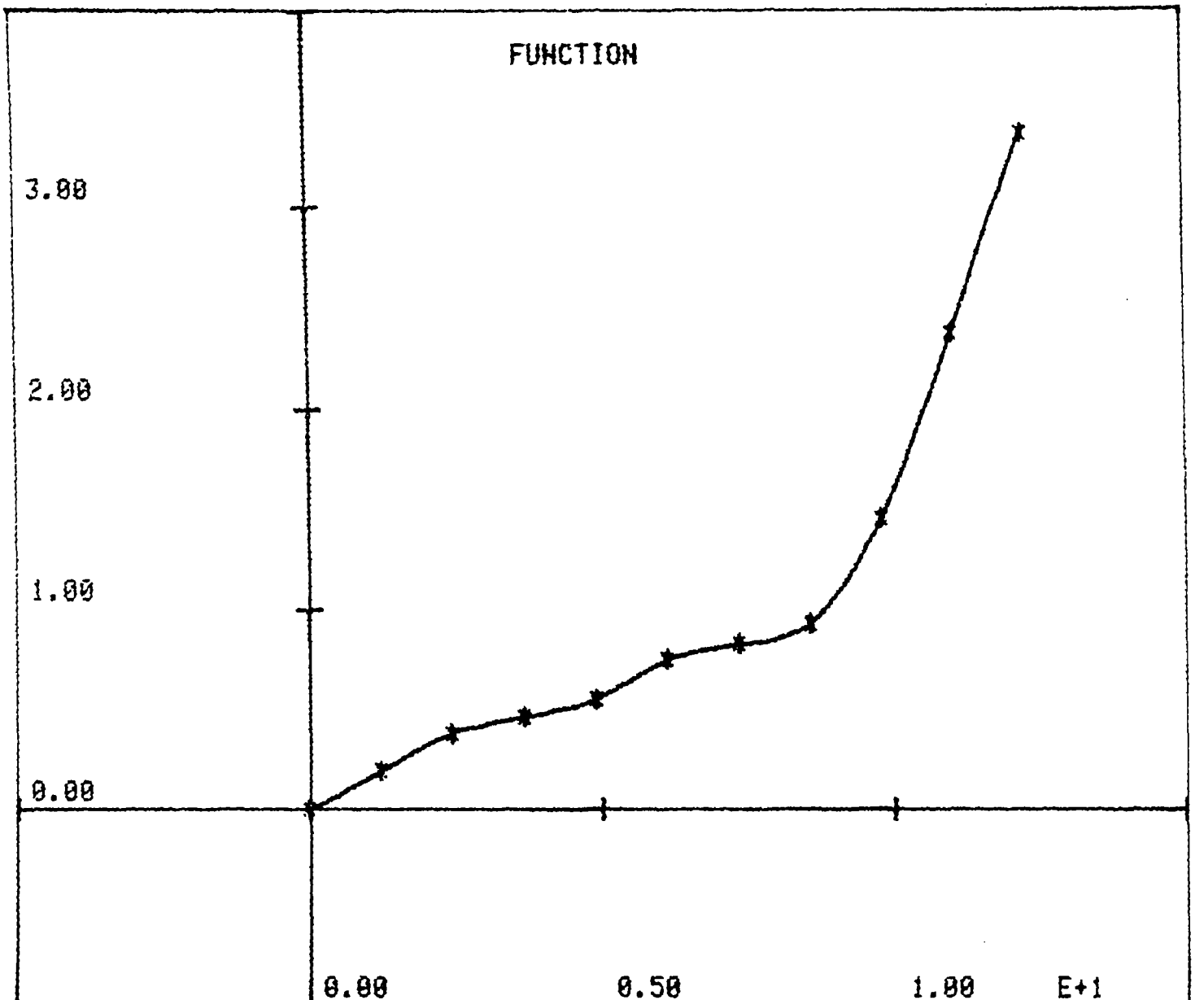
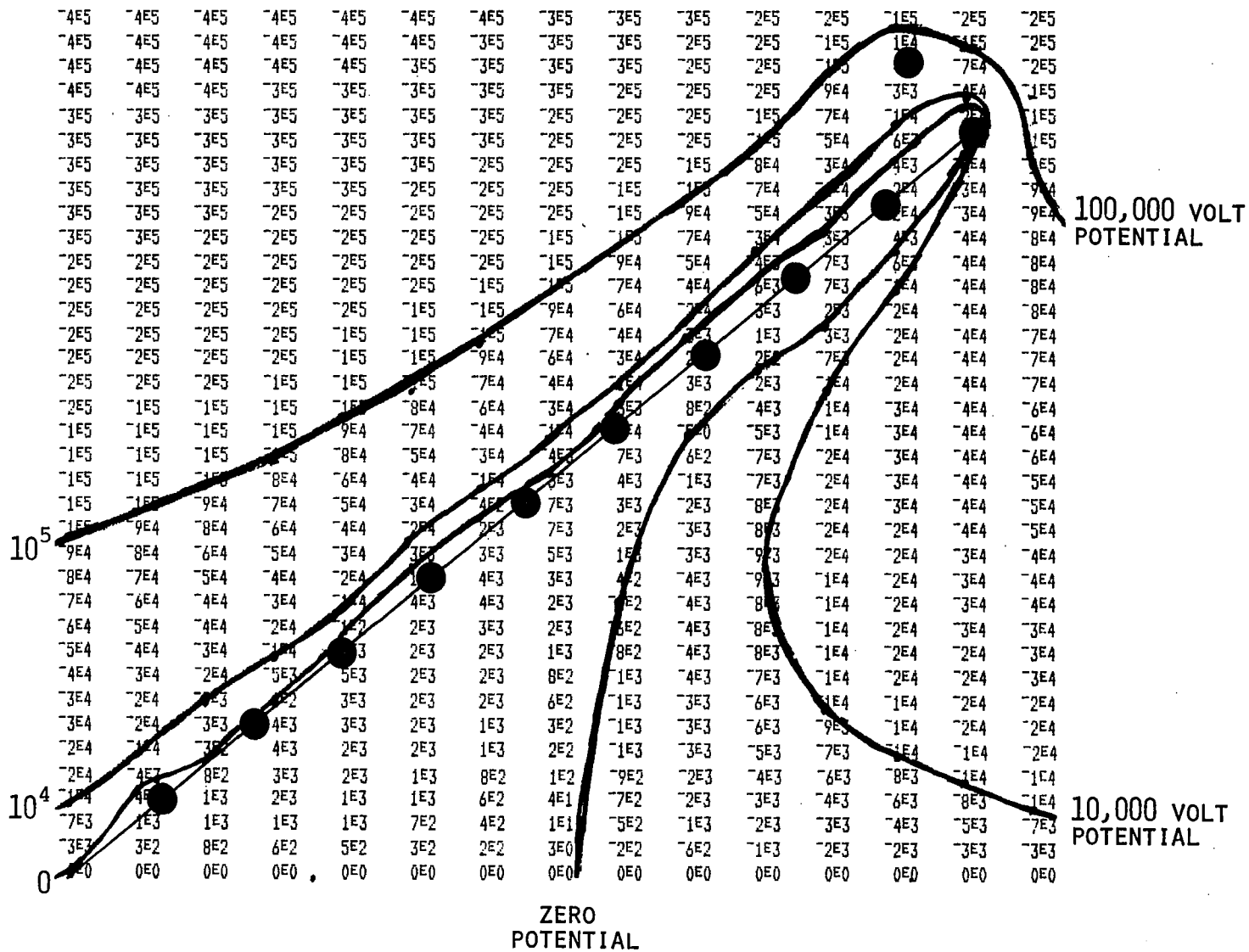


FIGURE 34



● LOCATION OF LINE CHARGES SIMULATING BILLBOARD

FIGURE 35

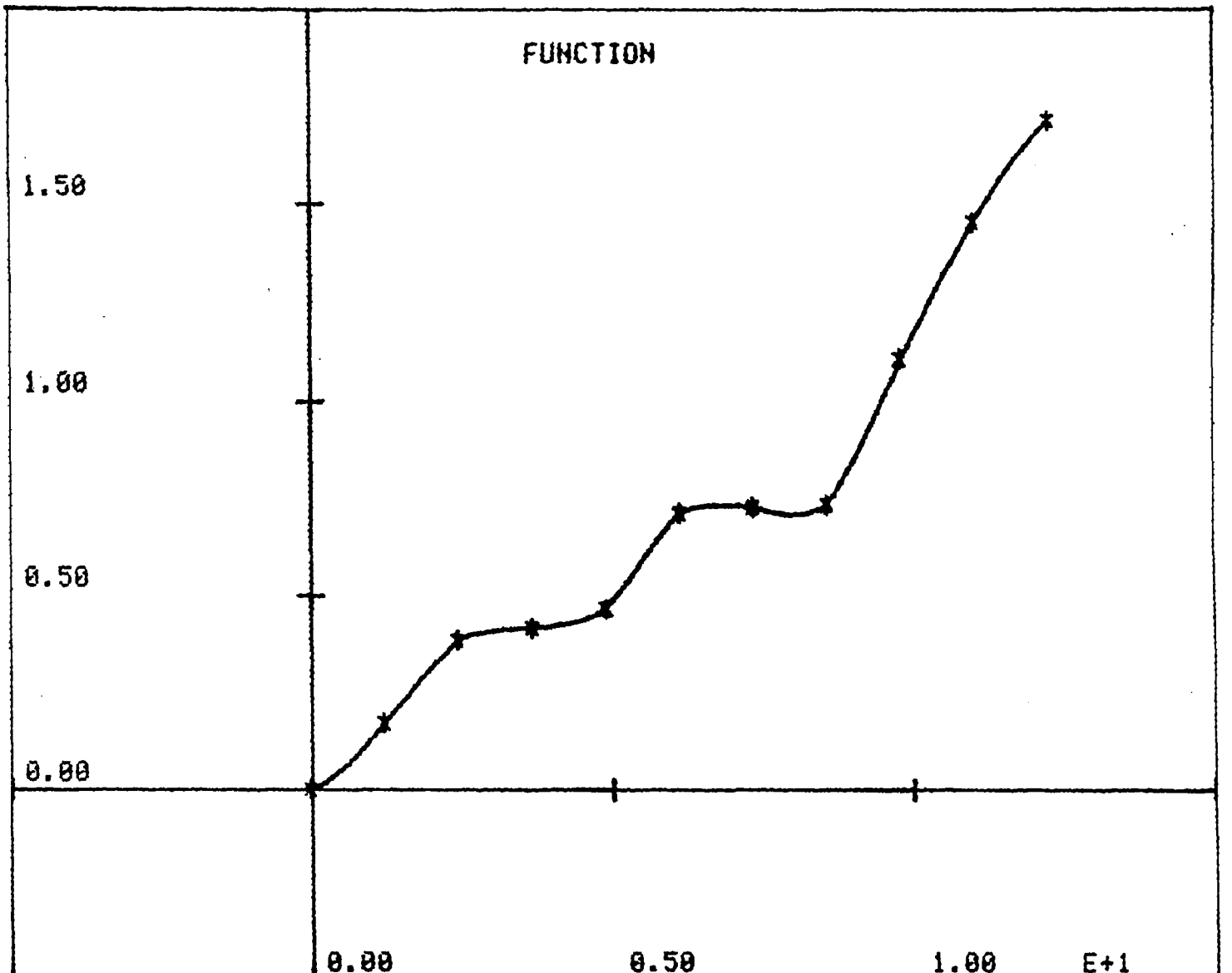


FIGURE 36

VIII. COMPUTATION OF LIGHTNING ELECTRIC FIELDS

In section VII, a rectenna was simulated in the presence of a uniform electric field of 100,000 Volts. The induced surface charges derived from the simulation are directly proportioned to the imposed electric field strength.

In this section we describe a computer program that was written to derive values for the lightning-produced electric fields as a function of time and of distance from "ground zero" - the point of strike. We have run the program for a range of lightning parameters obtained from actual measurements reported in the literature.

The program computes the contribution to the electric field from the thundercloud charge center participating in the cloud-to-ground flash, the charge on the lightning channel, and the images of these charges. All charges are allowed to vary with time in a manner consistent with observations [Terrestial Environment (Climatic) Criteria Guidelines for Use in Aerospace Vehicle Development, 1977 Revision; Edited by John W. Kaufman, NASA Technical Memorandum 78118].

Figure 37 displays the relevant equations and configurations covering the leader phases of the computation.

In Figure 38 the equations and conditions during the return stroke portion are shown. The program used in computing the fields is provided in the appendix.

The material following Figure 38 provides the tabular and graphic data used in these computations for the return stroke phase. These data are contained in Figures (39-44) inclusive.

The output of the computer program is a "blow-by-blow" history of the electrical field at a specified distance from ground zero as a function of time. Figure 45 displays one section of the output from one of the computer runs. This corresponds to a worst-case situation, 10 meters away from the very-severe-model. The units of time are seconds(along the abscissa), and the units of the ordinate are kilovolts per meter.

Table 8.4 in figure 46 provides a summary of the output for the various computer runs. Listed are the peak negative fields, the peak positive fields (when positive fields occur), and the ΔE and ΔT for the portion of the flash with the peak rate of change of electric field.

These values are our input data to the computation of diode failure when used in conjunction with the induced surface charge results of the rectenna electrostatic simulations.

STEPPED OR DART LEADER PROCESSES:

INITIAL SPECIFICATIONS

$$\begin{cases} Y_0 \ (\sim 5 \text{ KM}) \\ Q_0 \ (\sim -10 \text{ Coul}) \\ V_L \ (\sim 10^5 \text{ M/s}) \\ T = 0 \ , \ Y = Y_0 \\ Q_L \ (\sim -5 \text{ Coul}) \\ P = P_L = Q_L / Y_0 \end{cases}$$

TEMPORAL FUNCTIONS:

$$X = Y_0 - V_L T$$

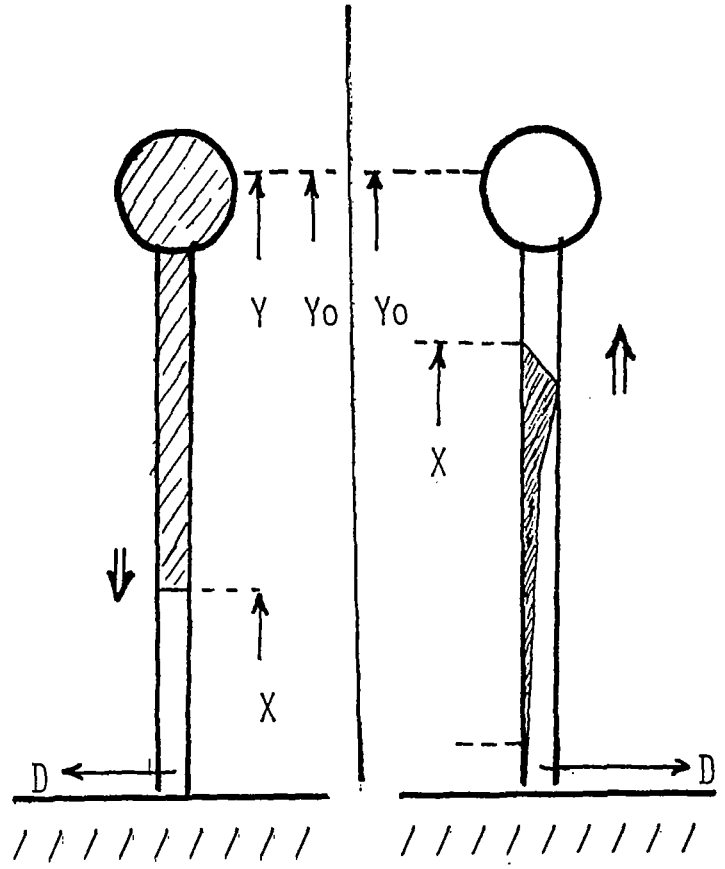
$$Q = Q_0 - P_L (Y - X)$$

SOLVE FOR $E_L (T,D)$ FOR $T \leq T_L$ WHERE

$T_L = (Y_0 - X_L) / V_L$

X_L ($\sim$50 METERS)

FOR $T > T_L$, $E_L (T,D) = E_L (T_L, D)$



$$E = \frac{2P}{4\pi\varepsilon_0} \left\{ \frac{1}{(D^2 + X^2)^{1/2}} - \frac{1}{(D^2 + Y^2)^{1/2}} \right\} + \frac{2 Q Y_0}{4\pi \varepsilon_0 (D^2 + Y_0^2)^{3/2}}$$

FIGURE 37

RETURN STROKE PROCESS:

INITIAL SPECIFICATIONS

Y_0, Q_0, Q_L

SAME AS LEADER PROCESS

$T' = T - T_L$

V_R ($\sim 5 \times 10^7$ m/s)

$X = 0$

$I(T)$  SIGN OPPOSITE TO Q_0

TEMPORAL FUNCTIONS:

$Y = V_R T'$

$$\left.\begin{aligned} P &= \int I\,dT/Y \\ Q &= 0 \end{aligned}\right\} \text{ FOR } Y < Y_0$$

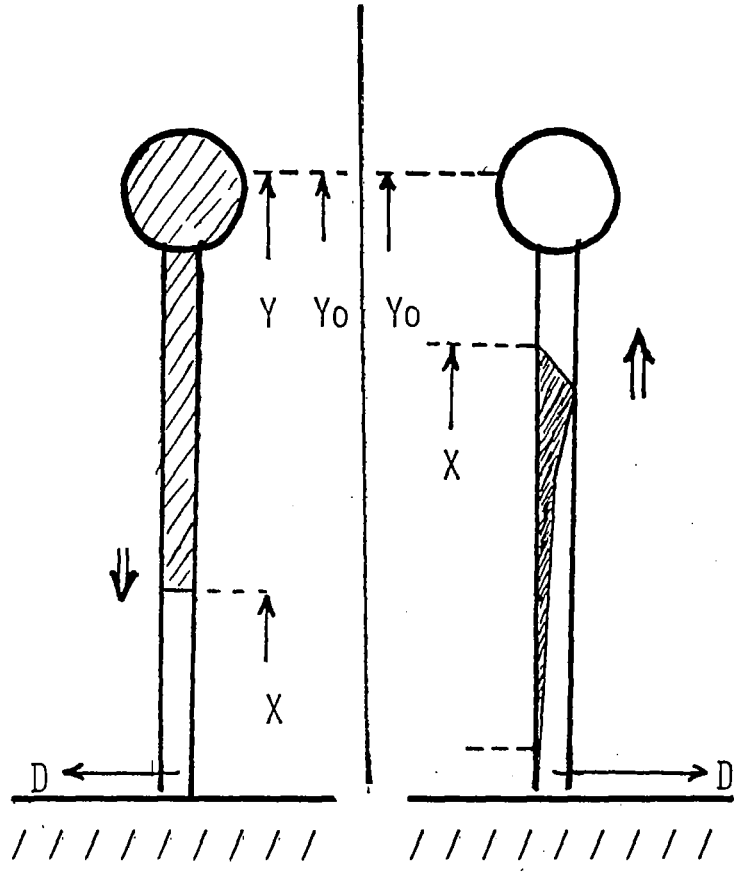
$$\left.\begin{aligned} P &= \int I\,dT/Y_0 \\ Q &= 0 \end{aligned}\right\} \text{ FOR } Y > Y_0 \text{ AND } P \leq -P_L$$

$$\left.\begin{aligned} P &= -P_L \\ Q &= \int I\,dT + Q_L \end{aligned}\right\} \text{ FOR } Y > Y_0 \text{ AND } P > -P_L \text{ AND } Q \leq -(Q_0 - Q_L)$$

SOLVE FOR $E_R(T', D)$ FOR $T > T_L$ OR $T' > 0$

TOTAL FIELD $E_T(T,D) = E_L(T_L, D) + E_R(T,D)$

TERMINATE COMPUTATION WHEN $Q \geq -(Q_0 - Q_L)$



$$E = \frac{2P}{4\pi\varepsilon_0}\left\{\frac{1}{(D^2 + X^2)^{1/2}} - \frac{1}{(D^2 + Y^2)^{1/2}}\right\} + \frac{2\,QY_0}{4\pi\varepsilon_0\,(D^2 + Y_0^2)^{3/2}}$$

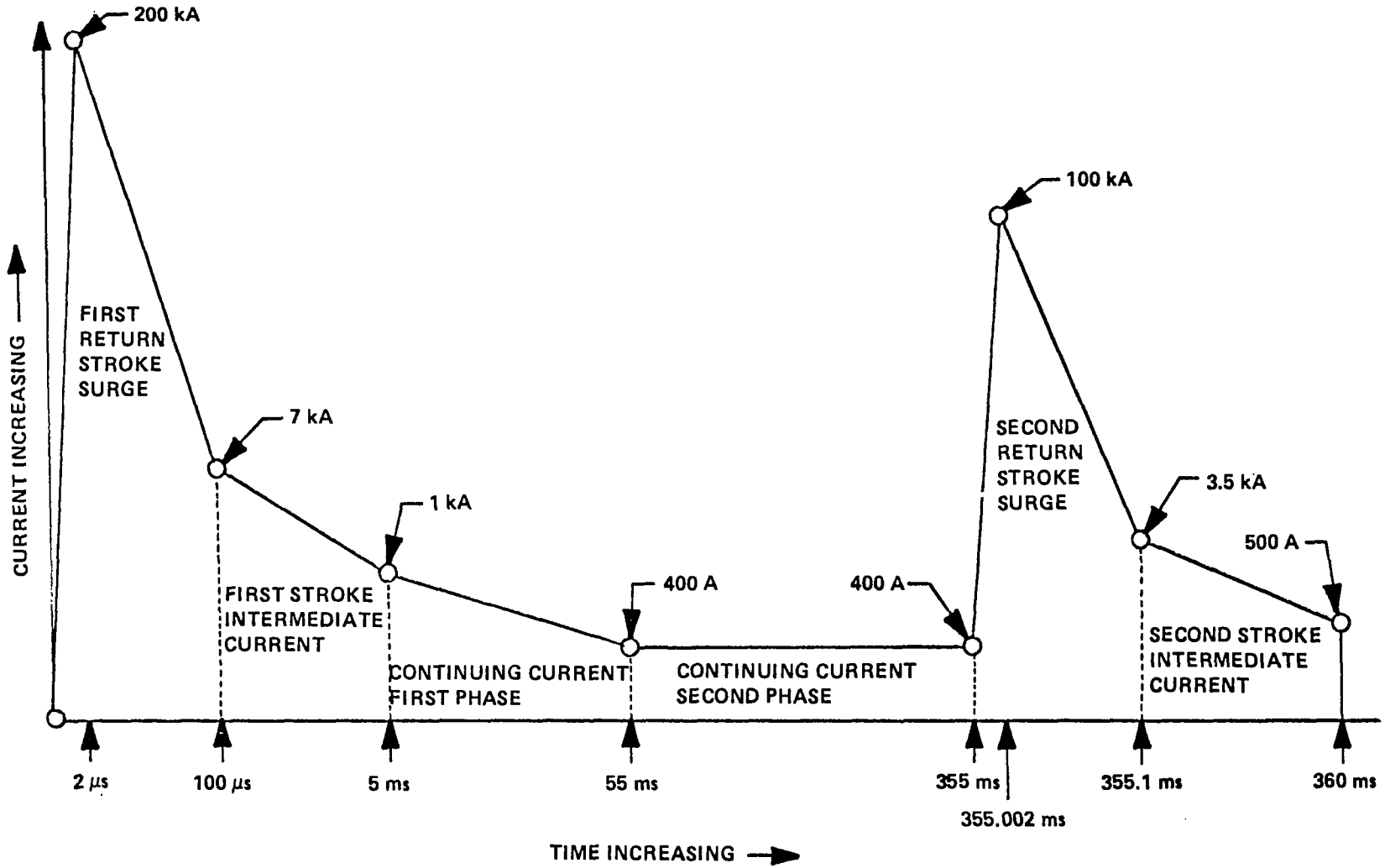
FIGURE 38

DETAILS OF A VERY SEVERE LIGHTNING MODEL (MODEL 1)

Stage	Key Points	Rate of Current Change	Charge Passing
1. First Return Stroke Surge	t = 0 i = 0 t = 2 μs i = 200 kA t = 100 μs i = 7 kA	Linear Rise - 100 kA/μs Linear Fall - 193 kA in 98 μs	0.2 C* ~ 10.2 C
2. First Stroke Intermediate Current	t = 100 μs i = 7 kA t = 5 ms i = 1 kA	Linear Fall - 6 kA in 4.9 ms	19.6 C
3. Continuing Current-- First Phase	t = 5 ms i = 1 kA t = 55 ms i = 400 A	Linear Fall - 600 A in 50 ms	35.0 C
4. Continuing Current-- Second Phase	t = 55 ms i = 400 A t = 355 ms i = 400 A	Steady Current	120.0 C
5. Second Return Stroke Surge	t = 355 ms i = 400 A t = 355.002 ms i = 100 kA t = 355.1 ms i = 3.5 kA	Linear Rise ~ 50 kA/μs Linear Fall - 96.5 kA in 98 μs	~ 0.1 C ~ 5.1 C
6. Second Stroke Intermediate Current	t = 355.1 ms i = 3.5 kA t = 360 ms i = 500 A	Linear Fall - 3 kA in 4.9 ms	9.8 C

* Coulomb (C) is the quantity of electricity transported in one second by a current of one ampere.

FIGURE 39



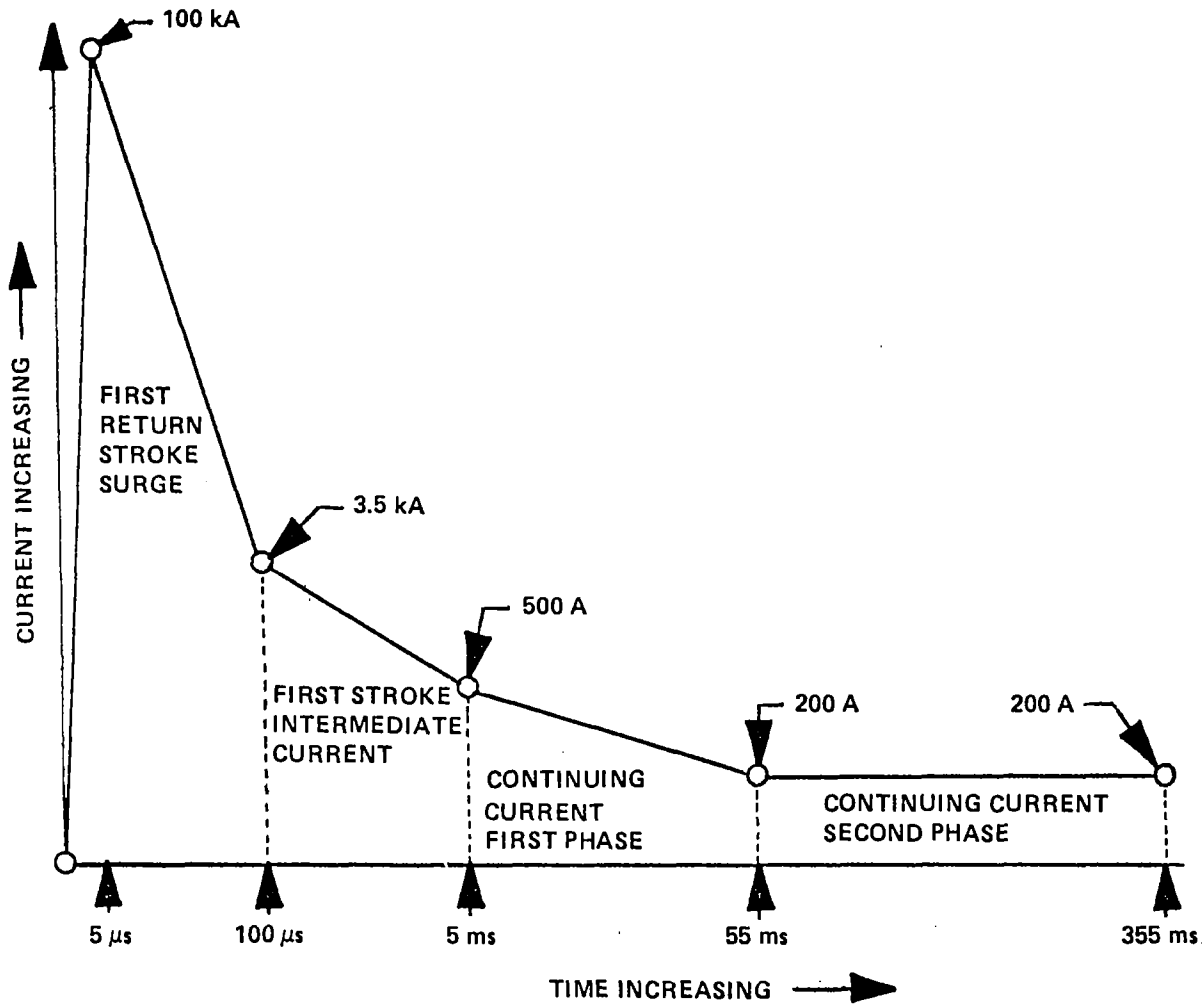
DIAGRAMMATIC REPRESENTATION OF A VERY SEVERE LIGHTNING MODEL (MODEL 1) (Note that the diagram is not to scale)

FIGURE 40

DETAILS OF A 98 PERCENTILE PEAK CURRENT LIGHTNING MODEL (MODEL 2)

Stage	Key Points		Rate of Current Change	Charge Passing
1. First Return Stroke Surge	t = 0	i = 0	Linear Rise - 20 kA/μs	0.3 C
	t = 5 μs	i 100 kA	Linear Fall - 96.5 kA in 95 μs	~ 4.9 C
	t = 100 μs	i 3.5 kA		
2. First Stroke Intermediate Current	t = 100 μs	i 3.5 kA	Linear Fall - 3 kA in 4.9 ms	9.8 C
	t = 5 ms	i 500 A		
3. Continuing Current-- First Phase	t = 5 ms	i 500 A	Linear Fall - 300 A in 50 ms	17.5 C
	t = 55 ms	i 200 A		
4. Continuing Current-- Second Phase	t = 55 ms	i 200 A	Steady Current	60 C
	t = 355 ms	i 200 A		

FIGURE 41



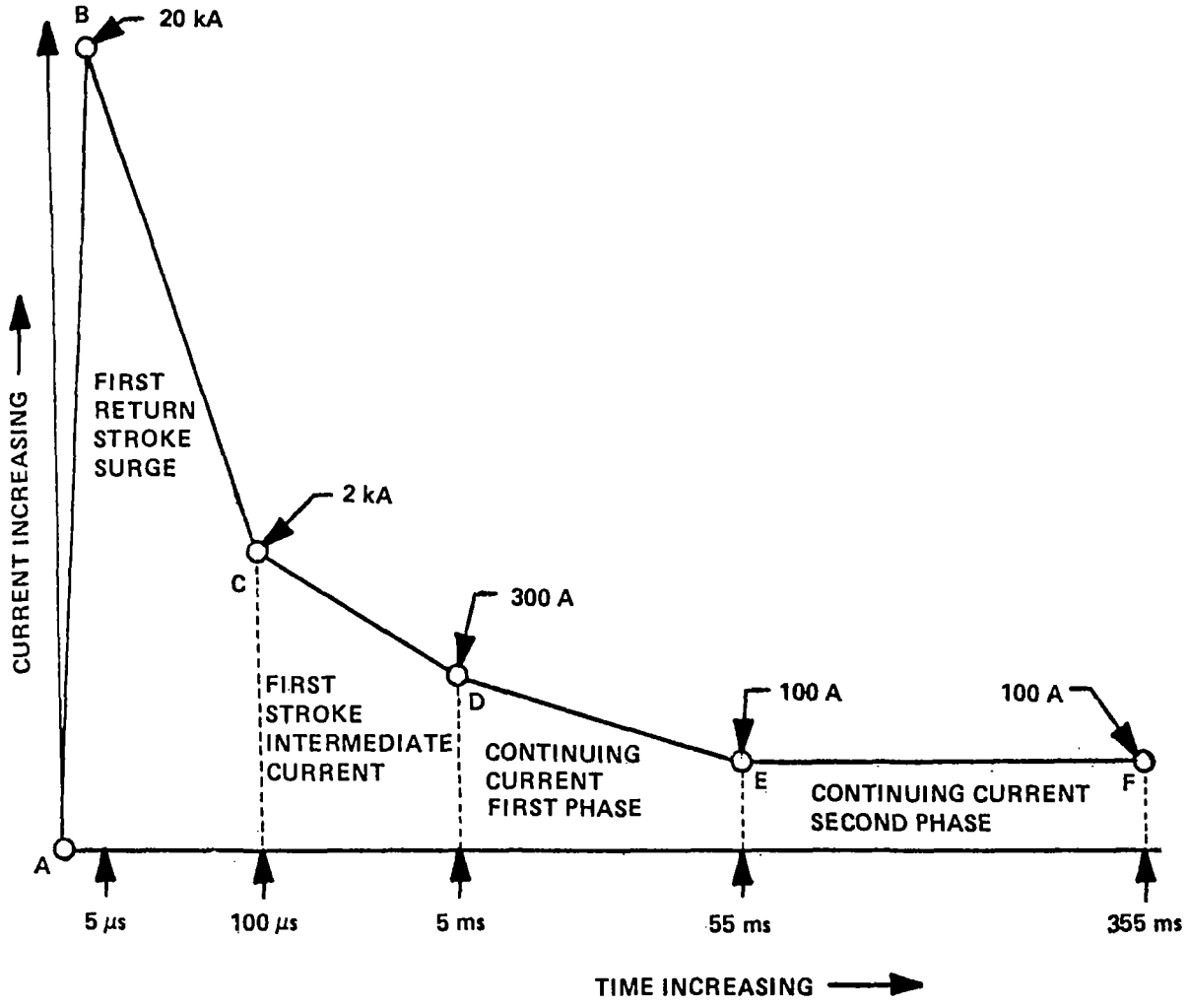
DIAGRAMMATIC REPRESENTATION OF A 98 PERCENTILE PEAK CURRENT LIGHTNING MODEL (MODEL 2) (Note that the diagram is not to scale.)

FIGURE 42

DETAILS OF AN AVERAGE LIGHTNING MODEL (MODEL 3)

Stage	Key Points		Rate of Current Change	Charge Passing
1. First Return Stroke Surge	t = 0	i = 0	Linear Rise - 4 kA/μs	0.1 C
	t = 5 μs	i = 20 kA	Linear Fall - 18 kA in 95 μs	~ 1.0 C
	t = 100 μs	i = 2 kA		
2. First Stroke Intermediate Current	t = 100 μs	i = 2 kA	Linear Fall - 1.7 kA in 4.9 ms	5.6 C
	t = 5 ms	i = 300 A		
3. Continuing Current -- First Phase	t = 5 ms	i = 300 A	Linear Fall - 200 A in 50 ms	10.0 C
	t = 55 ms	i = 100 A		
4. Continuing Current -- Second Phase	t = 55 ms	i = 100 A	Steady Current	30.0 C
	t = 355 ms	i = 100 A		

FIGURE 43



DIAGRAMMATIC REPRESENTATION OF AN AVERAGE LIGHTNING MODEL (MODEL 3) (Note that the diagram is not to scale.)

FIGURE 44

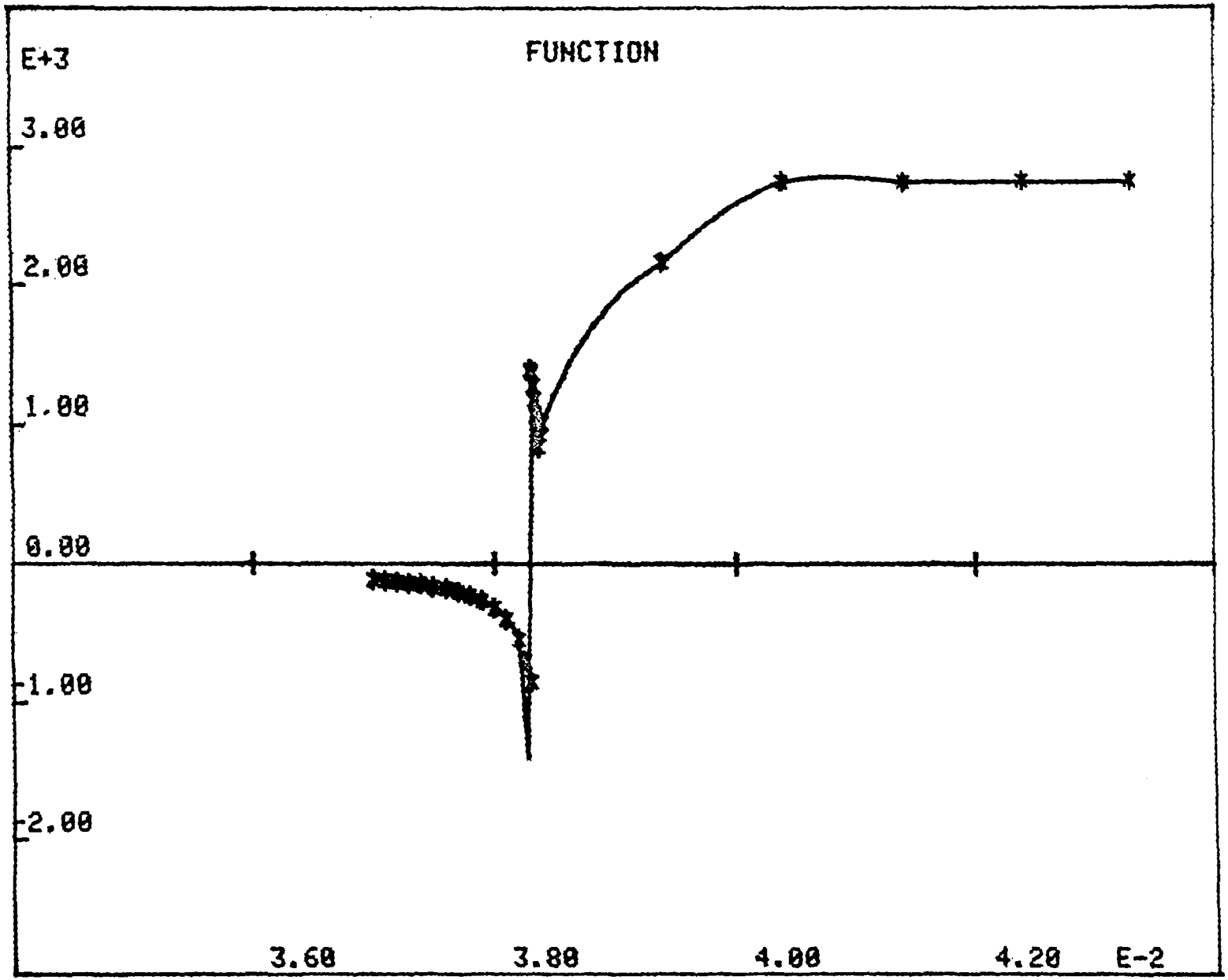


FIGURE 45

TABLE 8.4

Distance	VERY SEVERE MODEL Peak Negative	VERY SEVERE MODEL Peak Positive	VERY SEVERE MODEL $\Delta E/\Delta T$ Peak	98 PERCENTILE MODEL Peak Negative	98 PERCENTILE MODEL Peak Positive	98 PERCENTILE MODEL $\Delta E/\Delta T$ Peak	AVERAGE MODEL Peak Negative	AVERAGE MODEL Peak Positive	AVERAGE MODEL $\Delta E/\Delta T$ Peak
10 m	$-8.5X10^5$	$2.8X10^6$	$\frac{2.2X10^6}{1.2X10^{-5}}$	$-5.95X10^5$	$1.81X10^6$	$\frac{6.46X10^5}{3.00X10^{-6}}$	$-5.09X10^5$	$1.30X10^6$	$\frac{5.68X10^5}{2.59X10^{-5}}$
50 m	$-5.7X10^5$	$1.7X10^5$	$\frac{4.37X10^5}{2.2X10^{-5}}$	$-3.88X10^5$	$1.04X10^5$	$\frac{3.59X10^5}{2.5X10^{-5}}$	$-3.10X10^5$	$6.1X10^4$	$\frac{1.14X10^5}{2.50X10^{-5}}$
100 m	$-3.49X10^5$	$2.49X10^4$	$\frac{2.15X10^5}{2.2X10^{-5}}$	$-2.36X10^5$	N/A	$\frac{1.75X10^5}{2.5\ X10^{-5}}$	$-1.85X10^5$	N/A	$\frac{5.47X10^4}{3.5\ X\ 10^{-5}}$
500 m	$-8.94X10^4$	N/A	$\frac{3.79X10^4}{3.2\ X10^{-5}}$	$-6.15X10^4$	N/A	$\frac{2.96X10^4}{4.5\ X\ 10^{-5}}$	$-5.12X10^4$	N/A	N/A
1000 M	$-5.35X10^4$	N/A	$\frac{1.69X10^4}{4.2X10^{-5}}$	$-2.61X10^4$	N/A	N/A	$-3.29X10^4$	N/A	N/A

FIGURE 46

IX. COMPUTATIONS OF DIODE FAILURE

We are now to the point of having generated all of the data that are required to evaluate the conditions under which the microwave rectifier diodes will fail due to induced currents from nearby lightning flashes. For a given ΔE and ΔT (from Table 8.4) we obtain from Figure 31 the power required for diode failure and from Figure 32 the induced charge/unit area on the rectenna surface. We assume that a diode designed to operate at 67 V will have a breakdown voltage of about 100 Volts.

The surface area of the rectenna that has an induced surface charge of the size sufficient to cause diode failure is then computed from comparison with areas of the rectenna served by individual diodes and by series strings of diodes. Sample computations follow.

SAMPLE COMPUTATION OF DIODE FAILURE (98TH PERCENTILE - 10 METER - NO PROTECTION)

1. 98 percentile model - 10 meters: $\Delta T = 3 \times 10^{-6}$ and $\Delta E = 6.46 \times 10^{5}$.
2. Expected diode failure power from Figure 30: 250 Watts.
3. Energy dissipated in the diode: 250 Watts x 3×1^{-6} s = 7.5×10^{-4} Joules.
4. Charge transferred across 100 Volts diode breakdown voltage = 7.5×10^{-6} Coulombs.
5. From ΔE in step 1 and figure 37, the induced charge/unit area = 3×10^{-6} c/m^2 x 6.46 = 19.38×10^{-6} c/m^2.
6. From steps 4 and 5, the rectenna area with surface charge equivalent to the charge required to cause diode failure is: 0.39 m^2.
7. Area served by diodes: rectenna center, .

$$\frac{25 \text{ watts}}{230 \text{ w/m}^2} = 0.11 \text{ m}^2; \text{ rectenna edge, } \frac{25 \text{ watts}}{10 \text{ w/m}^2} = 2.5 \text{ m}^2.$$

8. Compare 6 with 7: single diode configuration near rectenna center is safe. Single diode configuration near rectenna edge is vulnerable.
9. <u>However</u>, the diodes are to be put in series (597 to a string) hence the diodes near the bottom must carry all of the induced current to the entire string. For these bottom-string diodes the area served with respect to the induced charge is: rectenna center, 60 m^2; rectenna edge, 1400 m^2.
10. To protect against the 98 percentile flash within 10 meters of ground zero would require fast surge protection diodes (back to back zeners) on all diodes in the rectenna. This extent of protection may not be cost effective; however the considerations in Section X indicate that simpler protection arrangements will probably be effective near the rectenna center.

FAILURES PRODUCED BY THE AVERAGE LIGHTNING FLASH

The situation considered here is the extent of the protection required for an "average" lightning flash if we are willing to accept losses from the extreme cases.

The computation sequence follows the same procedure described immediately above. Here we use data for the average flash from Table 8.4 at a 10 m distance from ground zero.

SAMPLE COMPUTATION OF DIODE FAILURE
(AVERAGE FLASH, 10 M, WITH "STATIC" PROTECTION)

1. From Table 8.4: $\Delta E = 5.68 \times 10^{5}$ v/m; $\Delta T = 2.59 \times 10^{-5}$ s.
2. From Figure 6.1: 80 watts.
3. $80 \text{ w} \times 2.59 \times 10^{-5} \text{ s} \simeq 2 \times 10^{-3}$ Joules.
4. 2×10^{-5} coulombs.
5. From 1 and Figure 38: $1.5 \times 10^{-6} \times 5.68 = 8.52 \times 10^{-6}$ coul/m^2.
6. From 4 and 5: Area = 2.35 m^2.
7. Since the rectenna area served by individual diodes even on the edge < 2.5 m^2, the individual diodes are self-protecting and able to take an "average" lightning flash.
8. <u>However</u>, when arranged in a series stack of 597, the diodes at the bottom of the stack must conduct the induced currents for the whole stack. The diodes <u>cannot</u> safely carry these currents.

X. LIGHTNING PROTECTION FOR SERIES DIODE STRINGS

As demonstrated in Section IX, the connection of microwave rectifier diodes in series requires special lightning protection considerations. We cannot make specific recommendations for these protection devices at this time because the rectenna current design is not advanced to the point that allows such detailed analysis. Rockwell International has provided us with an equivalent circuit for the rectenna; a slightly modified form of that circuit is shown in Figure 46. We have assumed that the series connections are to be made at the points indicated by the large spots and that the output filler operates around 30 Hz. A series string of rectenna elements of this design can be protected with a variety of methods. One cost-effective means is a spark gap arrangement incorporated in the diode feedthroughs, or the output filter inductors, or on the billboard configuration itself.

RECTENNA EQUIVALENT CIRCUIT AT 2.45 GHz

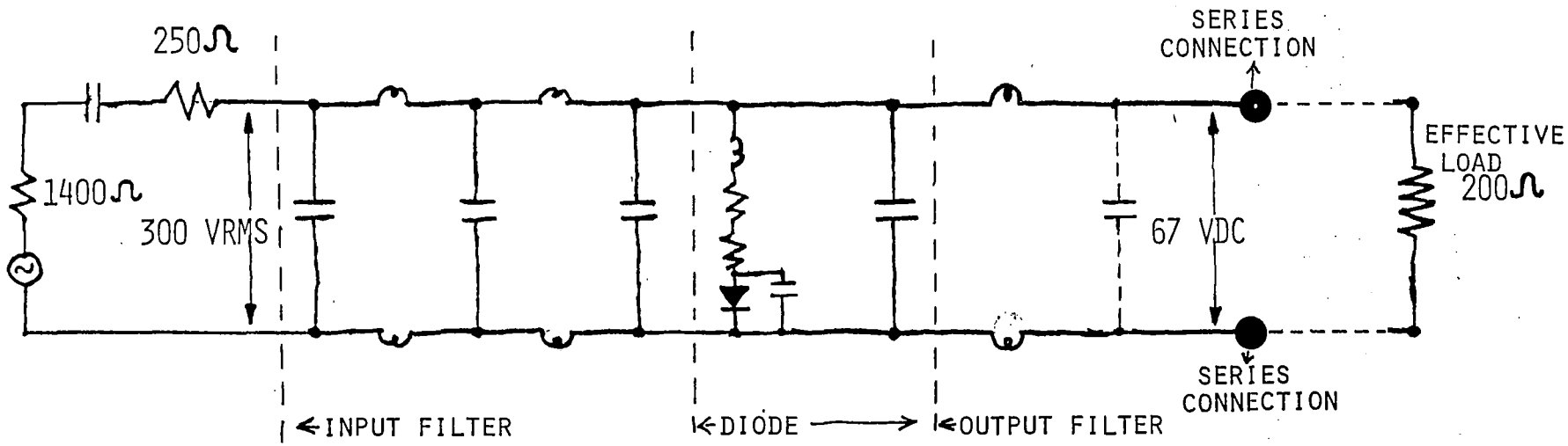


FIGURE 46

XI. CLOUD-TO-GROUND LIGHTNING DISTRIBUTION IN THE UNITED STATES

In order to have a working estimate of the hazard presented by lightning to rectennas, we need to know the cloud-to-ground lightning flash density for various possible rectenna sites in the United States. The cloud-to-ground lightning flash density (in #/km^2 for example) is not a parameter that is measured as a climatological variable. We have found it necessary to use the number-of-thunderstorm days as a proxy variable because it is available as a climatological variable. Figure 47 gives contours of annual number-of-thunderstorm days.

XI.1. Pierce Conversion Formula

Several attempts have been made to derive a conversion formula to convert thunderstorm days into the flash density by using lightning flash counters in research areas for correlation with the count of thunderstorm days. The best of the various conversion formulas is that due to E.T. Pierce ("A Relationship Between Thunderstorm Days and Lightning Flash Density," Trans. AGU, 49, 686, 1967.) The Pierce formula (as does most others) has a quadratic term, which reflects the relationship between frequencies of local storms and storm intensity. In addition, the formula utilizes the monthly thunderstorm days as opposed to the annual average in order to incorporate seasonal effects in the conversion formula.

This formula is

$$q_M^2 = aT_M + a^2T_M^4,$$

where: T_M = monthly number of thunderstorm days and q_M is the monthly ground flash density (#km^2/Mt.) The parameter a is,

$$a = 3 \times 10^{-2}$$

If σ is the annual ground flash density (# km^{-2}/yr.), then

$$\sigma = \sum_{M=1}^{12} \sigma_M.$$

XI.2. Climatological Data -- Number of Thunderstorm Days

The inputs needed to compute the U.S. Distribution of ground lightning flash density are: (1) The monthly number of thunderstorm days for all U.S. stations recording these observations, (2) the coordinates of the observing sites, and (3) the computer software to compute the density and display the results geographically.

Items 1 and 2 were obtained from "Local Climatological Data - Annual Summaries for 1977" published by The National Oceanic and Atmospheric Administration on magnetic tape. The geographic plotting software of Item 3 was obtained from The National Technical Information Service, and the computer programming was done by J.L. Bohannon at Rice.

A detailed list of flash density for all of the stations used is provided in the Appendix.

Note the hot spots on the contours in Figure 48 that result when stations are located near geographic features that promote local thunderstorms. There are probably other similar hot spots in the U.S. that do not show up on this display because of the absence of an observing station nearby.

UNITED STATES DISTRIBUTION OF THE NUMBER OF THUNDERSTORM DAYS

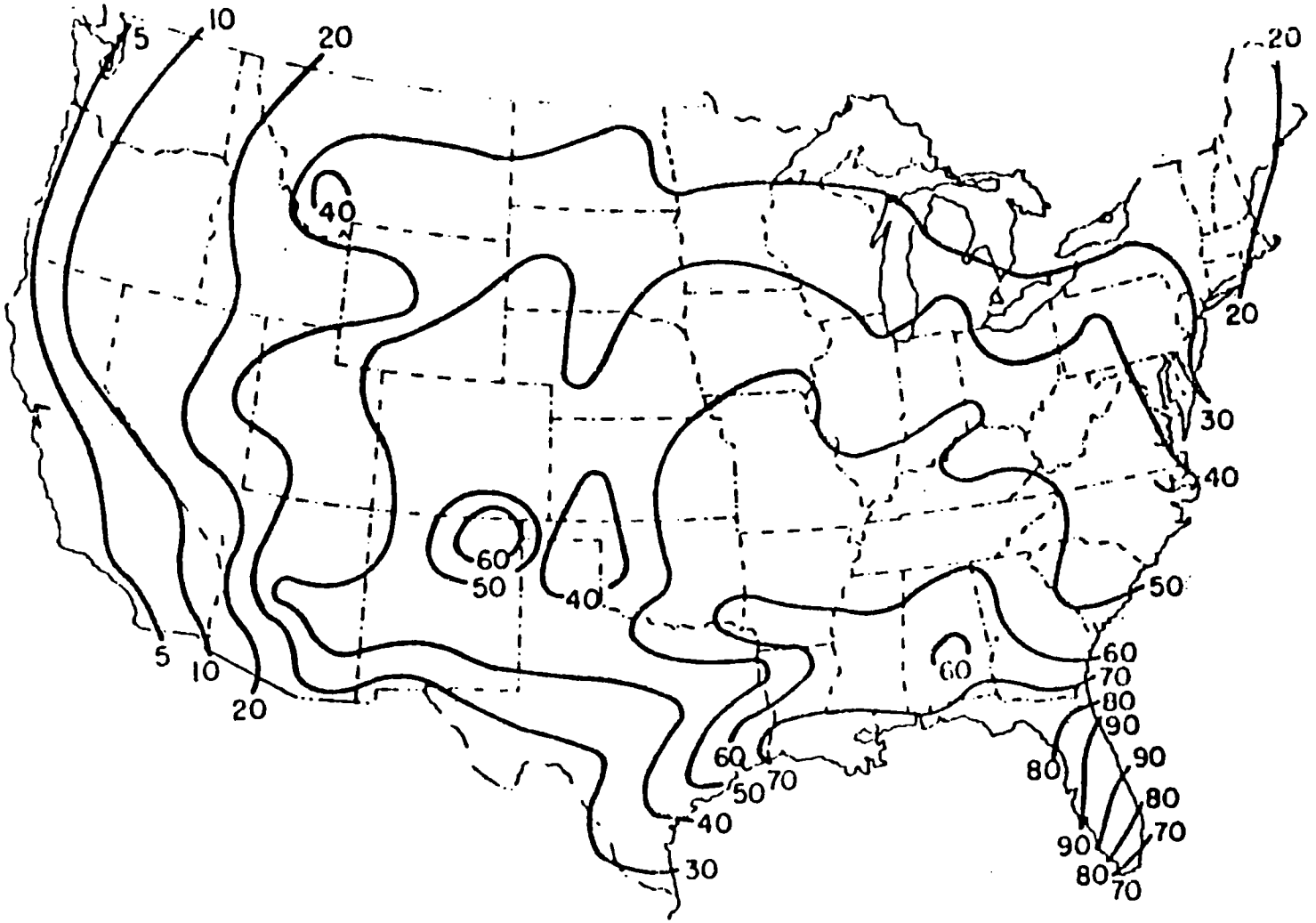
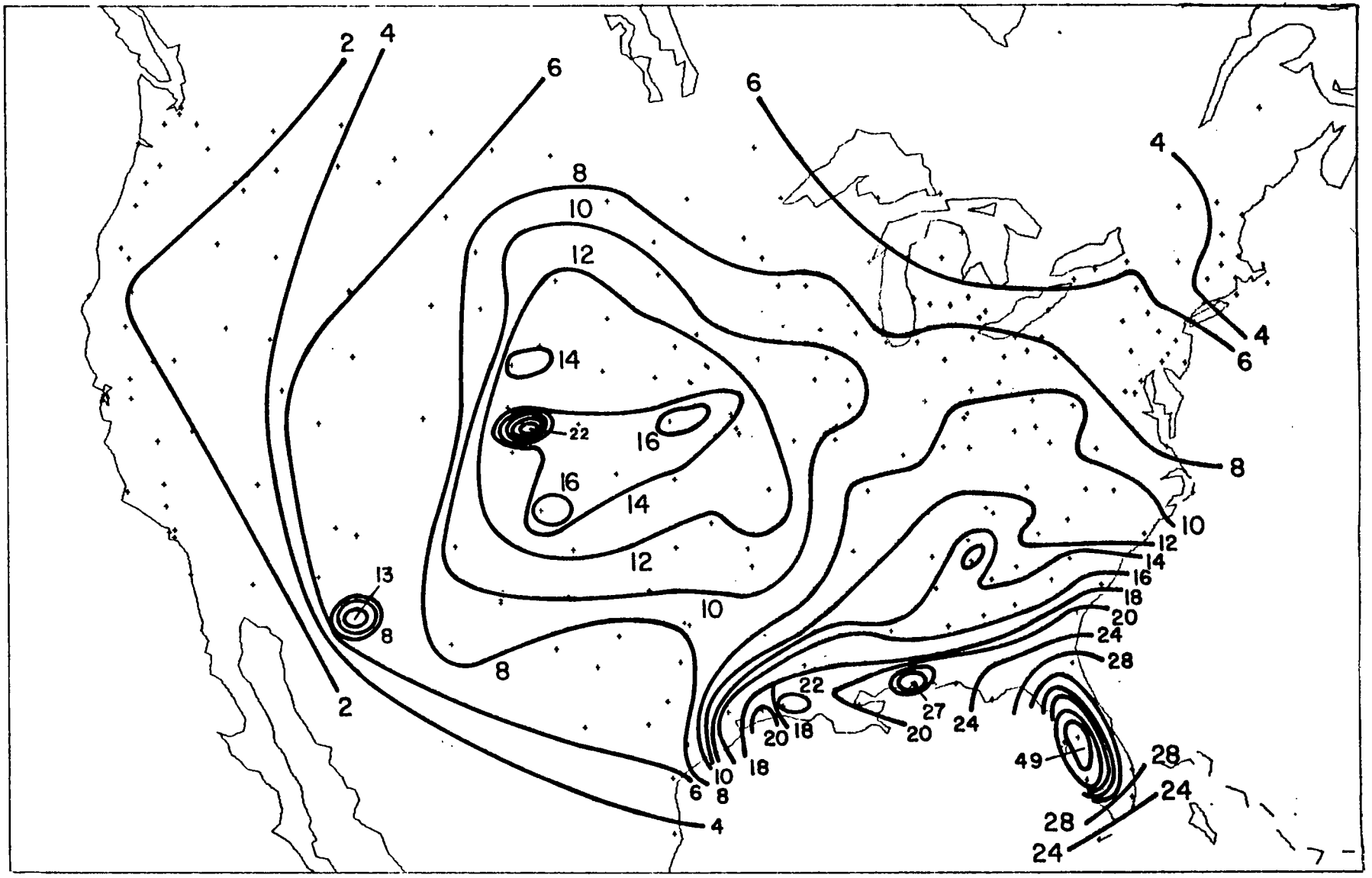


FIGURE 47


2
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6
4
4
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8
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12
14
22
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16
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18
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28
24

FIGURE 48

APPENDICES

Computer programs developed under this contract.

All programs are in FORTRAN H, unless otherwise specified. All of the programs were run on an IBM 370/155 and/or an Itel AS/6 computer.

Apendix A

Computer Program PANEL:
A Computer Model of the SPS Plasma Interaction

The following pages are the listing of the program "PANEL," written to model the interaction of a high voltage solar array with an ambient Maxwellian plasma. The program was originally written by Dr. Lee W. Parker and was modified for application to the SPS problem by David L. Cooke.

```
                                        XX  XXXXXXXXXXXX  XX
 XXXXXXXXXX    XXXXXXXXXXX  XXX       XX  XXXXXXXXXXXX  XX
XX        XX  XX        XX  XXXX      XX  XX            XX
XX        XX  XX        XX  XX XX     XX  XX            XX
XX        XX  XX        XX  XX  XX    XX  XX            XX
XXXXXXXXXXXX  XXXXXXXXXXXX  XX   XX   XX  XXXXXXX       XX
XXXXXXXXXX    XXXXXXXXXXXX  XX    XX  XX  XXXXXXX       XX
XX            XX        XX  XX     XX XX  XX            XX
XX            XX        XX  XX      XXXX  XX            XX
XX            XX        XX  XX       XXX  XX            XX
XX            XX        XX  XX        XX  XXXXXXXXXXXX  XXXXXXXXXXXX
XX            XX        XX  XX         X  XXXXXXXXXXXX  XXXXXXXXXXXX

XXXXXXXXXXXX                                                           XXXXXXXXXX         XXX    X
XXXXXXXXXXX                                                           XXXXXXXXXXXX       XXXX   XX
XX      XX                                                            XX        XX      XX XX  XX
       XX                                                                       XX     XX  XX  XX
      XX                                                                        XX    XX   XX  XX
     XX                                                                        XX    XXXXXXXXXXX XX
     XX                                                                      XX     XXXXXXXXXXXX XX
     XX                                                                    XX              XX    XX
     XX                                                                  XX                XX    XX
     XX                                                                XX                  XX    XX
     XX                                                               XXXXXXXXXXXX         XX     XX
     XX                                                               XXXXXXXXXXXX         XX      X

 XXXXXXXXXX   XXXXXXXXXXXX  XXXXXXXXXXXX  XX        XX  XXXXXXXXXXXX
XXXXXXXXXXXX  XXXXXXXXXXXX  XXXXXXXXXXXX  XX       XX   XXXXXXXXXXXX
XX        XX  XX        XX  XX        XX  XX      XX    XX
XX            XX        XX  XX        XX  XX     XX     XX
XX            XX        XX  XX        XX  XX    XX      XX
XX            XX        XX  XX        XX  XXXXXXX       XXXXXXXX
XX            XX        XX  XX        XX  XXXXXXX       XXXXXXXX
XX            XX        XX  XX        XX  XX    XX      XX
XX            XX        XX  XX        XX  XX     XX     XX
XX        XX  XX        XX  XX        XX  XX      XX    XX
XXXXXXXXXXXX  XXXXXXXXXXXX  XXXXXXXXXXXX  XX       XX   XXXXXXXXXXXX
 XXXXXXXXXX   XXXXXXXXXXXX  XXXXXXXXXXXX  XX        XX  XXXXXXXXXXXX

PRINTER3 A    END JOB 2404    BIN 7     COOKE    437075SCPS    4:02:00 PM 27 MAR 79    PANEL
PRINTER3 A    END JOB 2404    BIN 7     COOKE    437075SCPS    4:02:00 PM 27 MAR 79    PANEL
PRINTER3 A    END JOB 2404    BIN 7     COOKE    437075SCPS    4:02:00 PM 27 MAR 79    PANEL
PRINTER3 A    END JOB 2404    BIN 7     COOKE    437075SCPS    4:02:00 PM 27 MAR 79    PANEL
PRINTER3 A    END JOB 2404    BIN 7     COOKE    437075SCPS    4:02:00 PM 27 MAR 79    PANEL
PRINTER3 A    END JOB 2404    BIN 7     COOKE    437075SCPS    4:02:00 PM 27 MAR 79    PANEL
  INTER3 A    END JOB 2404    BIN 7     COOKE    437075SCPS    4:02:00 PM 27 MAR 79    PANEL
    NTER3 A   END JOB 2404    BIN 7     COOKE    437075SCPS    4:02:00 PM 27 MAR 79    PANEL
       ER3 A  END JOB 2404    BIN 7     COOKE    437075SCPS    4:02:00 PM 27 MAR 79    PANEL
         R A  END JOB 2404    BIN 7     COOKE    437075SCPS    4:02:00 PM 27 MAR 79    PANEL
           A  END JOB 2404    BIN 7     COOKE    437075SCPS    4:02:00 PM 27 MAR 79    PANEL
              END JOB 2404    BIN 7     COOKE    437075SCPS    4:02:00 PM 27 MAR 79    PANEL
              END JOB 2404    BIN 7     COOKE    437075SCPS    4:02:00 PM 27 MAR 79    PANEL
  NR          END JOB 2404    BIN 7     COOKE    437075SCPS    4:02:00 PM 27 MAR 79    PANEL
  NIE         END JOB 2404    BIN 7     COOKE    437075SCPS    4:02:00 PM 27 MAR 79    PANEL
  NIEN        END JOB 2404    BIN 7     COOKE    437075SCPS    4:02:00 PM 27 MAR 79    PANEL
  NIER3 A     END JOB 2404    BIN 7     COOKE    437075SCPS    4:02:00 PM 27 MAR 79    PANEL
```

```
          COMPILER OPTIONS - NAME=  MAIN,OPT=02,LINECNT=60,SIZE=0000K,
                             SOURCE,EBCDIC,NOLIST,NODECK,LOAD,MAP,NOEDIT,NOID,NOXREF
                C
                C       SOLAR PANEL PROBLEM
ISN 0002                COMMON/CP/NPRINT,NPTS,MA,MB,ME,KMAX,XPT,YPT,AL1,BE1,EV,SMACH,
                       1 TVOLTS,CUR,XMETER
ISN 0003                COMMON/BK/IIM,IIP,JJM,JJP,KK,NTOT,IV,JV,II,JJ,M,N,VP(30),
                       1XYZ(2080,3),VV(30,20,10),XP(30),XM(10),YP(20),YM(10),ZZ(10),
                       2XX(40),YY(30),ILX,IUX,KUK,MBC,MBD,VRF,NFPS,SKPRFL,SKPLST
ISN 0004                COMMON/FLD/X(2080,2),COEF(2080,7),INDX(2080,6),SKPCO
ISN 0005                COMMON/CD/PVOLTS,XMACH,DENST,NN,PARTCL(2),PART1(2),PART2(2)
ISN 0006                COMMON/INTER/INT,IIA,JJA,KKA,IGOUT,JGOUT,KGOUT,XA,YA,ZA,
                       1XI(30),YJ(20),ZK(10)
ISN 0007                DIMENSION DATE(20)
ISN 0008                DIMENSION VFC(4),IF(4),JF(4),KF(4)
ISN 0009                INTEGER SKPRFL,SKPLST,SKPCO
ISN 0010                NF(IX,JX,KX)=IX+II*(JX-1)+II*JJ*(KX-1)
ISN 0011                L=5
ISN 0012                M=6
ISN 0013         100    READ(L,9999,END=99) DATE
ISN 0014        9999    FORMAT(20A4)
ISN 0015        2       WRITE(M,9998) DATE
ISN 0016        9998    FORMAT(42H1SOLAR PANEL ELECTRIC FIELD AND CURRENTS. ,20A4)
                C       READ GEOMETRIC PARAMETERS
                C
ISN 0017                READ(L,111) IIP,IIM,JJP,JJM,KK,IV,JV
ISN 0018                II=IIM+IIP-1
ISN 0019                JJ=JJM+JJP-1
ISN 0020                NTOT=II*JJ*KK
ISN 0021                READ(L,222) (XP(I),I=1,IIP)
ISN 0022                READ(L,222) (XM(I),I=1,IIM)
ISN 0023                READ(L,222) (YP(J),J=1,JJP)
ISN 0024                READ(L,222) (YM(J),J=1,JJM)
ISN 0025                READ(L,222) (ZZ(K),K=1,KK)
                C       READ PANEL POTENTIALS
ISN 0026                READ(L,116)(VP(I),I=1,IV),VRF
ISN 0027                READ(L,111)SKPRFL,SKPLST,ILX,IUX,KLK,KUK,MBC,MBD,NFPS,SKPCO
ISN 0028                DO 140 NPC=1,NTOT
ISN 0029                X(NPC,1)=0
ISN 0030        140     X(NPC,2)=0
ISN 0031                IIM1= IIM+IV-1
ISN 0032                JJM1 = JJM+JV-1
ISN 0033                DO 150 I = IIM,IIM1
ISN 0034                DO 150  J = JJM,JJM1
ISN 0035                III = I+1-IIM
ISN 0036                N = NF(I,J,1)
ISN 0037                X(N,1) = VP(III)
ISN 0038                X(N,2) = 1
ISN 0039        150     CONTINUE
                C
                C       CONSTRUCT REFLECTORS
ISN 0040                IF(SKPRFL.EQ.1)GO TO 163
ISN 0042                DO 160 I = ILX,IUX
ISN 0043                DO 160 K = KLK,KUK
ISN 0044                JW = MBC-K
ISN 0045                NW = NF(I,JW,K)
ISN 0046                X(NW,1) = VRF
ISN 0047                X(NW,2) = 1
```

```
ISN 0048              JW = K+MBD
ISN 0049              NW = NF(I,JW,K)
ISN 0050              X(NW,2) = 1
ISN 0051              X(NW,1) = VRF
ISN 0052       160    CONTINUE
ISN 0053              WRITE(M,231) VRF
ISN 0054       231    FORMAT(//1X,'REFLECTOR POTENTIAL = ',1PE15.5)
               C
               C      READ ADDITIONAL FIXED POTENTIALS
ISN 0055       163    IF(NFPS.LE.3)GO TO 220
ISN 0057              WRITE(M,118)
ISN 0058       118    FORMAT(//'ADDITIONAL FIXED POTENTIALS'/
                     14(6X,'POT',7X,'I',3X,'J',3X,'K' ))
ISN 0059              DO 170 NQC = 1,NFPS,4
ISN 0060              READ(L,119)(VFC(I),IF(I),JF(I),KF(I),I=1,4)
ISN 0061       119    FORMAT(4(E8.0,3I4))
ISN 0062              WRITE(M,117)(VFC(I),IF(I),JF(I),KF(I), I=1,4 )
ISN 0063       117    FORMAT(/4(3X,1PE10.2,3I4))
ISN 0064       165    DO 170 I=1,4
ISN 0065              NN = NF(IF(I),JF(I),KF(I))
ISN 0066              X(NN,1)=VFC(I)
ISN 0067              X(NN,2)=1
ISN 0068       170    CONTINUE
ISN 0069       220    CONTINUE
ISN 0070              IVP=IV+1
ISN 0071              JVP=JV+1
ISN 0072              WRITE(M,113)IIP,IIM,JJP,JJM,KK,IV,JV
ISN 0073              WRITE(M,223) (I,XP(I),I=1,IV)
ISN 0074              WRITE(M,224) (I,XP(I),I=IVP,IIP)
ISN 0075              WRITE(M,225) (I,XM(I),I=1,IIM)
ISN 0076              WRITE(M,226) (J,YP(J),J=1,JV)
ISN 0077              WRITE(M,227) (J,YP(J),J=JVP,JJP)
ISN 0078              WRITE(M,228) (J,YM(J),J=1,JJM)
ISN 0079              WRITE(M,229) (K,ZZ(K),K=1,KK)
ISN 0080              WRITE(M,230) (XP(I),I=1,IV)
ISN 0081              WRITE(M,241)(VP(I),I=1,IV)
               C
ISN 0082       111    FORMAT(16I5)
ISN 0083       113    FORMAT(//1X,I3,18H POSITIVE X-VALUES/
                     1          1X,I3,18H NEGATIVE X-VALUES/
                     2          1X,I3,18H POSITIVE Y-VALUES/
                     3          1X,I3,18H NEGATIVE Y-VALUES/
                     4          1X,I3,25H Z-VALUES (POSITIVE ONLY)/
                     5          1X,I3,33H POSITIVE X-VALUES DEFINING PANEL/
                     6          1X, I3,33H POSITIVE Y-VALUES DEFINING PANEL)
ISN 0084       116    FORMAT(8E10.0)
ISN 0085       222    FORMAT(16E5.0)
ISN 0086       223    FORMAT(//1X,27HX-VALUES POSITIVE ON PANEL=/(I3,1PE15.4))
ISN 0087       224    FORMAT(//1X,35HX-VALUES POSITIVE OUTSIDE OF PANEL=/(I3,1PE15.4))
ISN 0088       225    FORMAT(//1X,18HX-VALUES NEGATIVE=/(I3,1PE15.4))
ISN 0089       226    FORMAT(//1X,27HY-VALUES POSITIVE ON PANEL=/(I3,1PE15.4))
ISN 0090       227    FORMAT(//1X,35HY-VALUES POSITIVE OUTSIDE OF PANEL=/(I3,1PE15.4))
ISN 0091       228    FORMAT(//1X,18HY-VALUES NEGATIVE=/(I3,1PE15.4))
ISN 0092       229    FORMAT(//1X,37HZ-VALUES (POSITIVE ONLY) ABOVE PANEL=/(I3,1PE15.4))
ISN 0093       230    FORMAT(////1X,25HARRAY OF PANEL POTENTIALS//
                     1 15X,3HX =,3X,(8(F8.4,4X)/20X))
ISN 0094       240    FORMAT(/1X,2HY(,I2,2H)=,F8.4,6X,(8(1PE12.4)/20X))
ISN 0095       241    FORMAT(8X,'ALL Y,',5X,(8(1PE12.4)/20X))
```

```
I4,15I5)
/1X,34HNPRINT,NPTS,MA,MB,ME,KMAX,PROBNO =,6I6,I10/
NUMBER =, F9.1, 9X,13HTEMPERATURE =, F9.1, 6H VOLTS,9X,
    F9.1, 7H PER CC, 9X, 6HMASS =, F9.0,11H ELECTRONS /
TI SCALE =,F9.1,30H METERS = X-DIMENSION OF PANEL)
23HSINGLE SPACE POINT. X =,F10.5,5X, 3HY =,F10.5)
34HSINGLE ENERGY (MONOENERGETIC). E =,F10.5, 6H VOLTS)
27HSINGLE TRAJECTORY. X =,F10.5,5X, 3HY =,F10.5/
LI ALPHA =,F20.8 , 8H DEGREES/
LI BETA  =,F20.8 , 8H DEGREES/
RGY      =,F20.5,  6H VOLTS)
32HRANDOM THERMAL CURRENT DENSITY =,1PE13.4,
FI SQUARE METER, FOR,2A5)
1I 1NTERFACE X-VALUES/(I3,1PE15.4))
18HINTERFACE Y-VALUES/(I3,1PE15.4))
18HINTERFACE Z-VALUES/(I3,1PE15.4))
 F22H -- CURRENTS AND POWER))

II

  GO TO 420

   I

        6
  0 TO 480
   J

  I-1)+XX(I))

  J-1)+YY(J))
```

YY(1) = YM(6) = -5

YY(11) = 5

YY(6) = 0

```
ISN 0141              ZK(1)=ZZ(1)
ISN 0142              ZK(KKA)=ZZ(KK)
ISN 0143              DO 560 K=2,KK
ISN 0144        560   ZK(K)=.5*(ZZ(K-1)+ZZ(K))
ISN 0145              WRITE(M,561) (I,XI(I),I=1,IIA)
ISN 0146              WRITE(M,562) (J,YJ(J),J=1,JJA)
ISN 0147              WRITE(M,563) (K,ZK(K),K=1,KKA)
                C
ISN 0148              DO 600 N=1,NTOT
ISN 0149              CALL FIND(IFIND,JFIND,KFIND)
ISN 0150              XYZ(N,1)=XX(IFIND)
ISN 0151              XYZ(N,2)=YY(JFIND)
ISN 0152              XYZ(N,3)=ZZ(KFIND)
ISN 0153        600   CONTINUE
                C
ISN 0154              IF(SKPLST.EQ.1) GO TO 660
ISN 0156              NFPP=(NTOT/300)+1
ISN 0157              DO 650 IP=1,NFPP
ISN 0158              WRITE(M,9000)
ISN 0159       9000   FORMAT(1H1/6X,1HN,3X,4HX(N),2X,4HY(N),2X,4HZ(N)//)
ISN 0160              CALL LIST(2,IP)
ISN 0161        650   CONTINUE
ISN 0162        660   CONTINUE
                C
ISN 0163              DO 700 J=1,JJ
ISN 0164              DO 700 I=1,II
ISN 0165              N = NF(I,J,1)
ISN 0166              VV(I,J,1) = X(N,1)
ISN 0167        700   CONTINUE
                C
ISN 0168              K=1
ISN 0169              WRITE(M,8000) K,ZZ(K),(XX(I),I=1,II)
ISN 0170              DO 750 J=1,JJ
ISN 0171              WRITE(M,240)  J,YY(J),(VV(I,J,K),I=1,II)
ISN 0172        750   CONTINUE
                C
ISN 0173              CALL FIELD
                C
ISN 0174              DO 800 K=1,KK
ISN 0175              DO 800 J=1,JJ
ISN 0176              DO 800 I=1,II
ISN 0177              N=NF(I,J,K)
ISN 0178              VV(I,J,K) = X(N,1)
ISN 0179        800   CONTINUE
                C
ISN 0180              DO 900 K=1,KK
ISN 0181              WRITE(M,8000) K,ZZ(K),(XX(I),I=1,II)
ISN 0182       8000   FORMAT(   26H1ARRAY OF POTENTIALS AT Z(,I2,2H)=,F8.4//
                     1 15X,3HX =,3X,(8(F8.4,4X)/20X))
ISN 0183              DO 850 J=1,JJ
ISN 0184              WRITE(M,240)  J,YY(J),(VV(I,J,K),I=1,II)
ISN 0185        850   CONTINUE
ISN 0186        900   CONTINUE
                C
ISN 0187              NPROB=0
ISN 0188       1000   READ(L,333,END=99) NPRINT,NPTS,MA,MB,ME,KMAX,MORE
ISN 0189       1001   READ(L,116) SMACH,TVOLTS,DENCC,XMASS,XMETER
ISN 0190              NPROB=NPROB+1
```

```
ISN 0191          WRITE(M,999)
ISN 0192          WRITE(M,444) NPRINT,NPTS,MA,MB,ME,KMAX,NPROB ,SMACH,TVOLTS,DENCC,
                 1 XMASS,XMETER
ISN 0193          IF(NPTS.EQ.0.OR.ME.EQ.0.OR.MA.EQ.0) READ(L,222)XPT,YPT,AL1,BE1,EV
ISN 0195          IF(NPTS.EQ.0) WRITE(M,445) XPT,YPT
ISN 0197          IF(ME.EQ.0)    WRITE(M,446) EV
ISN 0199          IF(MA.EQ.0)    WRITE(M,447) XPT,YPT,AL1,BE1,EV
ISN 0201          IF(MA.GT.0.AND.XMASS.LE.0.) STOP
ISN 0203          IF(MA.GT.0) CUR=2.68E-8*DENCC*SQRT(ABS(TVOLTS)/XMASS)
ISN 0205          IF(TVOLTS.GT.0.) PARTCL(1)=PART1(1)
ISN 0207          IF(TVOLTS.GT.0.) PARTCL(2)=PART1(2)
ISN 0209          IF(TVOLTS.LT.0.) PARTCL(1)=PART2(1)
ISN 0211          IF(TVOLTS.LT.0.) PARTCL(2 )=PART2(2)
ISN 0213          WRITE(M,448) CUR,PARTCL
ISN 0214          CALL POWER
ISN 0215          IF (MORE.GT.0) GO TO 1000
ISN 0217          GO TO 100
ISN 0218     99   STOP
ISN 0219          END
```

```
          COMPILER OPTIONS - NAME=  MAIN,OPT=02,LINECNT=60,SIZE=0000K,
                             SOURCE,EBCDIC,NOLIST,NODECK,LOAD,MAP,NOEDIT,NOID,NOXREF
ISN 0002                SUBROUTINE ORBIT
                  C
                  C     STEP ACROSS 3-D BOX ASSUMING CONSTANT POTENTIAL WITHIN BOX
                  C
ISN 0003                COMMON/BK/IIM,IIP,JJM,JJP,KK,NTOT,IV,JV,II,JJ,M,N,VP(30),
                       1XYZ(2080,3),VV(30,20,10),XP(30),XM(10),YP(20),YM(10),ZZ(10),
                       2XX(40),YY(30),ILX,IUX,KUK,MBC,MBD,VRF,NFPS,SKPRFL,SKPLST
ISN 0004                COMMON/ORB/XDOT,YDOT,ZDOT,X1,X2,Y1,Y2,Z1,Z2,X,Y,Z,PHI,NTIME,SAVE
ISN 0005                DIMENSION TIME(6),U(3),UDOT(3),B(2,3)
                  C
ISN 0006                TOOM=3.3333E+33
ISN 0007                ROUND = 1.E-11
ISN 0008                ~~TROUND = 1.E-6~~  (5 x10^-5)
                  C
ISN 0009                IF(XDOT.EQ.0..AND.YDOT.EQ.0..AND.ZDOT.EQ.0.) WRITE(M,999)
ISN 0011                IF(XDOT.EQ.0..AND.YDOT.EQ.0..AND.ZDOT.EQ.0.) RETURN
ISN 0013          999   FORMAT(1X,38HSPEED=0 - HENCE PARTICLE DOES NOT MOVE)
                  C
                  C
ISN 0014                U(1)=X
ISN 0015                U(2)=Y
ISN 0016                U(3)=Z
                  C
ISN 0017                UDOT(1)=XDOT
ISN 0018                UDOT(2)=YDOT
ISN 0019                UDOT(3)=ZDOT
                  C
ISN 0020                B(1,1)=X1
ISN 0021                B(2,1)=X2
ISN 0022                B(1,2)=Y1
ISN 0023                B(2,2)=Y2
ISN 0024                B(1,3)=Z1
ISN 0025                B(2,3)=Z2
                  C
ISN 0026                DO 101 N2=1,3
ISN 0027                IF(UDOT(N2).EQ.0.) GO TO 101
ISN 0029                DO 100 N1=1,2
ISN 0030                NR=N1 + 2*(N2-1)
ISN 0031                TIME(NR)=TOOM
ISN 0032                TT=(B(N1,N2) - U(N2))/UDOT(N2)
ISN 0033                SS=U(N2) + UDOT(N2)*TT
ISN 0034                IF(SS.GE.B(1,N2).AND.SS.LE.B(2,N2)) TIME(NR)=TT
ISN 0036          100   CONTINUE
ISN 0037            101 CONTINUE
                  C
                  C   FIND SHORTEST SIGNIFICANT TIME
                  C
ISN 0038                TIMIN=TOOM
ISN 0039                DO 200 NR=1,6
ISN 0040                IF(TIME(NR).EQ.TOOM) GO TO 200
ISN 0042                IF(TIME(NR).GT.ROUND.AND.TIME(NR).LT.TIMIN) NTIME=NR
ISN 0044                IF(TIME(NR).GT.ROUND.AND.TIME(NR).LT.TIMIN) TIMIN=TIME(NR)
ISN 0046          200   CONTINUE
                  C
                  C   ADVANCE TO APPROPRIATE END-POINT
                  C
```

NR
1
2
3
4
5
6

X2 > X1
etc.

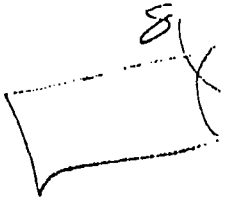
what or smallest
if you run the clockw
you'll take the next

SS = U(N2) +

SS = B

```
ISN 0047          X=X + XDOT*TIMIN
ISN 0048          Y=Y + YDOT*TIMIN
ISN 0049          Z=Z + ZDOT*TIMIN
            C
ISN 0050          XSAV=X
ISN 0051          YSAV=Y
ISN 0052          ZSAV=Z
            C
ISN 0053          IF(NTIME.EQ.1) X=X1
ISN 0055          IF(NTIME.EQ.2) X=X2
ISN 0057          IF(NTIME.EQ.3) Y=Y1
ISN 0059          IF(NTIME.EQ.4) Y=Y2
ISN 0061          IF(NTIME.EQ.5) Z=Z1
ISN 0063          IF(NTIME.EQ.6) Z=Z2
            C
ISN 0065          DX=X-XSAV
ISN 0066          DY=Y-YSAV
ISN 0067          DZ=Z-ZSAV
            C
ISN 0068          IF((NTIME.EQ.1.OR.NTIME.EQ.2).AND.ABS(DX).GT.TROUND) NTIME=-1
ISN 0070          IF((NTIME.EQ.3.OR.NTIME.EQ.4).AND.ABS(DY).GT.TROUND) NTIME=-2
ISN 0072          IF((NTIME.EQ.5.OR.NTIME.EQ.6).AND.ABS(DZ).GT.TROUND) NTIME=-3
ISN 0074          IF(NTIME.EQ.-1) SAVE=XSAV
ISN 0076          IF(NTIME.EQ.-2) SAVE=YSAV
ISN 0078          IF(NTIME.EQ.-3) SAVE=ZSAV
            C
ISN 0080          RETURN
ISN 0081          END
```

X = X + XDOT * (X1



```
          COMPILER OPTIONS - NAME=  MAIN,OPT=02,LINECNT=60,SIZE=0000K,
                             SOURCE,EBCDIC,NOLIST,NODECK,LOAD,MAP,NOEDIT,NOID,NOXREF
ISN 0002                SUBROUTINE DEN
                  C
                  C ROUTINE FOR EVALUATING CURRENT-DENSITY INTEGRALS OVER VELOCITY SPACE
                  C
ISN 0003                COMMON/BK/IIM,IIP,JJM,JJP,KK,NTOT,IV,JV,II,JJ,M,N,VP(30),
                       1XYZ(2080,3),VV(30,20,10),XP(30),XM(10),YP(20),YM(10),ZZ(10),
                       2XX(40),YY(30),ILX,IUX,KUK,MBC,MBD,VRF,NFPS,SKPRFL,SKPLST
ISN 0004                COMMON/CP/NPRINT,NPTS,MA,MB,ME,KMAX,XPT,YPT,AL1,BE1,EV,SMACH,
                       1 TVOLTS,CUR,XMETER
ISN 0005                COMMON/CD/PVOLTS,XMACH,DENST,NN,PARTCL(2),PART1(2),PART2(2)
ISN 0006                COMMON/ORB/XDOT,YDOT,ZDOT,X1,X2,Y1,Y2,Z1,Z2,X,Y,Z,PHI,NTIME,SAVE
ISN 0007                COMMON/INTER/INI,IIA,JJA,KKA,IGOUT,JGOUT,KGOUT,XA,YA,ZA,
                       1XI(30),YJ(20),ZK(10)
ISN 0008                DIMENSION A(2),END1(2),END2(2),FATE(2)
ISN 0009                DATA END1/4HABSO,4HRBED/,END2/4HESCA,4HPES /
ISN 0010                XSAVE=XPT
ISN 0011                YSAVE=YPT
ISN 0012                TEMP= ABS(TVOLTS)
ISN 0013                IF(TEMP.LE.0.) WRITE(M,999) TEMP
ISN 0015          999   FORMAT(////1X, 38HTROUBLE - NEGATIVE OR ZERO TEMPERATURE)
ISN 0016                IF(TEMP.LE.0.) RETURN
ISN 0018                IF(MA.EQ.0.OR.ME.EQ.0) EE=EV/TEMP
ISN 0020                PI=3.1415926536
ISN 0021                A(1)=-1./SQRT(3.)
ISN 0022                A(2)=-A(1)
ISN 0023                MOSTPS=0
ISN 0024                MSTEP=1000
                  C
                  C SET UP SUMS OVER TRAJECTORIES
                  C
ISN 0025                IF(MA.EQ.0) GO TO 250
ISN 0027                JAMAX=2
ISN 0028                JBMAX=2
ISN 0029                KAMAX=MA
ISN 0030                KBMAX=MB
ISN 0031                NUMBER=MA*MB*4
ISN 0032                IF(NN.EQ.1) WRITE(M,990) MA,MB,NUMBER
ISN 0034          990   FORMAT(/1X,I4,16H ALPHA-INTERVALS,3X,I4,15H BETA-INTERVALS,6X,
                       1 5HHENCE,I4,35H TRAJECTORIES FOR EACH ENERGY-VALUE)
                  C
ISN 0035                IF(ME.EQ.0) GO TO 200
ISN 0037                ME2=2*ME
ISN 0038                JEMAX=2
ISN 0039                KEMAX=ME
ISN 0040                IF(NN.EQ.1) WRITE(M,988) ME,ME2
ISN 0042          988   FORMAT(1X,I4,27H ENERGY INTERVALS AND HENCE,I4,14H ENERGY VALUES)
                  C
ISN 0043                GO TO 300
                  C
                  C SINGLE VALUE OF ENERGY
                  C
ISN 0044          200   JEMAX=1
ISN 0045                KEMAX=1
ISN 0046                IF(NN.EQ.1) WRITE(M,986) EV,EE
ISN 0048          986   FORMAT(1X,31H MONOENERGETIC CASE WTIH ENERGY,1PE16.4,30H VOLTS, OR
                       1 DIMENSIONLESS VALUE,E16.4)
```

```
                C
ISN 0049              GO TO 300
                C
                C SINGLE TRAJECTORY ONLY
                C
ISN 0050        250   JAMAX=1
ISN 0051              JBMAX=1
ISN 0052              JEMAX=1
ISN 0053              KAMAX=1
ISN 0054              KBMAX=1
ISN 0055              KEMAX=1
ISN 0056              AL=AL1*PI/180.
ISN 0057              BE=BE1*PI/180.
ISN 0058              WRITE(M,984) AL1,AL,BE1,BE,EV,EE
ISN 0059        984   FORMAT(/1X,17HSINGLE TRAJECTORY
                     1/1X, 7HALPHA =,F20.8 ,12H DEGREES, OR,F20.8 , 8H RADIANS
                     2/1X, 7HBETA  =,F20.8 ,12H DEGREES, OR,F20.8 , 8H RADIANS
                     3/1X, 8HENERGY =,1PE16.4,30H VOLTS, OR DIMENSIONLESS VALUE,E16.4)
ISN 0060              SINA=SIN(AL)
ISN 0061              COSA=COS(AL)
                C
                C SUM OVER ENERGY, BETA, AND ALPHA
                C
ISN 0062          300 CONTINUE
ISN 0063              DENST=0.
ISN 0064              DO 1001 KE=1,KEMAX
ISN 0065              DO 1001 JE=1,JEMAX
ISN 0066              DENS=0.
ISN 0067              NOESC=0
ISN 0068              DO 1000 KB=1,KBMAX
ISN 0069              DO 1000 JB=1,JBMAX
ISN 0070              DO 1000 KA=1,KAMAX
ISN 0071              DO 1000 JA=1,JAMAX
                C
                C INITIAL POSITION
                C
ISN 0072              Z=0.
ISN 0073              X=XSAVE
ISN 0074              Y=YSAVE
ISN 0075              IF(MA.EQ.0) GO TO 320
                C
ISN 0077              CA=(A(JA) + FLOAT(2*KA - 1 - MA))/FLOAT(MA)
ISN 0078              SINA=SQRT(.5*(1.+CA))
ISN 0079              COSA=SQRT(1. - SINA**2)
                C
ISN 0080              CBETA=(A(JB) + FLOAT(2*KB - 1 - MB))/FLOAT(MB)
ISN 0081              BE=PI*(1. + CBETA)
                C
                C
ISN 0082        320   XDOT=SINA*COS(BE)
ISN 0083              YDOT=SINA*SIN(BE)
ISN 0084              ZDOT=COSA
ISN 0085              INT=0
ISN 0086              CALL INTERP
                C
ISN 0087              IF(IGOUT.GE.1.AND.IGOUT.LE.IIA.AND.JGOUT.GE.1.AND.JGOUT.LE.JJA.
                     1 AND.KGOUT.GE.1.AND.KGOUT.LE.KKA) GO TO 340
ISN 0089        330   WRITE (M,9999)
```

```
ISN 0090      9999  FORMAT(/////1X,43HONE OF THE IG-JG-KG INDICES IS OUT OF RANGE)
ISN 0091            WRITE (M,888) KSTEP,X,Y,Z,XDOT,YDOT,ZDOT,IGOUT,JGOUT,KGOUT,PHI
ISN 0092            WRITE(M,982)KE,JE,KB,JB,KA,JA,BE1,AL1,EV,PVOLTS
ISN 0093            STOP
                C
ISN 0094      340   INT=1
ISN 0095            PHISAV=PHI
ISN 0096            SPEED=0.
ISN 0097            PHIOLD=PHI
ISN 0098            IF(ME.GT.0) GO TO 350
                C
ISN 0100            E=EE
ISN 0101            GO TO 400
                C
ISN 0102      350   CE=(A(JE) + FLOAT(2*KE-1-ME))/FLOAT(ME)
ISN 0103            E=(1.+CE)/(1.-CE)
ISN 0104            IF(XMACH.GT.1.) E=XMACH**2*(1.+CE)/(1.-CE)
ISN 0106            E=E + AMAX1(PHI, 0.)
                C
ISN 0107      400   IF(E.LT.PHI) GO TO 1001
ISN 0109            SPEED=SQRT(E-PHI)
                C
ISN 0110            XDOT=SPEED*SINA*COS(BE)
ISN 0111            YDOT=SPEED*SINA*SIN(BE)
ISN 0112            ZDOT=SPEED*COSA
ISN 0113            AL=ARCOS(COSA)
ISN 0114            AL1=AL*180./PI
ISN 0115            BE1=BE*180./PI
ISN 0116            EV=E*TEMP
ISN 0117            PVOLTS=PHISAV*TVOLTS
ISN 0118            ZOLD=Z
ISN 0119            KSTEP=0
ISN 0120            IF(NPRINT.NE.2.AND.NPRINT.NE.3) GO TO 490
                C
                C PRINT INITIAL CONDITIONS OF TRAJECTORY
                C
ISN 0122            WRITE(M,982) KE,JE,KB,JB,KA,JA,BE1,AL1,EV,PVOLTS
ISN 0123      982   FORMAT(/1X,52HKE,JE,  KB,JB,  KA,JA,  BETA,ALPHA,ENERGY,POTENTIAL=
                   1,/1X,3(I3,I2),1PE22.8 ,4H DEG,4X,E22.8 ,4H DEG,8X,E16.4,2H V,4X,
                   2 E16.4,2H V)
                C
ISN 0124            WRITE(M,980)
ISN 0125      980   FORMAT( 9X, 95HSTEPS      X           Y           Z          XDOT
                   1 YDOT        ZDOT         IG    JG    KG    PHI)
                C
ISN 0126            WRITE(M,888) KSTEP,X,Y,Z,XDOT,YDOT,ZDOT,IGOUT,JGOUT,KGOUT,PHI
ISN 0127      888   FORMAT( 9X,I5,1P6E11.3,3I6,E11.3)
                C
                C     TAKE A STEP
                C
ISN 0128      490   IF (KSTEP.EQ.0) GO TO 550
ISN 0130      500   CALL ORBIT
ISN 0131            KSTEP=KSTEP + 1
ISN 0132            IF(NPRINT.EQ.3) WRITE(M,888) KSTEP,X,Y,Z,XDOT,YDOT,ZDOT,IGOUT,
                   1 JGOUT,KGOUT,PHI
ISN 0134            IF(KSTEP.LE.MSTEP) GO TO 550
ISN 0136            WRITE(M,998) MSTEP
ISN 0137      998   FORMAT(/////1X, 9HMORE THAN,I6,19H STEPS - HENCE STOP)
```

```
ISN 0138              STOP
                C
                C
ISN 0139        550   IF(Z.EQ.0..AND.ZDOT.LT.0.
                     1.AND.Y.GE.YP(1).AND.Y.LE.YP(JV)) GO TO 600
                C
ISN 0141              IF((X.LE.XX(1).AND.ZDOT.LT.0.).OR.
                     1(X.GE.XX(II).AND.ZDOT.LT.0.))GO TO 600
                C
ISN 0143              IF((X.LE.XX(1).AND.XDOT.LT.0..AND.ZDOT.GT.0.).OR.
                     1   (Y.LE.YY(1).AND.YDOT.LT.0.).OR.
                     2(X.GE.XX(II).AND.XDOT.GE.0..AND.ZDOT.GT.0.).OR.
                     3   (Y.GE.YY(JJ).AND.YDOT.GT.0.).OR.
                     4   (Z.GE.ZZ(KK).AND.ZDOT.GT.0.))GO TO 700
                C
ISN 0145              IF(SKPRFL.EQ.1) GO TO 538
ISN 0147              IF(((Y.LE.(YY(MBC)-.5*Z)).AND.(Y.GT.(YY(MBC)-.5*ZZ(KUK)))).OR.
                     1((Y.GE.(YY(MBD)+.5*Z)).AND.(Y.LT.(YY(MBD)+.5*ZZ(KUK))))
                     2.AND.X.GE.XX(ILX).AND.X.LE.XX(IUX)) GO TO 600
ISN 0149        538   CONTINUE
ISN 0150              IF (Z.NE.0..OR .ZDOT.GE.0.) GO TO 540
ISN 0152              ZDOT=-ZDOT
ISN 0153              IF (NPRINT.EQ.3) WRITE(M,888) KSTEP,X,Y,Z,XDOT,YDOT,ZDOT,IGOUT,
                     1 JGOUT,KGOUT,PHI
ISN 0155              GO TO 590
ISN 0156        540   CONTINUE
                C
ISN 0157              IF (KSTEP.EQ.0) GO TO 500
ISN 0159              PHIOLD=PHI
ISN 0160              CALL INTERP
ISN 0161              IF(IGOUT.LT.1.OR.IGOUT.GT.IIA.OR.JGOUT.LT.1.OR.JGOUT.GT.JJA.OR.
                     1KGOUT.LT.1.OR.KGOUT.GT.KKA) GO TO 330
ISN 0163              IF(NTIME.LT.1.OR.NTIME.GT.6) GO TO 580
                C
ISN 0165              IF(NTIME.NE.1.AND.NTIME.NE.2) GO TO 560
ISN 0167              XDOTS=XDOT**2 + PHIOLD-PHI
ISN 0168              IF(XDOTS.EQ.0.) XDOT=0.
ISN 0170              IF(XDOTS.GT.0..AND.XDOT.NE.0.) XDOT=SQRT(XDOTS)*SIGN(1.,XDOT)
ISN 0172              IF(XDOTS.LT.0..AND.XDOT.NE.0.) XDOT=-XDOT
ISN 0174              IF(NPRINT.EQ.3.AND.XDOTS.LT.0) WRITE(M,888) KSTEP,X,Y,Z,XDOT,YDOT,
                     1 ZDOT,IGOUT,JGOUT,KGOUT,PHI
                C
ISN 0176        560   IF(NTIME.NE.3.AND.NTIME.NE.4) GO TO 570
ISN 0178              YDOTS=YDOT**2 + PHIOLD-PHI
ISN 0179              IF(YDOTS.EQ.0.) YDOT=0.
ISN 0181              IF(YDOTS.GT.0..AND.YDOT.NE.0.) YDOT=SQRT(YDOTS)*SIGN(1.,YDOT)
ISN 0183              IF(YDOTS.LT.0..AND.YDOT.NE.0.) YDOT=-YDOT
ISN 0185              IF(NPRINT.EQ.3.AND.YDOTS.LT.0) WRITE(M,888) KSTEP,X,Y,Z,XDOT,YDOT,
                     1 ZDOT,IGOUT,JGOUT,KGOUT,PHI
                C
ISN 0187        570   IF(NTIME.NE.5.AND.NTIME.NE.6) GO TO 590
ISN 0189              ZDOTS=ZDOT**2 + PHIOLD-PHI
ISN 0190              IF(ZDOTS.EQ.0.) ZDOT=0.
ISN 0192              IF(ZDOTS.GT.0..AND.ZDOT.NE.0.) ZDOT=SQRT(ZDOTS)*SIGN(1.,ZDOT)
ISN 0194              IF(ZDOTS.LT.0..AND.ZDOT.NE.0.) ZDOT=-ZDOT
ISN 0196              IF(NPRINT.EQ.3.AND.ZDOTS.LT.0) WRITE(M,888) KSTEP,X,Y,Z,XDOT,YDOT,
                     1 ZDOT,IGOUT,JGOUT,KGOUT,PHI
ISN 0198              GO TO 590
```

$Y < 0 + .5(Z)^{+}$

```
                C
ISN 0199        580   WRITE(M,997) NTIME
ISN 0200        997   FORMAT(////1X,17HTROUBLE - NTIME =,I3,19H = OUT OF RANGE 1-6)
ISN 0201              WRITE(M,887) KSTEP,X,Y,Z,XDOT,YDOT,ZDOT,IGOUT,JGOUT,KGOUT,PHI,SAVE
ISN 0202        887   FORMAT( 9X,I5,1P6E11.3,3I6,E11.3,'SAVE=',E18.10)
ISN 0203              STOP
                C
ISN 0204        590   CALL INTERP
ISN 0205              IF(IGOUT.LT.1.OR.IGOUT.GT.IIA.OR.JGOUT.LT.1.OR.JGOUT.GT.JJA.OR.
                     1KGOUT.LT.1.OR.KGOUT.GT.KKA) GO TO 330
ISN 0207              IF(NPRINT.EQ.3) WRITE(M,888) KSTEP,X,Y,Z,XDOT,YDOT,ZDOT,IGOUT,
                     1 JGOUT,KGOUT,PHI
ISN 0209              GO TO 500
                C
                C PARTICLE IS ABSORBED
ISN 0210        600   CONTINUE
ISN 0211              IF(NPRINT.NE.2.AND.NPRINT.NE.3) GO TO 1002
ISN 0213              FATE(1)=END1(1)
ISN 0214              FATE(2)=END1(2)
ISN 0215              GO TO 750
                C
                C PARTICLE ESCAPES
                C
ISN 0216        700   CONTINUE
ISN 0217              IF(NPRINT.EQ.1) GO TO 720
ISN 0219              IF(NPRINT.NE.2.AND.NPRINT.NE.3) GO TO 740
ISN 0221              FATE(1)=END2(1)
ISN 0222              FATE(2)=END2(2)
ISN 0223              GO TO 740
ISN 0224        720   WRITE(M,982) KE,JE,KB,JB,KA,JA,BE1,AL1,EV,PVOLTS
ISN 0225        740   NOESC=NOESC + 1
ISN 0226              IF(ME.EQ.0) GO TO 750
                C
ISN 0228              CSANGL=ZDOT/SQRT(XDOT**2+YDOT**2+ZDOT**2)
ISN 0229              XPON=-2.*XMACH*SQRT(E)*CSANGL - E - XMACH**2
ISN 0230              COEFA=SPEED**2/FLOAT(NUMBER)
ISN 0231              IF(ABS(XPON).GT.36.) GO TO 1000
ISN 0233              ADD =COEFA*EXP(XPON)
ISN 0234              DENS=DENS + ADD
                C
ISN 0235        750   IF(NPRINT.NE.2.AND.NPRINT.NE.3) GO TO 1002
ISN 0237              WRITE(M,889) FATE,KSTEP,X,Y,Z,XDOT,YDOT,ZDOT,IGOUT,JGOUT,KGOUT,PHI
ISN 0238        889   FORMAT(1X,2A4,I5,1P6E11.3,3I6,E11.3)
                C
ISN 0239        1002  CONTINUE
ISN 0240              IF(MOSTPS.GE.KSTEP) GO TO 1000
ISN 0242              KES=KE
ISN 0243              JES=JE
ISN 0244              KBS=KB
ISN 0245              JBS=JB
ISN 0246              KAS=KA
ISN 0247              JAS=JA
ISN 0248              MOSTPS=KSTEP
ISN 0249        1000  CONTINUE
                C
                C END OF SUM OVER ANGLES
                C
ISN 0250              FRACT=FLOAT(NOESC)/FLOAT(NUMBER)
```

```
                C
ISN 0251              WRITE(M,978) NOESC,NUMBER,FRACT,EV,DENS
ISN 0252        978   FORMAT(/1X,16HRATIO ESCAPING =,I5, 7H OUT OF,I5,14H OR A FRACTION,
                     1 F13.8,14H AT ENERGY E =,F13.8, 6H VOLTS,4X,6H(DENS=,1PE14.4,1H))
                C
ISN 0253              IF(NPRINT.EQ.0) GO TO 800
ISN 0255              IF(ME.NE.0) WRITE(M,976)
ISN 0257        976   FORMAT(1X,80HDENS IS THE SUM OF ADD=SPEED**2*EXP(XPON)/NUMBER OVER
                     1 A HEMISPHERE OF DIRECTIONS//)
                C
ISN 0258        800   IF(ME.EQ.0) GO TO 1001
ISN 0260              COEFE=2./(1. - CE)**2/FLOAT(ME)
ISN 0261              IF(XMACH.GT.1.) COEFE=COEFE*XMACH**2
ISN 0263              DENST=DENST + COEFE*DENS
ISN 0264        1001  CONTINUE
                C
ISN 0265              IF(ME.EQ.0) DENST=SPEED**2*FRACT
                C
                C     TRAJECTORY WITH MOST STEPS. PRINT K AND J INDICES.
                C
ISN 0267              WRITE(M,972) MOSTPS,KES,JES,KBS,JBS,KAS,JAS
ISN 0268        972   FORMAT(///1X,I5,3(I3,I2),29H =MOSTPS, KE,JE, KB,JB, KA,JA)
ISN 0269              WRITE(M,974) XSAVE,YSAVE,PHISAV,DENST,PARTCL
ISN 0270        974   FORMAT(/1X,26HAT DIMENSIONLESS X,Y,PHI =,3F12.6,1H,,5X,1PE16.4,
                     1  33H = NORMALIZED CURRENT DENSITY FOR,2A5//)
ISN 0271              RETURN
ISN 0272              END
```

```
          COMPILER OPTIONS - NAME=  MAIN,OPT=02,LINECNT=60,SIZE=0000K,
                             SOURCE,EBCDIC,NOLIST,NODECK,LOAD,MAP,NOEDIT,NOID,NOXREF
ISN 0002                SUBROUTINE INTERP
                  C
                  C     INTERPOLATION WITHIN GRID
                  C
ISN 0003                COMMON/BK/IIM,IIP,JJM,JJP,KK,NTOT,IV,JV,II,JJ,M,N,VP(30),
                       1XYZ(2080,3),VV(30,20,10),XP(30),XM(10),YP(20),YM(10),ZZ(10),
                       2XX(40),YY(30),ILX,IUX,KUK,MBC,MBD,VRF,NFPS,SKPRFL,SKPLST
ISN 0004                COMMON/ORB/XDOT,YDOT,ZDOT,X1,X2,Y1,Y2,Z1,Z2,X,Y,Z,PHI,NTIME,SAVE
ISN 0005                COMMON/INTER/INT,IIA,JJA,KKA,IGOUT,JGOUT,KGOUT,XA,YA,ZA,
                       1XI(30),YJ(20),ZK(10)
                  C
ISN 0006                IGOUT=0
ISN 0007                JGOUT=0
ISN 0008                KGOUT=0
ISN 0009                NCH=0
                  C
ISN 0010                XA=X
ISN 0011                YA=Y
ISN 0012                ZA=Z
                  C
                  C     LOCATE XA
                  C
ISN 0013                IF(XA.EQ.XI(IIA)) IG=IIA-1
ISN 0015                IF(XA.EQ.XI(IIA)) GO TO 103
ISN 0017                IF(INT.NE.0)      GO TO 100
                  C
ISN 0019                DO 10 I=2,IIA
ISN 0020                IG=I-1
ISN 0021                IF(XA.LT.XI(I))   GO TO 103
ISN 0023          10    CONTINUE
                  C
ISN 0024          100   IF(XA.GE.XI(IG+1)) GO TO 102
ISN 0026                IF(XA.GE.XI(IG))   GO TO 104
ISN 0028          101   IG=IG-1
ISN 0029                IF(XA.LT.XI(IG))   GO TO 101
ISN 0031                GO TO 103
ISN 0032          102   IG=IG+1
ISN 0033                IF(XA.GE.XI(IG+1)) GO TO 102
                  C
ISN 0035          103   NCH=1
ISN 0036          104   CONTINUE
                  C
                  C     ACCEPT IF XI(IG) LESS THAN OR EQUAL TO XA LESS THAN XI(IG+1).
                  C
                  C
                  C     LOCATE YA
                  C
ISN 0037                IF(YA.EQ.YJ(JJA)) JG=JJA-1
ISN 0039                IF(YA.EQ.YJ(JJA)) GO TO 203
ISN 0041                IF(INT.NE.0)      GO TO 200
                  C
ISN 0043                DO 20 J=2,JJA
ISN 0044                JG=J-1
ISN 0045                IF(YA.LT.YJ(J))   GO TO 203
ISN 0047          20    CONTINUE
                  C
```

```
ISN 0048      200   IF(YA.GE.YJ(JG+1)) GO TO 202
ISN 0050            IF(YA.GE.YJ(JG))   GO TO 204
ISN 0052      201   JG=JG-1
ISN 0053            IF(YA.LT.YJ(JG))   GO TO 201
ISN 0055            GO TO 203
ISN 0056      202   JG=JG+1
ISN 0057            IF(YA.GE.YJ(JG+1)) GO TO 202
                C
ISN 0059      203   NCH=1
ISN 0060      204   CONTINUE
                C
                C   ACCEPT IF YJ(JG) LESS THAN OR EQUAL TO YA LESS THAN YJ(JG+1).
                C
                C
                C   LOCATE ZA
                C
ISN 0061            IF(ZA.EQ.ZK(KKA)) KG=KKA-1
ISN 0063            IF(ZA.EQ.ZK(KKA)) GO TO 303
ISN 0065            IF(INT.NE.0)      GO TO 300
                C
ISN 0067            DO 30 K=2,KKA
ISN 0068            KG=K-1
ISN 0069            IF(ZA.LT.ZK(K))    GO TO 303
ISN 0071      30    CONTINUE
                C
ISN 0072      300   IF(ZA.GE.ZK(KG+1)) GO TO 302
ISN 0074            IF(ZA.GE.ZK(KG))   GO TO 304
ISN 0076      301   KG=KG-1
ISN 0077            IF(ZA.LT.ZK(KG))   GO TO 301
ISN 0079            GO TO 303
ISN 0080      302   KG=KG+1
ISN 0081            IF(ZA.GE.ZK(KG+1)) GO TO 302
                C
ISN 0083      303   NCH=1
ISN 0084      304   CONTINUE
                C
                C   ACCEPT IF ZK(KG) LESS THAN OR EQUAL TO ZA LESS THAN ZK(KG+1).
                C
                C   LOCATE LINE AND BOX
                C
ISN 0085            X1=XI(IG)
ISN 0086            Y1=YJ(JG)
ISN 0087            Z1=ZK(KG)
ISN 0088            X2=XI(IG+1)
ISN 0089            Y2=YJ(JG+1)
ISN 0090            Z2=ZK(KG+1)
                C
ISN 0091            IF(X.NE.X1.OR.XDOT.GE.0.) GO TO 400
ISN 0093            IG=IG-1
ISN 0094            X2=X1
ISN 0095            X1=XI(IG)
                C
ISN 0096      400   IF(Y.NE.Y1.OR.YDOT.GE.0.) GO TO 500
ISN 0098            JG=JG-1
ISN 0099            Y2=Y1
ISN 0100            Y1=YJ(JG)
                C
ISN 0101      500   IF(Z.NE.Z1.OR.ZDOT.GE.0.) GO TO 600
```

```
ISN 0103          KG=KG-1
ISN 0104          Z2=Z1
ISN 0105          Z1=ZK(KG)
            C
ISN 0106    600   PHI=VV(IG,JG,KG)
ISN 0107          IGOUT=IG
ISN 0108          JGOUT=JG
ISN 0109          KGOUT=KG
ISN 0110          RETURN
ISN 0111          END
```

```
        COMPILER OPTIONS - NAME=  MAIN,OPT=02,LINECNT=60,SIZE=0000K,                    DATE
                           SOURCE,EBCDIC,NOLIST,NODECK,LOAD,MAP,NOEDIT,NOID,NOXREF
ISN 0002                SUBROUTINE POWER
                  C
                  C CURRENT DENSITIES AND POWER LOSS
                  C
ISN 0003                COMMON/BK/IIM,IIP,JJM,JJP,KK,NTOT,IV,JV,II,JJ,M,N,VP(30),
                       1XYZ(2080,3),VV(30,20,10),XP(30),XM(10),YP(20),YM(10),ZZ(10),
                       2XX(40),YY(30),ILX,IUX,KUK,MBC,MBD,VRF,NFPS,SKPRFL,SKPLST
ISN 0004                COMMON/CP/NPRINT,NPTS,MA,MB,ME,KMAX,XPT,YPT,AL1,BE1,EV,SMACH,
                       1 TVOLTS,CUR,XMETER
ISN 0005                COMMON/CD/PVOLTS,XMACH,DENST,NN,PARTCL(2),PART1(2),PART2(2)
ISN 0006                DIMENSION A(2)
ISN 0007                IF(NPTS.EQ.0.OR.MA.EQ.0) WRITE(M,997) XPT,YPT,AL1,BE1,EV
ISN 0009          997   FORMAT(/1X,  9HX AND Y =,2F10.5,20X,19HALPHA,BETA,ENERGY =,3F20.5)
ISN 0010                IF(NPRINT.EQ.0) WRITE(M,990)
ISN 0012                IF(NPRINT.EQ.1) WRITE(M,991)
ISN 0014                IF(NPRINT.EQ.2) WRITE(M,992)
ISN 0016                IF(NPRINT.EQ.3) WRITE(M,993)
ISN 0018          990   FORMAT(/38H NPRINT=0 MEANS NO TRAJECTORY PRINTING)
ISN 0019          991   FORMAT(/53H NPRINT=1 PRINT INDICES OF ESCAPING TRAJECTORIES ONLY)
ISN 0020          992   FORMAT(/56H NPRINT=2 PRINT FIRST AND LAST STEPS OF ALL TRAJECTORIE
                       1S)
ISN 0021          993   FORMAT(/52H NPRINT=3 MEANS PRINT EVERY STEP OF ALL TRAJECTORIES)
                  C
ISN 0022                IF(TVOLTS.EQ.0.) RETURN
                  C
ISN 0024                XMACH=SMACH
                  C
                  C NON-DIMENSIONALIZE THE POTENTIAL DISTRIBUTION.  THEN RESTORE AT END.
                  C
ISN 0025                DO 200 K=1,KK
ISN 0026                DO 200 J=1,JJ
ISN 0027                DO 200 I=1,II
ISN 0028                VV(I,J,K )=VV(I,J,K)/TVOLTS
ISN 0029          200   CONTINUE
                  C
                  C DEFINE THE PANEL POINTS AT WHICH THE CURRENT AND POWER IS EVALUATED
                  C
                  C CASE OF A SINGLE POINT
                  C
ISN 0030                IF(NPTS.EQ.0.OR.MA.EQ.0) COEFM = XMETER**2
                  C
                  C CASE OF MULTIPLE POINTS FOR INTEGRATION OVER PANEL SUB-AREAS
                  C
ISN 0032                JVM=1
ISN 0033                IVM=1
ISN 0034                IF(JV.GT.1) JVM=JV-1
ISN 0036                IF(IV.GT.1) IVM=IV-1
ISN 0038                NA=0
ISN 0039                NAREAS=IVM*JVM
ISN 0040                TPOWER=0.
ISN 0041                TCURNT=0.
ISN 0042                TAREA=0.
ISN 0043                NN=0
ISN 0044                DO 500 J=1,JVM
ISN 0045                DO 500 I=1,IVM
ISN 0046                NA=NA+1
```

```
ISN 0047            NP=0
ISN 0048            IF(NPTS.EQ.0.OR.MA.EQ.0) GO TO 250
ISN 0050            PO = 0
ISN 0051            CU = 0
ISN 0052            A(1)=-1./SQRT(3.)
ISN 0053            A(2)=-A(1)
ISN 0054            GO TO 260
ISN 0055      250   CONTINUE
ISN 0056            JXMAX=1
ISN 0057            JYMAX=1
ISN 0058            KMAX=1
ISN 0059            GO TO 270
ISN 0060      260   JXMAX=2
ISN 0061            JYMAX=2
ISN 0062      270   CONTINUE
ISN 0063            DO 400 KY=1,KMAX
ISN 0064            DO 400 KX=1,KMAX
ISN 0065            DO 400  JY=1,JYMAX
ISN 0066            DO 400  JX=1,JXMAX
ISN 0067            NP=NP+1
ISN 0068            NN=NN+1
ISN 0069            IF(NPTS.EQ.0.OR.MA.EQ.0) GO TO 300
ISN 0071            CX=(A(JX) + FLOAT(2*KX - 1 - KMAX))/FLOAT(KMAX)
ISN 0072            CY=(A(JY) + FLOAT(2*KY - 1 - KMAX))/FLOAT(KMAX)
ISN 0073            XPT=(XP(I+1)-XP(I))/2.*CX + (XP(I+1)+XP(I))/2.
ISN 0074            YPT = (YP(J+1)-YP(J))/2.*CY + (YP(J+1)+YP(J))/2.
ISN 0075            COEF = (XP(I+1)-XP(I))*(YP(J+1)-YP(J))
ISN 0076            AREA = COEF * XMETER**2
ISN 0077            COEFM = AREA/4./FLOAT(KMAX**2)
                C
                C
                C COMPUTE EACH CURRENT DENSITY AND MULTIPLY BY LOCAL POTENTIAL TO
                C EVALUATE POWER DENSITY
ISN 0078      300   CALL DEN
ISN 0079            DENCUR=DENST*CUR
ISN 0080            POWDEN=PVOLTS*DENCUR
ISN 0081            IF(MA.EQ.0) GO TO 600
ISN 0083            XPTM=XPT*XMETER
ISN 0084            YPTM=YPT*XMETER
ISN 0085            XPM=XP(I)*XMETER
ISN 0086            XPPM=XP(I+1)*XMETER
ISN 0087            YPM=YP(J)*XMETER
ISN 0088            YPPM=YP(J+1)*XMETER
                C
ISN 0089      995   FORMAT (6X,12HAT POINT NO.,I3,10H, WITH X =,F10.5,13H METERS,  Y =
                   1,F10.5,27H METERS,  AND COEFFICIENT =,F10.5,14H SQUARE METERS)
                C
ISN 0090            IF(NPTS.GT.0.AND.MA.GT.0) WRITE(M,994) NA,XPM,XPPM,YPM,YPPM
ISN 0092      994   FORMAT( /5X,16H IN SUB-AREA NO.,I3,1X,17HBOUNDED BY X IN (,
                   1 F10.5,3H TO,F10.5, 9H) METERS,,4X,13HAND BY Y IN (,
                   2 F10.5,3H TO,F10.5, 8H) METERS)
                C
ISN 0093            WRITE (M,995) NP,XPTM,YPTM,COEFM
ISN 0094            WRITE(M,988) PVOLTS,DENCUR,POWDEN,PARTCL
ISN 0095      988   FORMAT(6X,53HTHE VOLTAGE, CURRENT DENSITY, AND POWER DENSITY ARE =
                   1/6X,1PE16.4,6H VOLTS,4X,E16.4,23H AMP/(SQ-METER),    AND,E16.4,
                   2 24H WATT/(SQ-METER),    FOR,2A5//)
ISN 0096            IF(NPTS.EQ.0) GO TO 600
```

$4 \times 4 \times 4 \times 4 \times 2 \times$

LTRJ = NN/(MA·MB·ME·4

NIMB = 3.8 *

LTRJCT = NN/NIMB

```
ISN 0098              CU = CU + COEFM*DENCUR
ISN 0099              PO = PO + COEFM * POWDEN
ISN 0100        400   CONTINUE
ISN 0101              AVCD = CU/AREA
ISN 0102              AVPD = PO/AREA
                C
ISN 0103              WRITE(M,986) NA,CU,PO,PARTCL
ISN 0104              WRITE(M,984) NA,AREA,AVCD,AVPD
ISN 0105        984   FORMAT(  1X,18HIN SUB-AREA NUMBER,I3,8H OF AREA,1PE16.4,15H SQUARE
                     1 METERS,/52H THE AVERAGE CURRENT DENSITY AND POWER DENSITY ARE =,
                     2 E16.4,19H AMP/(SQ-METER) AND,E16.4,16H WATT/(SQ-METER))
ISN 0106        986   FORMAT( /1X,18HIN SUB-AREA NUMBER,I3,28H THE CURRENT AND POWER ARE
                     1 =,1PE16.4,12H AMP,    AND,E16.4,14H WATTS,    FOR,2A5)
                C
ISN 0107              TAREA=TAREA + AREA
ISN 0108              TCURNT = TCURNT + CU
ISN 0109              TPOWER = TPOWER + PO
ISN 0110        500   CONTINUE
                C
ISN 0111              WRITE(M,982) TCURNT,TPOWER,PARTCL
ISN 0112        982   FORMAT(///1X,34HTOTAL CURRENT AND POWER LOSS ARE =,1PE16.4,
                     1 12H AMP,    AND,E16.4,13H WATT,    FOR,2A5)
ISN 0113              AVCD=TCURNT/TAREA
ISN 0114              AVPD=TPOWER/TAREA
ISN 0115              WRITE(M,980) TAREA,AVCD,AVPD
ISN 0116        980   FORMAT(/1X,26HWITH A TOTAL PANEL AREA OF,1PE16.4,15H SQUARE METERS
                     1,/1X,51HTHE AVERAGE CURRENT DENSITY AND POWER DENSITY ARE =,
                     2 E16.4,19H AMP/(SQ-METER) AND,E16.4,16H WATT/(SQ-METER))
                C
                C
                C     RESTORE POTENTIAL DISTRIBUTION TO DIMENSIONAL VALUES
                C
ISN 0117          600 CONTINUE
ISN 0118              DO 700 K=1,KK
ISN 0119              DO 700 J=1,JJ
ISN 0120              DO 700 I=1,II
ISN 0121              VV(I,J,K)=VV(I,J,K)*TVOLTS
ISN 0122        700   CONTINUE
ISN 0123              RETURN
ISN 0124              END
```

```
        COMPILER OPTIONS - NAME=  MAIN,OPT=02,LINECNT=60,SIZE=0000K,
                           SOURCE,EBCDIC,NOLIST,NODECK,LOAD,MAP,NOEDIT,NOID,NOXREF
ISN 0002                SUBROUTINE LIST(LST,IP)
ISN 0003                COMMON/BK/IIM,IIP,JJM,JJP,KK,NTOT,IV,JV,II,JJ,M,N,VP(30),
                       1XYZ(2080,3),VV(30,20,10),XP(30),XM(10),YP(20),YM(10),ZZ(10),
                       2XX(40),YY(30),ILX,IUX,KUK,MBC,MBD,VRF,NFPS,SKPRFL,SKPLST
ISN 0004                COMMON/FLD/X(2080,2),COEF(2080,7),INDX(2080,6),SKPCO
ISN 0005                DIMENSION KOUT(5),XOUT(5),YOUT(5),ZOUT(5)
ISN 0006                DO 500 LINE=1,60
ISN 0007                DO 200 NP=1,5
ISN 0008                KP=LINE + (NP-1)*60 + (IP-1) * 300
ISN 0009                IF(KP.GT.NTOT.AND.NP.EQ.1) RETURN
ISN 0011                IF(KP .GT. NTOT) GO TO 300
ISN 0013                NMAX=NP
ISN 0014                KOUT(NP) = KP
ISN 0015                IF(LST.EQ.1) XOUT(NP) = X(KP,1)
ISN 0017                IF(LST .EQ. 2) XOUT(NP) =XYZ(KP,1)
ISN 0019                IF(LST .EQ. 2) YOUT(NP)=XYZ(KP,2)
ISN 0021                IF(LST .EQ. 2) ZOUT(NP) =XYZ(KP,3)
ISN 0023        200     CONTINUE
ISN 0024        300     GO TO (400,450),LST
ISN 0025        400     WRITE(M,1000) (KOUT(NP),XOUT(NP), NP=1,NMAX)
ISN 0026        1000    FORMAT(5(I8,F16.8))
ISN 0027                GO TO 500
ISN 0028        450     WRITE(M,3000) (KOUT(NP),XOUT(NP),YOUT(NP),ZOUT(NP),NP=1,NMAX)
ISN 0029        3000    FORMAT(5(I8,3F6.2))
ISN 0030        500     CONTINUE
ISN 0031                RETURN
ISN 0032                END
```

```
        COMPILER OPTIONS - NAME=  MAIN,OPT=02,LINECNT=60,SIZE=0000K,
                           SOURCE,EBCDIC,NOLIST,NODECK,LOAD,MAP,NOEDIT,NOID,NOXREF
ISN 0002                SUBROUTINE RELAX
                  C     POINT-SUCCESSIVE OVERRELAXATION METHOD
ISN 0003                COMMON/BK/IIM,IIP,JJM,JJP,KK,NTOT,IV,JV,II,JJ,M,N,VP(30),
                       1XYZ(2080,3),VV(30,20,10),XP(30),XM(10),YP(20),YM(10),ZZ(10),
                       2XX(40),YY(30),ILX,IUX,KUK,MBC,MBD,VRF,NFPS,SKPRFL,SKPLST
ISN 0004                COMMON/FLD/X(2080,2),COEF(2080,7),INDX(2080,6),SKPCO
ISN 0005                OMEGA=1.9
ISN 0006                EPS = 1.E-3
ISN 0007                ITMAX=2000
ISN 0008                ITR=0
ISN 0009                IPROLD=0
ISN 0010                IGO=1
ISN 0011          200   ITR=ITR+1
ISN 0012                DELTAM=0.
ISN 0013                DO 500 N=1,NTOT
ISN 0014                IF(X(N,2).EQ.1)GO TO 500
ISN 0016                X1=X(N,1)
                  C
ISN 0017                FN=COEF(N,1)/COEF(N,7)
ISN 0018                FS=COEF(N,2)/COEF(N,7)
ISN 0019                FE=COEF(N,3)/COEF(N,7)
ISN 0020                FW=COEF(N,4)/COEF(N,7)
ISN 0021                FU=COEF(N,5)/COEF(N,7)
ISN 0022                FD=COEF(N,6)/COEF(N,7)
                  C
ISN 0023                NN=INDX(N,1)
ISN 0024                NS=INDX(N,2)
ISN 0025                NE=INDX(N,3)
ISN 0026                NW=INDX(N,4)
ISN 0027                NU=INDX(N,5)
ISN 0028                ND=INDX(N,6)
                  C
ISN 0029                SUM=0.
ISN 0030                IF(NN.GT.0) SUM = SUM+FN*X(NN,1)
ISN 0032                IF(NS.GT.0) SUM = SUM+FS*X(NS,1)
ISN 0034                IF(NE.GT.0) SUM = SUM+FE*X(NE,1)
ISN 0036                IF(NW.GT.0) SUM = SUM+FW*X(NW,1)
ISN 0038                IF(ND.GT.0) SUM = SUM+FD*X(ND,1)
ISN 0040                IF(NU.GT.0) SUM = SUM+FU*X(NU,1)
                  C
ISN 0042                X(N,1) = OMEGA*SUM+(1.-OMEGA)*X1
ISN 0043                DELTA = ABS(X(N,1)-X1)
ISN 0044                IF(ABS(X1).GT.1.E-10) DELTA=ABS((X(N,1)-X1)/X1)
ISN 0046                IF(DELTA .GT. DELTAM) DELTAM=DELTA
ISN 0048          500   CONTINUE
ISN 0049                IF(ITR.GT.ITMAX) WRITE(M,8888) ITR
ISN 0051                IF(ITR.GT.ITMAX) GO TO 700
ISN 0053         8888   FORMAT(////10H MORE THAN, I4,11H ITERATIONS)
ISN 0054                IPR=ITR/500
ISN 0055                IF(IPR.LE.IPROLD) GO TO 600
ISN 0057                IPROLD=IPR
ISN 0058                GO TO 800
                  C
ISN 0059          600   IF(DELTAM.GT.EPS) GO TO 200
                  C
                  C     ITERATION FINISHED.  PRINT AND EXIT.
```

```
              C
ISN 0061      700    IGO=2
ISN 0062      800    NFPP=(NTOT/300) +1
ISN 0063             DO 900 IP=1,NFPP
ISN 0064             WRITE(M,7777) ITR,EPS,DELTAM,OMEGA
ISN 0065      7777   FORMAT(15H1SOLUTION AFTER,I6,2X,25HITERATIONS WITH TOLERANCE,
                    1 F12.8,8X,18HMAXIMUM DIFFERENCE,F12.8,8X,6HOMEGA=,F8.5)
ISN 0066             CALL LIST(1,IP)
ISN 0067      900    CONTINUE
              C
ISN 0068             GO TO (600,1000),IGO      IF(IGO.EQ.1) GO TO 600
ISN 0069      1000   RETURN
ISN 0070             END
```

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LEVEL 21.8 ( JUN 74 )                                   OS/360  FORTRAN H

          COMPILER OPTIONS - NAME=  MAIN,OPT=02,LINECNT=60,SIZE=0000K,
                             SOURCE,EBCDIC,NOLIST,NODECK,LOAD,MAP,NOEDIT,NOID,NOXREF
  ISN 0002                 SUBROUTINE FIND(I,J,K)
  ISN 0003                 COMMON/BK/IIM,IIP,JJM,JJP,KK,NTOT,IV,JV,II,JJ,M,N,VP(30),
                          1XYZ(2080,3),VV(30,20,10),XP(30),XM(10),YP(20),YM(10),ZZ(10),
                          2XX(40),YY(30),ILX,IUX,KUK,MBC,MBD,VRF,NFPS,SKPRFL,SKPLST
  ISN 0004                 IIJJ=II*JJ
  ISN 0005                 K=N/IIJJ+1
  ISN 0006                 IF(K .GE. 2 .AND. MOD(N,IIJJ) .EQ. 0) K=K-1
  ISN 0008                 NKIJ=N - IIJJ*(K-1)
  ISN 0009                 J=NKIJ/II+1
  ISN 0010                 IF(J .GE. 2 .AND. MOD(NKIJ,II) .EQ. 0) J=J-1
  ISN 0012                 I=NKIJ - II*(J-1)
  ISN 0013                 RETURN
  ISN 0014                 END
```

```
          COMPILER OPTIONS - NAME=  MAIN,OPT=02,LINECNT=60,SIZE=0000K,
                             SOURCE,EBCDIC,NOLIST,NODECK,LOAD,MAP,NOEDIT,NOID,NOXREF
ISN 0002                SUBROUTINE ARRAY
ISN 0003                COMMON/BK/IIM,IIP,JJM,JJP,KK,NTOT,IV,JV,II,JJ,M,N,VP(30),
                       1XYZ(2080,3),VV(30,20,10),XP(30),XM(10),YP(20),YM(10),ZZ(10),
                       2XX(40),YY(30),ILX,IUX,KUK,MBC,MBD,VRF,NFPS,SKPRFL,SKPLST
ISN 0004                COMMON/FLD/X(2080,2),COEF(2080,7),INDX(2080,6),SKPCO
ISN 0005                COMMON/CCC/CN,CS,CE,CW,CU,CD,CC,NN,NS,NE,NW,NU,ND
                  C
                  C     COEFFICIENT ARRAY = COEF(N,7), WHERE
                  C     COEF(N,1)=CN (NORTH=+Y NEIGHBOR)
                  C     COEF(N,2)=CS (SOUTH=-Y NEIGHBOR)
                  C     COEF(N,3)=CE ( EAST=+X NEIGHBOR)
                  C     COEF(N,4)=CW ( WEST=-X NEIGHBOR)
                  C     COEF(N,5)=CU (    UP=+Z NEIGHBOR)
                  C     COEF(N,6)=CD ( DOWN=-Z NEIGHBOR)
                  C     COEF(N,7)=CC (      = CENTRAL POINT)
                  C
                  C     SAVE COEFFICIENTS AND INDICES
                  C
ISN 0006                COEF(N,1)=CN
ISN 0007                COEF(N,2)=CS
ISN 0008                COEF(N,3)=CE
ISN 0009                COEF(N,4)=CW
ISN 0010                COEF(N,5)=CU
ISN 0011                COEF(N,6)=CD
ISN 0012                COEF(N,7)=CC
                  C
ISN 0013                INDX(N,1)=NN
ISN 0014                INDX(N,2)=NS
ISN 0015                INDX(N,3)=NE
ISN 0016                INDX(N,4)=NW
ISN 0017                INDX(N,5)=NU
ISN 0018                INDX(N,6)=ND
ISN 0019                IF(SKPCO.EQ.1) GO TO 20
ISN 0021                WRITE(M,1000) ND,CD,NS,CS,NW,CW,N,CC,NE,CE,NN,CN,NU,CU
ISN 0022          1000  FORMAT(/7(1X,1H(,I4,2H)=,1PE10.4))
ISN 0023            20  CONTINUE
ISN 0024                RETURN
ISN 0025                END
```

```
          COMPILER OPTIONS - NAME=  MAIN,OPT=02,LINECNT=60,SIZE=0000K,
                             SOURCE,EBCDIC,NOLIST,NODECK,LOAD,MAP,NOEDIT,NOID,NOXREF
ISN 0002                SUBROUTINE CUD(MP,C,A)
ISN 0003                COMMON/BK/IIM,IIP,JJM,JJP,KK,NTOT,IV,JV,II,JJ,M,N,VP(30),
                       1XYZ(2080,3),VV(30,20,10),XP(30),XM(10),YP(20),YM(10),ZZ(10),
                       2XX(40),YY(30),ILX,IUX,KUK,MBC,MBD,VRF,NFPS,SKPRFL,SKPLST
ISN 0004                COMMON/CCC/CN,CS,CE,CW,CU,CD,CC,NN,NS,NE,NW,NU,ND
ISN 0005                NF(IX,JX,KX) = IX+II*(JX-1) + II*JJ*(KX-1)
ISN 0006                A=0.
ISN 0007                C=0.
ISN 0008                CALL FIND(I,J,K)
ISN 0009                IF(I .EQ. 1) GO TO 100
ISN 0011                IF(I .EQ. II) GO TO 200
ISN 0013                NH=NF(I+1,J,K)
ISN 0014                NL=NF(I-1,J,K)
ISN 0015                DX=XYZ(NH,1) - XYZ(NL,1)
ISN 0016                GO TO 300
ISN 0017          100   NH=NF(2,J,K)
ISN 0018                DX=XYZ(NH,1) - XYZ(N,1)
ISN 0019                GO TO 300
ISN 0020          200   NL=NF(II-1,J,K)
ISN 0021                DX=XYZ(N,1) - XYZ(NL,1)
ISN 0022          300   CONTINUE
ISN 0023                IF(J .EQ. 1) GO TO 400
ISN 0025                IF(J .EQ. JJ) GO TO 500
ISN 0027                NH=NF(I,J+1,K)
ISN 0028                NL=NF(I,J-1,K)
ISN 0029                DY=XYZ(NH,2) - XYZ(NL,2)
ISN 0030                GO TO 600
ISN 0031          400   NH=NF(I,2,K)
ISN 0032                DY=XYZ(NH,2) - XYZ(N,2)
ISN 0033                GO TO 600
ISN 0034          500   NL=NF(I,JJ-1,K)
ISN 0035                DY=XYZ(N,2) - XYZ(NL,2)
ISN 0036          600   A=DX*DY/4.
ISN 0037                IF(MP .EQ. 1) GO TO 700
ISN 0039                IF(MP .EQ. 2) GO TO 800
ISN 0041                RETURN
ISN 0042          700   NU=0
ISN 0043                IF(K .EQ. KK) RETURN
ISN 0045                NH=NF(I,J,K+1)
ISN 0046                NU=NH
ISN 0047                DZ=XYZ(NH,3) - XYZ(N,3)
ISN 0048                 GO TO 900
ISN 0049          800   ND=0
ISN 0050                IF(K .EQ. 1) RETURN
ISN 0052                NL=NF(I,J,K-1)
ISN 0053                ND=NL
ISN 0054                DZ=XYZ(N,3) - XYZ(NL,3)
ISN 0055          900   C=A/DZ
ISN 0056                RETURN
ISN 0057                END
```

```
          COMPILER OPTIONS - NAME=  MAIN,OPT=02,LINECNT=60,SIZE=0000K,
                             SOURCE,EBCDIC,NOLIST,NODECK,LOAD,MAP,NOEDIT,NOID,NOXREF
ISN 0002                SUBROUTINE CNS(MP,C,A)
ISN 0003                COMMON/BK/IIM,IIP,JJM,JJP,KK,NTOT,IV,JV,II,JJ,M,N,VP(30),
                       1XYZ(2080,3),VV(30,20,10),XP(30),XM(10),YP(20),YM(10),ZZ(10),
                       2XX(40),YY(30),ILX,IUX,KUK,MBC,MBD,VRF,NFPS,SKPRFL,SKPLST
ISN 0004                COMMON/CCC/CN,CS,CE,CW,CU,CD,CC,NN,NS,NE,NW,NU,ND
ISN 0005                NF(IX,JX,KX)=IX+II*(JX-1)+II*JJ*(KX-1)
ISN 0006                A=0.
ISN 0007                C=0.
ISN 0008                CALL FIND(I,J,K)
ISN 0009                IF(I.EQ.1) GO TO 100
ISN 0011                IF(I.EQ.II) GO TO 200
ISN 0013                NH=NF(I+1,J,K)
ISN 0014                NL=NF(I-1,J,K)
ISN 0015                DX=XYZ(NH,1) - XYZ(NL,1)
ISN 0016                GO TO 300
ISN 0017          100   NH=NF(2,J,K)
ISN 0018                DX=XYZ(NH,1) - XYZ(N,1)
ISN 0019                GO TO 300
ISN 0020          200   NL=NF(II-1,J,K)
ISN 0021                DX=XYZ(N,1) - XYZ(NL,1)
ISN 0022          300   CONTINUE
ISN 0023                IF(K.EQ.1) GO TO 400
ISN 0025                IF(K.EQ.KK) GO TO 500
ISN 0027                NH=NF(I,J,K+1)
ISN 0028                NL=NF(I,J,K-1)
ISN 0029                DZ=XYZ(NH,3) - XYZ(NL,3)
ISN 0030                GO TO 600
ISN 0031          400   NH=NF(I,J,2)
ISN 0032                DZ=XYZ(NH,3) - XYZ(N,3)
ISN 0033                GO TO 600
ISN 0034          500   NL=NF(I,J,KK-1)
ISN 0035                DZ=XYZ(N,3) - XYZ(NL,3)
ISN 0036          600   A=DX*DZ/4.
ISN 0037                IF(MP.EQ.1) GO TO 700
ISN 0039                IF(MP.EQ.2) GO TO 800
ISN 0041                RETURN
ISN 0042          700   NN=0
ISN 0043                IF(J.EQ.JJ) RETURN
ISN 0045                NH=NF(I,J+1,K)
ISN 0046                NN=NH
ISN 0047                DY=XYZ(NH,2) - XYZ(N,2)
ISN 0048                GO TO 900
ISN 0049          800   NS=0
ISN 0050                IF(J.EQ.1) RETURN
ISN 0052                NL=NF(I,J-1,K)
ISN 0053                NS=NL
ISN 0054                DY=XYZ(N,2) - XYZ(NL,2)
ISN 0055          900   C=A/DY
ISN 0056                RETURN
ISN 0057                END
```

```
          COMPILER OPTIONS - NAME=  MAIN,OPT=02,LINECNT=60,SIZE=0000K,
                             SOURCE,EBCDIC,NOLIST,NODECK,LOAD,MAP,NOEDIT,NOID,NOXREF
ISN 0002                SUBROUTINE CEW(MP,C,A)
ISN 0003                COMMON/BK/IIM,IIP,JJM,JJP,KK,NTOT,IV,JV,II,JJ,M,N,VP(30),
                       1XYZ(2080,3),VV(30,20,10),XP(30),XM(10),YP(20),YM(10),ZZ(10),
                       2XX(40),YY(30),ILX,IUX,KUK,MBC,MBD,VRF,NFPS,SKPRFL,SKPLST
ISN 0004                COMMON/CCC/CN,CS,CE,CW,CU,CD,CC,NN,NS,NE,NW,NU,ND
ISN 0005                NF(IX,JX,KX)= IX+ II*(JX-1) + II*JJ*(KX-1)
ISN 0006                A=0.
ISN 0007                C=0.
ISN 0008                CALL FIND(I,J,K)
ISN 0009                IF(J.EQ.1) GO TO 100
ISN 0011                IF(J .EQ. JJ) GO TO 200
ISN 0013                NH=NF(I,J+1,K)
ISN 0014                NL=NF(I,J-1,K)
ISN 0015                DY=XYZ(NH,2) - XYZ(NL,2)
ISN 0016                GO TO 300
ISN 0017          100   NH=NF(I,2,K)
ISN 0018                DY=XYZ(NH,2) - XYZ(N,2)
ISN 0019                GO TO 300
ISN 0020          200   NL=NF(I,JJ-1,K)
ISN 0021                DY=XYZ(N,2) - XYZ(NL,2)
ISN 0022          300   CONTINUE
ISN 0023                IF(K .EQ. 1) GO TO 400
ISN 0025                IF(K .EQ. KK) GO TO 500
ISN 0027                NH=NF(I,J,K+1)
ISN 0028                NL=NF(I,J,K-1)
ISN 0029                DZ=XYZ(NH,3) - XYZ(NL,3)
ISN 0030                GO TO 600
ISN 0031          400   NH=NF(I,J,2)
ISN 0032                DZ=XYZ(NH,3) - XYZ(N,3)
ISN 0033                GO TO 600
ISN 0034          500   NL=NF(I,J,KK-1)
ISN 0035                DZ=XYZ(N,3) - XYZ(NL,3)
ISN 0036          600   A=DY*DZ/4.
ISN 0037                IF(MP .EQ. 1) GO TO 700
ISN 0039                IF(MP .EQ. 2) GO TO 800
ISN 0041                RETURN
ISN 0042          700   NE=0
ISN 0043                IF(I.EQ.II) RETURN
ISN 0045                NH=NF(I+1,J,K)
ISN 0046                NE=NH
ISN 0047                DX=XYZ(NH,1) - XYZ(N,1)
ISN 0048                GO TO 900
ISN 0049          800   NW=0
ISN 0050                IF(I .EQ. 1) RETURN
ISN 0052                NL=NF(I-1,J,K)
ISN 0053                NW=NL
ISN 0054                DX=XYZ(N,1) - XYZ(NL,1)
ISN 0055          900   C=A/DX
ISN 0056                RETURN
ISN 0057                END
```

```
COMPILER OPTIONS - NAME=  MAIN,OPT=02,LINECNT=60,SIZE=0000K,
                   SOURCE,EBCDIC,NOLIST,NODECK,LOAD,MAP,NOEDIT,NOID,NOXREF                DATE
ISN 0002              SUBROUTINE FIELD
                C
                C     CONSTRUCTION OF COEFFICIENTS (MATRIX ELEMENTS)
                C     IN LINEAR DIFFERENCE EQUATIONS
                C     SOLUTION BY OVERRELAXATION
                C
ISN 0003              COMMON/BK/IIM,IIP,JJM,JJP,KK,NTOT,IV,JV,II,JJ,M,N,VP(30),
                     1XYZ(2080,3),VV(30,20,10),XP(30),XM(10),YP(20),YM(10),ZZ(10),
                     2XX(40),YY(30),ILX,IUX,KUK,MBC,MBD,VRF,NFPS,SKPRFL,SKPLST
ISN 0004              COMMON/FLD/X(2080,2),COEF(2080,7),INDX(2080,6),SKPCO
ISN 0005              COMMON/CCC/CN,CS,CE,CW,CU,CD,CC,NN,NS,NE,NW,NU,ND
                C
ISN 0006              INTEGER OO,ON/'NORT'/,OS/'SOUT'/,OE/'EAST'/,OW/'WEST'/,
                     1 OU/'UP  '/,OD/'DOWN'/
                C     ASSUME ASYMPTOTIC MONOPOLE AT INFINITY
                C
ISN 0007              ALPHAF(UUU)=ABS(UUU/RS)
                C
                C     NDO=POSITIVE FOR DIAGNOSTIC OUTPUT
ISN 0008              NDO=0
                C
ISN 0009              WRITE(M,1000)
ISN 0010        1000  FORMAT(1H1/18HOFIELD CALCULATION)
ISN 0011              WRITE(M,2000)
ISN 0012        2000  FORMAT(////1X,17HCOEFFICIENT ARRAY)
ISN 0013              X0=.5*XP(IV)
ISN 0014              Y0=.5*YP(JV)
ISN 0015              ZOLD=0.
ISN 0016              DO 600 N=1,NTOT
ISN 0017              RS=(XYZ(N,1)-X0)**2 +(XYZ(N,2)-Y0)**2 +XYZ(N,3)**2
ISN 0018              CALL FIND (I,J,K)
ISN 0019              IF(ZZ(K).LE.ZOLD.AND.N.GT.1) GO TO 200
ISN 0021              ZOLD=ZZ(K)
ISN 0022              WRITE(M,3000) K,ZZ(K)
ISN 0023        3000  FORMAT(  //1X,2HZ(,I2,2H)=,F6.3/
                     1 12X,1HD,17X,1HS,17X,1HW,17X,1HC,17X,1HE,17X,1HN,17X,1HU)
ISN 0024        200   CC=0.
                C
                C  MODIFICATION TO SOLVE HELMHOLTZ EQUATION USING LINEARIZED SPACE
                C  CHARGE.   HELM = DEBYE-LENGTH-LIKE PARAMETER.  (ASSUMES POTEN-
                C  TIALS ARE DIMENSIONLESS)
                C
ISN 0025              HELM=0.0
ISN 0026              VOLSQ=1.
ISN 0027              DO 300 MP=1,2
ISN 0028              CALL CNS(MP,C,AREA)
ISN 0029              IF (MP.EQ.1) OO=ON
ISN 0031              IF (MP.EQ.2) OO=OS
ISN 0033              IF (NDO.GT.0) WRITE (M,888) N,I,J,K,OO,AREA,C
ISN 0035        888   FORMAT(1X,18HN,I,J,K,OO,AREA,C=,I4,2X,3I3,1X,A5,1P2E16.4)
ISN 0036              CC=CC+C
ISN 0037              IF(C.GT.0.) GO TO 250
ISN 0039              YYY=XYZ(N,2)-Y0
ISN 0040               ALPHA=ALPHAF(YYY)
ISN 0041              IF (NDO.GT.0) WRITE (M,999) N,I,J,K,ALPHA
ISN 0043        999   FORMAT(1X,14HN,I,J,K,ALPHA=,I4,2X,3I3,1PE16.4)
```

```
ISN 0044              CC=CC+AREA*ALPHAF(YYY)
ISN 0045       250    IF(MP.EQ.1) CN=C
ISN 0047              IF(MP.EQ.2) CS=C
ISN 0049       300    CONTINUE
ISN 0050              VOLSQ=VOLSQ*AREA
ISN 0051              DO 400 MP=1,2
ISN 0052              CALL CEW(MP,C,AREA)
ISN 0053               IF (MP.EQ.1) DD=DE
ISN 0055               IF (MP.EQ.2) DD=DW
ISN 0057              IF (NDD.GT.0) WRITE (M,888) N,I,J,K,DD,AREA,C
ISN 0059              CC=CC+C
ISN 0060              IF(C.GT.0.) GO TO 350
ISN 0062              XXX=XYZ(N,1)-X0
ISN 0063               ALPHA=ALPHAF(XXX)
ISN 0064              IF (NDD.GT.0) WRITE (M,999) N,I,J,K,ALPHA
ISN 0066              CC=CC+AREA*ALPHAF(XXX)
ISN 0067       350    IF(MP.EQ.1) CE=C
ISN 0069              IF(MP.EQ.2) CW=C
ISN 0071       400    CONTINUE
ISN 0072              VOLSQ=VOLSQ*AREA
ISN 0073              DO 500 MP=1,2
ISN 0074              CALL CUD(MP,C,AREA)
ISN 0075               IF (MP.EQ.1) DD=DU
ISN 0077               IF (MP.EQ.2) DD=DD
ISN 0079              IF (NDD.GT.0) WRITE (M,888) N,I,J,K,DD,AREA,C
ISN 0081              CC=CC+C
ISN 0082              IF(C.GT.0..OR.(C.EQ.0..AND.MP.EQ.2))GO TO 450
ISN 0084               ALPHA=ALPHAF(XYZ(N,3))
ISN 0085              IF (NDD.GT.0) WRITE (M,999) N,I,J,K,ALPHA
ISN 0087              CC=CC+AREA*ALPHAF(XYZ(N,3))
ISN 0088       450    IF(MP.EQ.1) CU=C
ISN 0090              IF(MP.EQ.2) CD=C
ISN 0092       500    CONTINUE
ISN 0093              VOLSQ=VOLSQ*AREA
ISN 0094              VOL=SQRT(VOLSQ)
ISN 0095              IF(HELM.GT.0.) CC=CC+VOL/HELM**2
ISN 0097              CALL ARRAY
ISN 0098       600    CONTINUE
               C
ISN 0099              CALL RELAX
ISN 0100              RETURN
ISN 0101              END
```

```
        COMPILER OPTIONS - NAME=  MAIN,OPT=02,LINECNT=60,SIZE=0000K,
                           SOURCE,EBCDIC,NOLIST,NODECK,LOAD,MAP,NOEDIT,NOID,NOXREF
ISN 0002              BLOCK DATA
ISN 0003              COMMON/CD/PVOLTS,XMACH,DENST,NN,PARTCL(2),PART1(2),PART2(2)
ISN 0004              REAL PART1/'IONS','    '/,PART2/'ELEC','TRON'/
ISN 0005              END
```

Appendix B

Computer Programs: Electric Fields Produced by Cloud-to-Ground Lightning Flashes

The following four pages contain a listing of the computer programs written to compute the electric field produced on the ground as a function of time and distance from "ground zero" by the charges associated with a cloud-to-ground lightning flash. This program was written by Jerry L. Bohannon.

```
TITL CLOUD-TO-GROUND SIMULATION
BATCH
LAE= STROKE
DBUG
      IMPLICIT INTEGER*2 (I-N)
      DIMENSION RSI(2,10),RSIS(2,10)
      DATA TPIE/5.56062E-11/,TPIM/2.0E-7/
      DATA ICARDS/'C'/,ITERM/'T'/,IY/'Y'/,IN/'N'/
      DATA IMA/X'1D15'/,ICY/X'1D16'/,IBEL/X'0707'/,IBG/X'1E10'/
      DATA IRD/X'1D11'/,IGR/X'1D12'/,IYE/X'1D13'/,IBL/X'1D14'/
      DATA IA7N/X'0E'/,IA7F/X'0F'/,NULL/X'00'/,IHOME/X'08'/
      DATA IBGY/X'1E13'/
      DATA RSI(1,1)/0.0/,RSI(2,1)/0.0/,RSI(2,10)/0.0/
      DATA PIE/3.1415926/
      DATA RHO/2.0E-9/
      CROOT=1./3.
      WRITE(14,1)
      FORMAT('1')
      DO 1000 I=1,32000
C     K=I
      WRITE(14,4) IA7N,IMA,IBEL,IA7F
      FORMAT(2A2,' LIGHTNING BOLT SIMULATION+ ',R01',2A2)
0     WRITE(14,11) IBL,IGR
1     FORMAT(A2,' READ DATA FROM CARDS OR TERMINAL',A2)
      READ(15,12) IWHERE
2     FORMAT(A1)
3     IF(IWHERE.EQ.ICARDS)GOTO 50
      IF(IWHERE.EQ.ITERM)GOTO 70
      WRITE(14,14) IRD,IRG
4     FORMAT(A2,' TRY AGAIN',A2)
      GOTO 10
0     READ(1,51,END=999) YO,QCL,QSL,VSL,VRS,((RSI(I,J),I=1,2),J=2,9)
1     FORMAT(5(F6.0,2X)/8(2F10.0/))
      GOTO 90
0     WRITE(14,71) IMA
1     FORMAT(A2,' ENTER FLOATING POINT INITIAL CONDITIONS  F6.0')
      WRITE(14,75) IBL,ICY
5     FORMAT(A2,' INITIAL HEIGHT  KM',A2)
      READ(15,73) YO
      WRITE(14,76) IBL,ICY
6     FORMAT(A2,' CLOUD CHARGE   COUL',A2)
      READ(15,73) QCL
      WRITE(14,72) IBL,ICY
2     FORMAT(A2,' STEPPED LEADER CHARGE  COUL',A2)
      READ(15,73) QSL
3     FORMAT(F6.0)
      WRITE(14,74) IBL,ICY
4     FORMAT(A2,' STEPPED LEADER VELOCITY  E5 M/S',A2)
      READ(15,73) VSL
      WRITE(14,77) IBL,ICY
7     FORMAT(A2,' RETURN STROKE VELOCITY  E7 M/S',A2)
      READ(15,73) VRS
3     WRITE(14,80) IBL,ICY
)     FORMAT(A2,' ENTER 8 TIMES (MS) AND CURRENTS (KAMP) TO DEFINE THE'/
     <' RETURN STROKE  2F10.0'/'!',(9),'!',A2)
      DO 82 J=2,9
      READ(15,81) RSI(1,J),RSI(2,J)
      IF(RSI(1,J).LT.0.0)GOTO 78
      CONTINUE
```

```
81    FORMAT(2F10.0)
90    VSLS=VSL
      RSI(1,10)=RSI(1,9)
      DO 1002 J=1,10
      RSIS(1,J)=RSI(1,J)
      RSIS(2,J)=RSI(2,J)
      RSI(1,J)=RSI(1,J)/1000.
      RSI(2,J)=RSI(2,J)*1000.
1002  CONTINUE
      QCL=-QCL
      QSL=-QSL
      YOS=YO
      RAD=(0.75*ABS(QCL)/RHO/PIE)**CROOT
      DO 1005 I=2,9
      A=RSI(2,I)
      B=RSI(2,I-1)
      C=RSI(2,I+1)
      IF(A.GT.B.AND.A.GT.C) IQT=I
1005  CONTINUE
      VRSS=VRS
100   VSL=-VSL*1.0E5
      YO=YO*1000.0
      VRS=VRS*1.0E7
      DTSL=1.0E-4
105   WRITE(14,110) IBL,ICY
110   FORMAT(A2,"WHAT IS RADIUS",A2)
      READ(15,73) D
      WRITE(13,111) IRD,IBGY
111   FORMAT(2A2/"1")
      DO 1001 I=1,32000
1001  K=I
      WRITE(13,149)
  149 FORMAT(1X,"SI UNITS"//)
150   WRITE(13,151) YOS,QCL,QSL,VSLS,VRSS,RSIS,D
151   FORMAT(1X,"HEIGHT= ",F7.0," KM"/1X,"Q-CLOUD= ",F7.1," C"/
     $1X,"Q-LEADER= ",F6.1," C"/1X,"V-LEADER= ",F6.1," E5 M/S"/1X,
     $ "V-RETURN= ",F6.1," E7 M/S"/1X,"RETURN STROKE MS. KAMP"/
     $10(2F10.4/)//1X,"RADIUS= ",F6.0," M"///)
      WRITE(13,152) IRG,IRD
152   FORMAT(1X,
     $A2,8X,"T",15X,"E",15X,"Q",16X,"H",A2)
      T=0.0
      SLRY2=1.0/(D*D+YO*YO)
      SLRY=SQRT(SLRY2)
      YC=YO+RAD
      SLRQC2=1.0/(D*D+YC*YC)
      SLRQCL=SQRT(SLRQC2)*SLRQC2
      DI=1.0/D
      X=YO
      EMAX=0.0
200   CONTINUE
      SLRX2=1.0/(D*D+X*X)
      SLRX=SQRT(SLRX2)
      SLRX32=SLRX*SLRX2
      E=QSL/TPIE/YO*(SLRX-SLRY)+SLRQCL*YC/TPIE*(QCL-QSL*(1.-X/YO))
      IF(ABS(E).GT.ABS(EMAX)) EMAX=E
      IF(ABS(E).LT.5.0E4) GOTO 211
      WRITE(13,210)T,E,X
210   FORMAT(F16.7, F16.0,16X, F16.1)
```

```
215   FORMAT(F16.7, F16.0,F16.5,F16.1,I10,F16.7,F16.0)
211   IF(ABS(E).LT.5.0E4.OR.X.GT.0.5E3) DTSL=1.0E-3
      T=T+DTSL
      IF(X.LT.50.) GOTO 500
      X=YO+VSL*T
      IF(X.LT.0.0) GOTO 500
      DTSL=1.0E-4
      GOTO 200
500   CONTINUE
      T=T-DTSL
      WRITE(13,501)
501   FORMAT(1X,"  ")
      ESL=E
      QRC=QSL-QCL
      PL=-QSL/YO
      SLRYO3=YC*SLRQCL
      KRNT=1
      RI=0.0
      TR=0.0
      KOLD=0
      Q=0.0
510   CONTINUE
      CALL CURENT(RSI,Q,DT,TR,RI,KRNT,KOLD)
      IF(RI.LE.0.0) GOTO 600
      T=T+DT
      Y=VRS*TR
      IF(Y.GT.YO) GOTO 522
      P=Q/Y
      SLRYR=1.0/SQRT(D*D+Y*Y)
      E=ESL+P*(DI-SLRYR)/TPIE
      IF(ABS(E).GT.ABS(EMAX)) EMAX=E
      IF(IQT.LT.KRNT.AND.ABS(E).LT.5.0E4) GOTO 510
      WRITE(13,215) T,E,Q,Y,KRNT,TR,RI
      GOTO 510
 22   WRITE(13,501)
 20   CONTINUE
      P=Q/YO
      IF(P.GT.PL) GOTO 572
      E=ESL+P*(DI-SLRY)/TPIE
      IF(ABS(E).GT.ABS(EMAX)) EMAX=E
      IF(IQT.LT.KRNT.AND.ABS(E).LT.5.0E4) GOTO 521
      WRITE(13,215) T,E,Q,YO,KRNT,TR,RI
 21   CALL CURENT(RSI,Q,DT,TR,RI,KRNT,KOLD)
      IF(RI.LE.0.0) GOTO 600
      T=T+DT
      GOTO 520
 72   WRITE(13,501)
 70   CONTINUE
      QRS=Q+QSL
      IF(QRS.GT.QRC) GOTO 600
      E=ESL+PL*(DI-SLRY)/TPIE+QRS*SLRYO3/TPIE
      IF(ABS(E).GT.ABS(EMAX)) EMAX=E
      IF(IQT.LT.KRNT.AND.ABS(E).LT.5.0E4) GOTO 571
      WRITE(13,215) T,E,Q,YO,KRNT,TR,RI
 71   CALL CURENT(RSI,Q,DT,TR,RI,KRNT,KOLD)
      IF(RI.LE.0.0) GOTO 600
      T=T+DT
      GOTO 570
 0    WRITE(13,599) Q ,EMAX
```

```
99    FORMAT(//1X,"QRT= ",F10.4," C",5X,"EMAX= ",E12.4," V/MC")
      WRITE(14,601) IBG,IBL,IGR,IBEL
601   FORMAT(2A2," DO YOU WANT ANOTHER RADIUS",2A2)
602   READ(15,12) IAD
      IF(IAD.EQ.IY) GOTO 105
      IF(IAD.EQ.IN) GOTO 650
      WRITE(14,14) IRD,IGR
      GOTO 602
50    WRITE(14,651) IBL,IGR
51    FORMAT(A2," DO YOU WANT ANOTHER EVENT",A2)
52    READ(15,12) IE
      IF(IE.EQ.IY) GOTO 13
      IF(IE.EQ.IN) GOTO 950
      WRITE(14,14) IRD,IGR
      GOTO 652
99    WRITE(14,998) IRD
98    FORMAT(A2," NO MORE CARDS")
50    WRITE(14,951) IMA,IGR
51    FORMAT(A2," END OF PROGRAM",A2)
      STOP 1
      END
LAB=  CURENT
DBUG
      SUBROUTINE CURENT(RSI,Q,DT,TR,RI,KRNT,KOLD)
      IMPLICIT INTEGER*2 (I-N)
      DIMENSION RSI(2,10)
      IF(KOLD.EQ.KRNT) GOTO 50
      TAU=RSI(1,KRNT+1)-RSI(1,KRNT)
      IF(TAU.LE.0.0) GOTO 100
      IF(TAU.LE.1.0E-5) DT=0.5E-6
      IF(TAU.GT.1.0E-5.AND.TAU.LE.1.0E-4) DT=1.0E-5
      IF(TAU.GT.1.0E-4.AND.TAU.LE.1.0E-3) DT=1.0E-4
      IF(TAU.GT.1.0E-3.AND.TAU.LE.1.0E-2) DT=1.0E-3
      IF(TAU.GT.1.0E-2.AND.TAU.LE.1.0E-1) DT=1.0E-2
      IF(TAU.GT.1.0E-1) DT=0.025
      DELI=(RSI(2,KRNT+1)-RSI(2,KRNT))/TAU
      IF(Q.EQ.0.0) RI1=0.0
      TRR=TR+DT
      IF(TRR.GT.RSI(1,KRNT+1)) DT=RSI(1,KRNT+1)-TR
      RI=RI+DELI*DT
      RI2=RI
      Q=Q+DT*(RI2+RI1)/2.
      TR=TR+DT
      KOLD=KRNT
      IF(TR.GE.RSI(1,KRNT+1)) KRNT=KRNT+1
      RI1=RI2
      RETURN
100   CONTINUE
      RI=0.0
      RETURN
      END
END
```

Appendix C

Computer Output Listing: Cloud-to-Ground Lightning Flash Density

The following seven pages are the computed output from the program that calculates the lightning flash density (cloud-to-ground) from the monthly thunderstorm days using the Pierce Conversion. This program, written by Jerry L. Bohannon, uses the Normals, Means and Extremes data from "Local Climatological Data -- Annual Summaries for 1977" published by the National Oceanic and Atmospheric Administration, Environmental Data Service, Asheville, North Carolina (available also on magnetic tape).

```
      ∇COMPUPOT [⎕]∇
      ∇ AAR←WID COMPUPOT HI
[1]   ⍝    THIS FUNCTION COMPUTES THE ELECTRIC POTENTIAL IN A REGION ARROUND
[2]   ⍝ ONE BILLBOARD OF THE RECTENNA,  THE MEASUREMENT AREA STARTS 31.96 METERS
[3]   ⍝ FROM THE LEFT HAND EDGE OF THE RECTENNA AND EXTENDS TO THE RIGHT 'AC' METERS,
[4]   ⍝ THE BOTTOM  OF THE MEASUREMENT AREA IS AT GROUND LEVEL, WHILE THE TOP
[5]   ⍝ IS 'UP' METERS HIGH,
[6]   ⍝    THE RESOLUTION IS CONTROLLED BY THE ARGUMENTS OF THE FUNCTION,  THE
[7]   ⍝ LEFT ARGUMENT SPECIFIES THE NUMBER OF COLUMNS IN THE OUTPUT,  THE RIGHT
[8]   ⍝ ARGUMENT IS THE NUMBER OF ROWS,
[9]   ⍝    THE FORMAT OF THE OUTPUT IS AN ARRAY OF NUMBERS IN SCIENTIFIC NOTATION
[10]  ⍝ WITH ONLY ONE SIGNIFICANT DIGIT PRINTED,
[11]  POT←(HI,WID)⍴0
[12]  ⎕PP←1
[13]  G←R←1
[14] LOOPH:H1←(G-1)×UP÷HI-1
[15]  R←1
[16] LOOPL:L1←31.96+(R-1)×AC÷WID-1
[17]  POT[G;R]←L1 FIELD H1
[18]  R←R+1
[19]  →(R≤WID)/LOOPL
[20]  G←G+1
[21]  →(G≤HI)/LOOPH
[22]  TRY←TRY+1
[23]  DA←1↓3↑⎕TS.
[24]  'THIS IS RUN NUMBER ',(⍕TRY),DATE
[25]  'THE CALCULATED VALUES OF THE ELECTRIC POTENTIAL, IN VOLTS, ARE SHOWN BELOW,'
[26]  ''
[27]  ''
[28]  AAR←POT+⍉POT
[29]  5⍴⎕AV[201]·
[30]  ⎕PP←10
[31]  'THE VECTOR OF LINE CHARGES USED IS... ',(⍕LA),' COULOMBS PER METER,'
[32]  'THE SUM OF THE LINE CHARGES IS ',(⍕+/LA),' COULOMBS PER METER,'
[33]  'THE TOP OF THE MEASUREMENT ARRAY IS ',(⍕UP),' METERS HIGH,'
[34]  'THE RIGHT EDGE OF THE ARRAY IS ',(⍕L1),' METERS FROM THE FIRST BILLBOARD,'
[35]  'THERE ARE ',(⍕AC÷WID),' COLUMNS PER METER, AND ',(⍕UP÷HI),' ROWS PER METER IN THE ARRAY,'
[36]  'RUN NO. ',(⍕TRY),DATE
[37]  ⎕PP←1
[38]  5⍴⎕AV[201]
[39]  →(SIGN=0)/0
[40]  'THE ARRAY BELOW SHOWS THE SIGN OF EACH OF THE NUMBERS IN THE ABOVE ARRAY,'
[41]  ''
[42]  XPOT
[43]  'THIS IS RUN NUMBER ',(⍕TRY),DATE
      ∇
```

```
      ∇PROTECT [⎕]∇
      ∇ WID PROTECT HI
[1]   ⍝    THIS FUNCTION COMPUTES THE ELECTRIC POTENTIAL IN A REGION OF SPACE
[2]   ⍝ DUE TO A CHARGED WIRE LOCATED SOME FIXED PERPENDICULAR DISTANCE FROM
[3]   ⍝ THE TOP OF EACH BILLBOARD OF THE RECTENNA,  THE MEASUREMENT AREA IS
[4]   ⍝ EXACTLY THE SAME AS THAT USED IN ((COMPUPOT)),  AS WITH ((COMPUPOT))
[5]   ⍝ THE RESOLUTION IS DETERMINED BY THE ARGUMENTS OF THE FUNCTION,
[6]   ⍝    THE FUNCTION DOES NOT PRINT ANY OUTPUT,  THE OUTPUT IS CONTAINED IN
[7]   ⍝ THE VARIABLE, ((PROT)),  THIS VARIABLE WILL HAVE THE SAME DIMENTIONS AS
[8]   ⍝ ((POT)), THE VARIABLE CONTAINING THE OUTPUT FROM ((COMPUPOT)),
[9]    PROT←(HI,WID)⍴0
[10]   G1←R1←1
[11]  ⍝  ((LOOPH)) COMPUTES ALL OF THE VERTICAL INDICES,
[12]  LOOPH:H2←(G1-1)×UP÷HI-1
[13]   R1←1
[14]  ⍝   ((LOOPL)) COMPUTES THE HORIZONTAL INDICES AND CALLS ((FIELDW)),
[15]  LOOPL:L2←31.96÷(R1-1)×AC÷WID-1
[16]   PROT[G1;R1]←L2 FIELDW H2
[17]   R1←R1+1
[18]   →(R1≤WID)/LOOPL
[19]   G1←G1+1
[20]   →(G1≤HI)/LOOPH
[21]   PROT←⍉PROT
[22]   TRY1←TRY1+1
[23]   'THIS IS RUN NUMBER ',(⍕TRY1),' OF PROTECT',DATE
[24]   ⎕PP←10
[25]   'THE PROTECTING WIRE IS LOCATED ',(⍕XU1),' METERS FROMT THE'
[26]   'LEFT EDGE OF THE ARRY, AND ',(⍕S1×XU1),' METERS FROM THE BOTTOM,'
      ∇
```

```
      ∇FIELD [⎕]∇
      ∇ UHL←L FIELD H
[1]   ⍝    THIS FUNCTION COMPUTES THE ELECTRIC POTENTIAL AT ANY POINT, (L,H)
[2]   ⍝ IN THE SPACE AROUND THE ARRAY OF FIVE BILLBOARDS,
[3]   LI←15.93×¯1+⍳N
[4]   XJ←(9.38×⍳N)÷N↑⍴LA
[5]   S←3○02÷9
[6]   A←L-XJ
[7]   I←1
[8]   UI←N⍴0
[9]   BBLOOP:NM←((H-S×XJ)*2)+NA←(A-LI[I])*2
[10]  DM←((H+S×XJ)*2)+NA
[11]  UI[I]←+/-(LA÷02×E0)×⍟(NM÷DM)×0.5
[12]  I←I+1
[13]  →(I<N+1)/BBLOOP
[14]  UHL←(¯100000×H)++/UI
      ∇
```

```
      ∇FIELDW [⎕]∇
      ∇ P←L FIELDW H
[1]   ⍝    THIS FUNCTION COMPUTES THE ELECTRIC POTENTIAL AT ANY POINT, (L,H),
[2]   ⍝ DUE TO THE CHARGED PROTECTION WIRE ABOVE THE BILLBOARD,  THIS WIRE IS
[3]   ⍝ ASSUMED TO BE PARALLEL TO THE BILLBOARD AND LOCATED A PERPENDICULAR
[4]   ⍝ DISTANCE, ((SPACE)), FROM THE TOP OF THE BILLBOARD,
[5]   ⍝    THE CHARGE ON THE WIRE IS ((LW)),
[6]   LI1←15.93×¯1+⍳N
[7]   N←⍴LW←,LW
[8]   LONG←12.24÷2○THTA←¯3○(÷12.24)×SPACE
[9]   XJ1←,XJ1←LONG×2○THTA+02÷9
[10]  S1←3○(02÷9)÷THTA
[11]  A1←L-XJ1
[12]  I←1
[13]  UI1←N⍴0
[14] LOOP:NM1←((H-S1×XJ1)*2)+NA1←(A1-LI1[I])*2
[15]  DM1←((H+S1×XJ1)*2)+NA1
[16]  UI1[I]←+/-(LW÷02×E0)×⍟(NM1÷DM1)×0.5
[17]  I←I+1
[18]  →(I<N+1)/LOOP
[19]  P←+/UI1
      ∇
```

STATE	STATION	THUNDERSTORM DAYS (NO./YEAR)	GROUND STRIKE DENSITY (NO./YR./KM^2)
AL	BIRMINGHAM	58.71	13.87
AL	HUNTSVILLE	59.20	13.34
AL	MOBILE	79.78	27.07
AL	MONTGOMERY	62.13	15.44
AK	ANCHORAGE	1.12	0.39
AK	ANNETTE	1.43	0.60
AK	BARROW	0.07	0.06
AK	BARTER ISLAND	0.26	0.17
AK	BETHEL	1.39	0.51
AK	BETTLES	4.67	0.78
AK	BIG DELTA	2.60	0.41
AK	COLD BAY	0.05	0.04
AK	FAIRBANKS	5.12	0.83
AK	GULKANA	4.70	0.76
AK	HOMER	0.38	0.15
AK	JUNEAU	0.32	0.24
AK	KING SALMON	1.31	0.48
AK	KODIAK	0.29	0.09
AK	KOTZEBUE	0.52	0.24
AK	MC GRATH	6.77	1.05
AK	NOME	0.42	0.19
AK	ST PAUL ISLAND	0.05	0.05
AK	SHEYMA ISLAND	0.15	0.10
AK	SUMMIT	5.00	0.82
AK	TALKEETNA	4.30	0.77
AK	UNALKLEET	1.90	0.46
AK	YAKUTAT	1.59	0.60
AZ	FLAGSTAFF	50.63	15.87
AZ	PHOENIX	23.03	4.60
AZ	TUCSON	39.84	13.29
AZ	WINSLOW	36.34	9.83
AZ	YUMA	7.26	1.43
AR	FORT SMITH	57.06	11.84
AR	LITTLE ROCK	56.97	11.51
AS	PAGO PAGO	26.09	3.73
CA	BAKERSFIELD	2.80	0.95
CA	BISHOP	13.24	2.21
CA	BLUE CANYON	11.83	1.97
CA	EUREKA	4.55	1.23
CA	FRESNO	5.43	1.37
CA	LONG BEACH	3.71	1.10
CA	LOS ANGLES (CITY)	6.21	1.43
CA	LOS ANGLES (LAX)	3.51	1.10
CA	MOUNT SHASTA	13.27	2.16
CA	OAKLAND	2.28	0.87
CA	RED BLUFF	9.70	1.82
CA	SACRAMENTO	4.76	1.27

STATE	STATION	THUNDERSTORM DAYS (NO./YEAR)	GROUNDSTRIKE DENSITY (NO./YR./KM^2)
CA	SANDBERG	4.22	1.14
CA	SAN DIEGO	2.70	0.96
CA	SAN FRANCISCO (CITY)	2.25	0.88
CA	SAN FRANCISCO (SFO)	2.12	0.55
CA	STOCKTON	3.11	1.01
CA	SANTA MARIA	2.32	0.89
CO	ALAMOSA	44.42	12.92
CO	COLORADO SPRINGS	59.69	22.43
CO	DENVER	41.33	11.02
CO	GRAND JUNCTION	34.32	6.38
CO	PUEBLO	40.32	10.99
CT	BRIDGEPORT	21.57	3.50
CT	HARTFORD	22.30	3.62
DE	WILMINGTON	31.03	5.73
DC	WASHINGTON (DCA)	29.07	5.18
DC	WASHINGTON (IAD)	27.13	4.60
FL	APALACHICOLA	70.19	22.99
FL	DAYTONA BEACH	79.61	29.25
FL	FORT MYERS	94.57	47.04
FL	JACKSONVILLE	63.94	20.26
FL	KEY WEST	52.66	19.38
FL	LAKELAND	99.50	48.56
FL	MIAMI	74.04	26.37
FL	ORLANDO	81.21	32.79
FL	ORLANDO (MC COY AFB)	78.62	30.37
FL	PENSACOLA	74.13	22.90
FL	TALLAHASSEE	86.37	35.05
FL	TAMPA	88.19	40.90
FL	WEST PALM BEACH	78.63	28.69
GA	ATHENS	51.82	13.00
GA	ATLANTA	50.19	11.57
GA	AUGUSTA	56.15	15.41
GA	COLUMBUS	58.71	15.61
GA	MACON	56.83	15.43
GA	ROME	61.42	15.87
GA	SAVANNAH	64.33	20.62
GU	TAGUAC	27.09	4.79
HI	HILO	8.75	1.67
HI	HONOLULU	7.07	1.48
HI	KAHULUI	4.95	1.20
HI	LIHUI	8.81	1.64

STATE	STATION	THUNDERSTORM DAYS (NO./YEAR)	GROUND-STRIKE DENSITY (NO./YR./KM^2)
ID	BOISE	14.34	2.34
ID	LEWISTON	15.75	2.45
ID	POCATELLO	23.11	4.02
IL	CARIO	52.77	10.95
IL	CHICAGO (MIDWAY)	40.54	7.53
IL	CHICAGO (O'HARE)	38.42	5.92
IL	MOLINE	47.36	10.01
IL	PEORIA	48.94	10.25
IL	ROCKFORD	42.19	5.38
IL	SPRINGFIELD	50.00	10.79
IN	EVANSVILLE	45.73	8.87
IN	FORT WAYNE	41.00	7.87
IN	INDIANAPOLIS	44.69	8.87
IN	SOUTH BEND	42.89	8.64
IA	BURLINGTON	50.58	11.06
IA	DES MOINES	49.73	11.22
IA	DUBUQUE	44.93	9.29
IA	SIOUX CITY	45.38	10.49
IA	WATERLOO	41.70	8.51
KS	CONCORDIA	58.93	15.71
KS	DODGE CITY	53.03	14.32
KS	GOODLAND	48.74	13.59
KS	TOPEKA	57.58	14.14
KS	WICHITA	55.29	13.25
KY	LEXINGTON	46.76	10.22
KY	LOUISVILLE	45.40	9.13
LA	ALEXANDRIA	68.07	16.95
LA	BATON ROUGE	70.46	20.07
LA	LAKE CHARLES	76.88	22.59
LA	NEW ORLEANS	68.93	20.38
LA	SHREVEPORT	54.16	10.21
ME	CARIBOU	20.33	3.57
ME	PORTLAND	18.05	2.98
MD	BALTIMORE	28.44	5.10
MA	BOSTON	19.33	3.14
MA	NANTUCKET	20.27	3.09
MA	WORCESTER	21.27	3.51

STATE	STATION	THUNDERSTORM DAYS (NO./YEAR)	GROUNDSTRIKE DENSITY (NO./YR./KM^2)
MI	ALPENA	33.29	6.25
MI	DETROIT (DTT)	32.02	5.67
MI	DETROIT (DTW)	33.26	5.57
MI	FLINT	33.03	5.97
MI	GRAND RAPIDS	36.71	6.50
MI	HOUGHTON LAKE	38.54	7.65
MI	LANSING	34.17	6.18
MI	MARQUETTE	28.07	5.03
MI	MUSKEGON	37.34	6.83
MI	SAULT STE MARIE	29.44	5.22
MN	DULUTH	34.66	7.38
MN	INTERNATIONAL FALLS	31.42	5.67
MN	MINNEAPOLIS	36.79	7.41
MN	ROCHESTER	41.00	8.32
MN	SAINT CLOUD	35.76	7.54
MS	JACKSON	65.79	16.30
MS	MERIDAN	58.59	13.31
MO	COLUMBIA	51.50	10.40
MO	KANSAS CITY (MCI)	51.20	11.39
MO	KANSAS CITY (MKC)	49.66	10.59
MO	SAINT JOSEPH	56.35	13.76
MO	ST. LOUIS	44.55	8.61
MO	SPRINGFIELD	58.00	13.00
MT	BILLINGS	28.79	6.00
MT	GLASGOW	27.11	5.30
MT	GREAT FALLS	25.60	5.17
MT	HAVRE	21.60	3.86
MT	HELENA	33.81	8.32
MT	KALISPELL	22.75	3.96
MT	MILES CITY	28.48	6.02
MT	MISSOULA	23.61	4.36
NE	GRAND ISLAND	47.99	11.76
NE	LINCOLN (APT)	46.33	10.77
NE	LINCOLN (CITY)	49.33	11.99
NE	NORFOLK	50.20	13.11
NE	NORTH PLATTE	45.92	11.95
NE	OMAHA (CITY)	40.50	8.00
NE	OMAHA (EPPLY FIELD)	48.60	11.26
NE	SCOTTSBLUFF	43.56	11.92
NE	VALENTINE	45.22	12.79
NV	ELKO	20.72	3.47
NV	ELY	32.00	6.75
NV	LAS VEGAS	14.97	2.05
NV	RENO	13.54	2.06
NV	WINNEMUCCA	14.36	2.24

STATE	STATION	THUNDERSTORM DAYS (NO./YEAR)	GROUND-STRIKE DENSITY (NO./YR./KM^2)
NH	CONCORD	20.47	3.49
NH	MT WASHINGTON	15.33	2.74
NJ	ATLANTIC CITY	25.47	4.36
NJ	NEWARK	25.47	4.40
NJ	TRENTON	33.22	6.53
NM	ALBUQUERQUE	42.34	11.18
NM	CLAYTON	54.11	17.03
NM	ROSWELL	32.60	6.30
NY	ALBANY	27.64	5.20
NY	BINGHAMTON	31.42	5.94
NY	BUFFALO	30.74	5.18
NY	NEW YORK (CITY)	19.47	3.16
NY	NEW YORK (JFK)	22.32	3.56
NY	NEW YORK (LA GUARDIA)	24.24	4.01
NY	ROCHESTER	29.24	5.21
NY	SYRACUSE	29.39	5.43
NC	ASHEVILLE	49.00	12.16
NC	CAPE HATTERAS	44.75	9.23
NC	CHARLOTTE	41.39	9.35
NC	GREENSBORO	46.57	11.30
NC	RALEIGH	45.67	10.67
NC	WILMINGTON	46.12	10.92
ND	FARGO	32.33	6.98
ND	BISMARK	33.58	7.99
ND	WILLISTON	26.77	5.65
OH	AKRON	40.41	8.13
OH	CINCINNATI (ABSE OBS)	50.41	11.52
OH	CINCINNATI (APT)	44.23	9.15
OH	CLEVELAND	36.42	6.65
OH	COLUMBUS	42.45	8.93
OH	DAYTON	40.32	7.85
OH	TOLEDO	40.00	8.11
OH	MANSFIELD	39.78	7.73
OH	YOUNGSTOWN	35.85	6.68
OK	OKLAHOMA CITY	50.68	10.84
OK	TULSA	52.26	11.21
OR	ASTORIA	7.67	1.52
OR	BURNS	13.86	2.02
OR	EUGENE	4.80	1.25
OR	MEACHAM	15.70	2.37
OR	MEDFORD	8.52	1.53

STATE	STATION	THUNDERSTORM DAYS (NO./YEAR)	GROUND STRIKE DENSITY (NO./YR./KM^2)
OR	PENDLETON	9.90	1.64
OR	PORTLAND	6.86	1.46
OR	SALEM	5.50	1.32
OR	SEXTON SUMMIT	5.70	1.20
PA	ALLENTOWN	32.82	6.31
PA	AVOCA	31.05	5.86
PA	ERIE	38.36	6.91
PA	HARRISBURG	32.79	6.34
PA	PHILADELPHIA	26.81	4.66
PA	PITTSBURG	36.28	6.80
PA	WILLIAMSPORT	34.29	7.11
PR	SAN JUAN	39.73	7.92
RI	BLOCK ISLAND	16.79	2.68
RI	PROVIDENCE	20.42	3.27
SC	CHARLESTON	56.46	16.60
SC	COLUMBIA	54.27	14.73
SC	GREER	43.37	9.54
SD	ABERDEEN	36.08	8.13
SD	HURON	40.34	9.63
SD	RAPID CITY	42.42	12.17
SD	SIOUX FALLS	43.69	10.23
TN	BRISTOL	45.50	10.55
TN	CHATTANOOGA	56.11	13.95
TN	KNOXVILLE	47.83	10.36
TN	MEMPHIS	52.93	10.28
TN	NASHVILLE	55.42	12.42
TN	OAK RIDGE	52.81	12.71
TX	ABILENE	41.73	7.65
TX	AMARILLO	48.81	12.28
TX	AUSTIN	40.81	6.71
TX	BROWNSVILLE	24.34	3.72
TX	CORPUS CHRISTI	30.76	4.69
TX	DALLAS-FT WORTH (DFW)	45.12	8.04
TX	DALLAS (LOVE FIELD)	40.15	5.62
TX	DEL RIO	35.36	6.39
TX	EL PASO	35.89	8.99
TX	HOUSTON	57.50	17.92
TX	LUBBOCK	45.32	10.12
TX	MIDLAND-ODESSA	36.45	6.76
TX	PORT ARTHUR	64.17	16.71
TX	SAN ANGELO	36.60	6.32
TX	SAN ANTONIO	36.00	5.74
TX	VICTORIA	45.13	9.91

STATE	STATION	THUNDERSTORM DAYS (NO./YEAR)	GROUND-STRIKE DENSITY (NO./YR./KM^2)
TX	WACO	45.44	7.82
TX	WICHITA FALLS	48.85	9.30
TT	JOHNSTON ISLAND	4.07	1.17
TT	KOROR ISLAND	36.65	5.46
TT	KWAJALEIN ISLAND	9.76	1.78
TT	MAJURO ATOLL	16.52	2.58
TT	PONAPE ISLAND	28.04	3.97
TT	TRUK ATOLL	19.42	2.82
TT	WAKE ISLAND	6.93	1.30
TT	YAP ISLAND	16.03	2.46
UT	MILFORD	32.06	7.33
UT	SALT LAKE CITY	35.29	6.84
UT	WENDOVER	29.00	5.77
VT	BURLINGTON	24.94	4.53
VA	LYNCHBURG	40.50	9.13
VA	NORFOLK	37.07	7.49
VA	RICHMOND	36.75	7.63
VA	ROANOKE	37.80	8.13
WA	OLYMPIA	4.65	1.24
WA	SEATTLE (APT)	7.27	1.60
WA	SEATTLE (CITY)	5.06	1.46
WA	SPOKANE	10.50	1.74
WA	STAMPEDE PASS	7.29	1.29
WA	WALLA WALLA	11.26	1.51
WA	YAKIMA	6.90	1.25
WV	BECKLEY	45.71	10.97
WV	CHARLESTON	43.37	9.42
WV	ELKINS	44.93	10.33
WV	HUNTINGTON	44.38	9.57
WV	PARKERSBURG	44.00	9.91
WI	GREEN BAY	34.79	6.49
WI	LA CROSSE	40.15	8.29
WI	MADISON	40.62	7.96
WI	MILWAUKEE	35.31	6.45
WY	CASPER	34.26	7.35
WY	CHEYENNE	49.86	15.41
WY	LANDER	31.71	7.05
WY	SHERIDAN	35.59	9.03

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16. ABSTRACT

Computer simulations and laboratory tests were used to evaluate the hazard posed by lightning flashes to ground on the SPS rectenna and to make recommendations on a lightning protection system for the rectenna. The distribution of lightning over the lower 48 of the continental United States was determined, as were the interactions of lightning with the rectenna and the modes in which those interactions could damage the rectenna. The studies showed that lightning protection was both required and feasible. Several systems of lightning protection were considered and evaluated. These included two systems that employed lightning rods of different lengths and placed on top of the rectenna's billboards and a third, distributed system. The distributed system is similar to one used by power distribution companies; it consists of short lightning rods all along the length of each billboard that are connected by a horizontal wire above the billboard. The system that not only affords greater protection than the others considered but offers easiest integration into the rectenna's structural design, was the distributed lightning protection system.

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